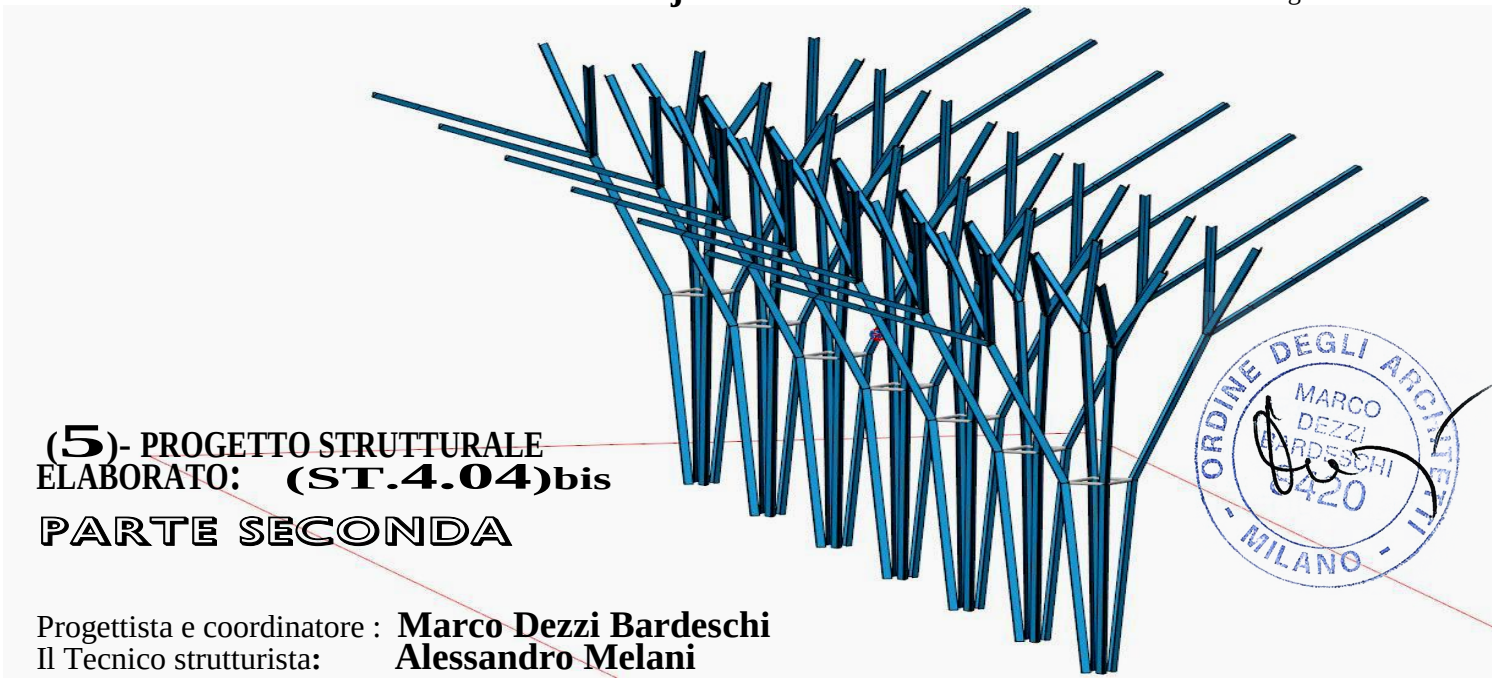
COMUNE DI CROTONE

MINISTERO PER I BENI E LE ATTIVITA' CULTURALI

Direzione Generale per i beni Culturali e Paesaggistici della Calabria
Sovrintenenza per i beni archeologici della Calabria

OGGETTO: Analisi statica dei telai in carpenteria d' acciaio che sostengono la copertura del grande atrio centrale del museo. Le strutture reticolari simulano con notevole ricercatezza formale una serie di "alberature" dis-poste in filare. Questo elemento, costituisce l' aspetto più caratterizzante per una costruzione praticamente ipogea, La mancanza di prospetti esterni riversa la vita dell' edificio verso l'atrio interno dal quale giunge anche la luce naturale. Le alberature sono inserite entro l' atrio stesso

Il R.U.P.: **Elisabetta Antonia Dominijanni** STRUTTURA: Vincenzo Felice Maria Dragonetti



(5)- PROGETTO STRUTTURALE
ELABORATO: (ST.4.04)bis

PARTE SECONDA

Progettista e coordinatore : **Marco Dezzi Bardeschi**
Il Tecnico strutturista: **Alessandro Melani**

VERIFICA DELLE MEMBRATURE IN ACCIAIO.
TABULATI NUMERICI (Codice di elaborazione: "MODEST, vers. 8.2).

Le verifiche delle alberature vengono effettuate considerando incastri perfetti al piede e presenza di ritegni sismici ai bordi della chioma. Il tutto in condizioni statiche ed in condizioni sismiche. I principali parametri di riferimento utilizzati nella calcolazione vengono riportati sulla **"Relazione Descrittiva modello strutturale e sulle ipotesi di calcolo assunte**" (**C.2**) Tutti i carichi e le azioni sismiche vengono combinati assieme in **VENTOTTO Condizioni di carico** successive (Vedi relazione di cui sopra) Le direzioni di applicazione delle azioni sismiche orizzontali si intendono coincidenti con gli assi principali di riferimento dell' alberatura.

La struttura in C.A., del tipo completamente intelaiato, viene considerata tipologicamente come: **"A pendolo inverso"** ai sensi della normativa sismica vigente (D.M. 14/01/2008)

L' intero modello comprende **2498** elementi bidimensionali che compongono le **14 "**lastre-chioma" di copertura . La maglia del reticolo che connette tutti questi elementi, comprende **1645** nodi. Le aste reali dei telai di supporto sono complessivamente. **372**

Un cosi alto numero di elementi bidimensionali derivano dalla scelta di operare una "meshiatura" in maglie di piccola dimensione dei continui (Lastre di copertura) ed ottenere di conseguenza una modellazione più aderente alla realtà. In conseguenza a tutte le condizioni esistenti, la modellazione prevede orizzontamenti deformabili nel proprio piano,.

Le masse sismiche presenti, risultano suddivise e distribuite su tutti i **1645** nodi corrispondenti nel modello, a quote variabili fra **+7,00 e +17,20** mt.

L'analisi sismica, del tipo dinamico, risulta estesa ai primi - **Centocinquanta** - modi caratteristici di vibrazione (necessari per eccitare una percentuale delle masse presenti maggiore dell' **85%)**

La verifica delle sezioni resistenti in C.A. viene effettuata secondo la procedura cosiddetta **"Agli stati limite**" Vengono prese in esame le seguenti condizioni: **SLU, SLU(S), SLE(R) , SLE(F), SLE(Q), SLD, SLV, SLC, SLO**

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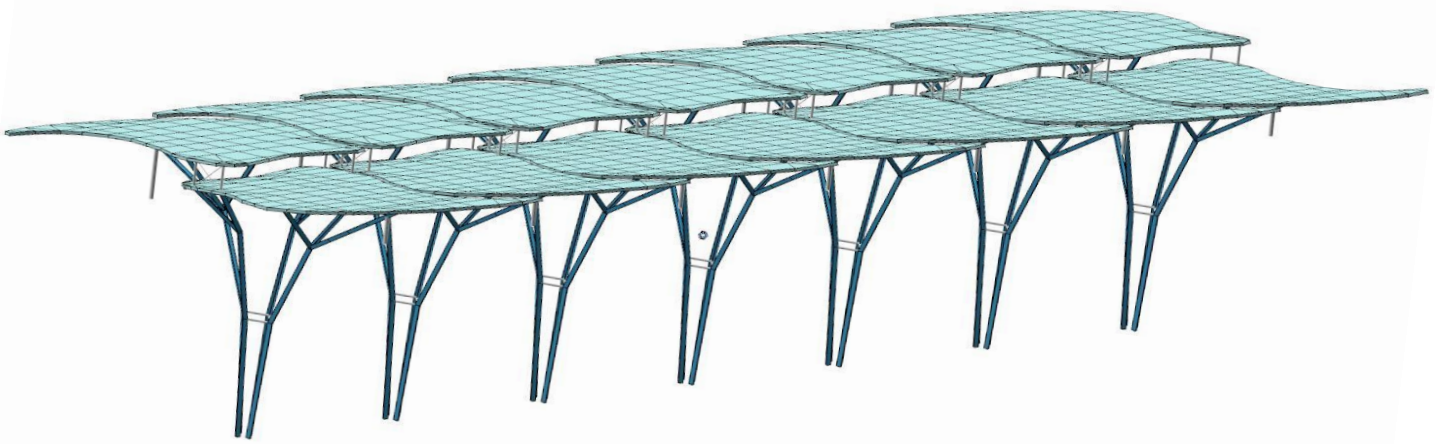

CALCOLO DELLE MEMBRATURE IN ACCIAIO E DELLE LASTRE IN C.A.
TABULATI NUMERICI (Codice di elaborazione: "MODEST, vers. 8.2).

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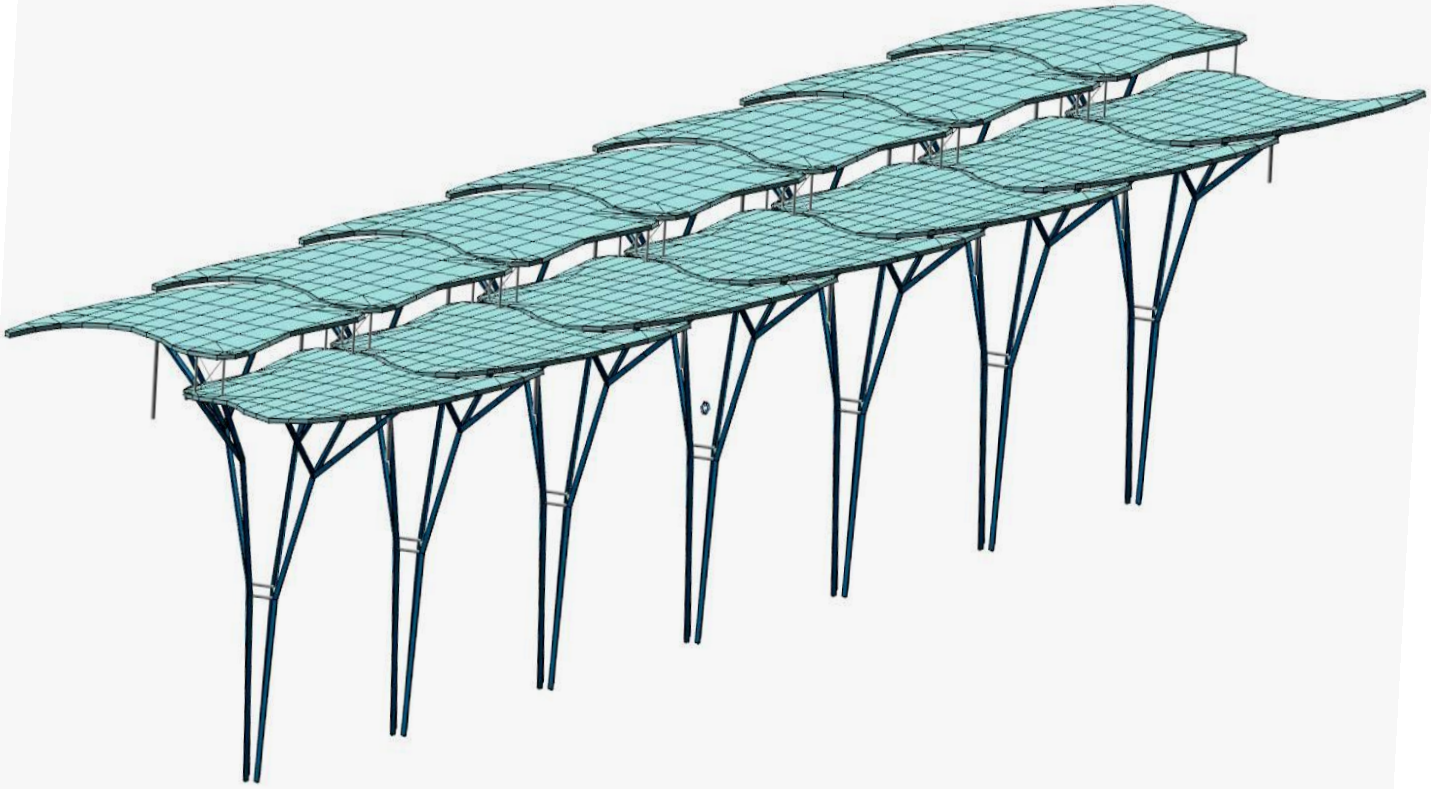
OGGETTO: **Analisi statica dei telai in carpenteria d' acciaio che sostengono la copertura del grande atrio centrale del museo.**
Le strutture reticolari simulano con notevole ricercatezza formale una serie di "alberature" disposte in filare. Questo elemento, costituisce l' aspetto più caratterizzante per una costruzione pratica-mente ipogea, La mancanza di prospetti esterni riversa la vita dell' edificio verso l' atrio interno dal quale giunge la luce naturale proveniente dall' alto. Le alberature sono inserite entro il volume pluripiano dell' atrio stesso



CALCOLO DELLE MEMBRATURE IN ACCIAIO E DELLE LASTRE IN C.A.
TABULATI NUMERICI (Codice di elaborazione: "MODEST, vers. 8.2).

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PARTE SECONDA

VERIFICA DELLE MEMBRATURE IN ACCIAIO.

(C.4.4) TABULATI NUMERICI (Codice di elaborazione: "MODEST, vers. 8.2).

(VEDI INTESTAZIONE GIA' INVIATA)

Criteri di progetto utilizzati

Sezioni generiche

Generali

Stampe
Tipo di relazione Estesa

10

Specifici

Materiali

Calcestruzzo	
-Tipo di calcestruzzo	C28/35
-Rck calcestruzzo <daN/cmq>	350.00
-Modulo elastico <daN/cmq>	325881.00
-Resistenza caratteristica cilindrica (Fck) <daN/cmq>	290.50
-Resistenza caratteristica a trazione (Fctk) <daN/cmq>	19.84
-Riduci Fcd per tutte le verifiche secondo il D.M. 08	Si
-γ_c per stati limite ultimi	
-Automatico	x
-Pari a	
-σ amm. calcestruzzo <daN/cmq>	110.00
-$\tau c0$ <daN/cmq>	6.70
-$\tau c1$ <daN/cmq>	19.70

Acciaio	
-D.M. 92/96	
-Tipo di acciaio (Fe B 22÷44 k)	44
-Modulo elastico <daN/cmq>	2.06E+006
-Tensione caratteristica di snervamento (Fyk) <daN/cmq>	4300.00
-Sigma amm. acciaio <daN/cmq>	2600.00
-Sigma amm. reti e tralicci <daN/cmq>	2600.00
-D.M. 08	
-Tipo di acciaio (B450A÷B450C)	B450C
-Modulo elastico <daN/cmq>	2.06E+006
-Tensione caratteristica di snervamento (Fyk) <daN/cmq>	4500.00
-γ_s per stati limite ultimi	
-Automatico	x
-Pari a	
Coeff. di omogeneizzazione	15.00

Materiali per edifici esistenti

-Considera come elemento nuovo	No
-Calcestruzzo	
-Livello di conoscenza	LC2
-Fattore di confidenza	1.20
-Tipo di calcestruzzo	C25/30
-Rck calcestruzzo	300.00
-Modulo elastico	314472.00
-Resistenza media (Fcm) <daN/cmq>	249.00
-Resistenza media a trazione (Fctm) <daN/cmq>	17.91
-Resistenza caratteristica cilindrica (Fck)	249.00
-Resistenza caratteristica a trazione (Fctk)	17.91
-Acciaio	
-Livello di conoscenza	LC2
-Fattore di confidenza	1.20
-Tipo di acciaio	44
-Modulo elastico	2060000.00
-Tensione media di snervamento (Fym)	4300.00
-Tensione caratteristica di snervamento (Fyk) <daN/cmq>	4300.00
-Allungamento (Agt) <%>	4.00
-Coeff. di omogeneizzazione	15.00

Parametri per analisi pushover

Numero fibre	200.00
Fattore di confinamento nucleo interno	1.00
Fattore di incrudimento acciaio <%>	0.10

Posizione barre e normativa

Copriferro reale al bordo staffa <cm>	2.50
Diametro staffa teorica <mm>	8.00
Distanza fra ferri su più strati <cm>	1.00
Verifica con barre in posizione teorica	Si
-Copriferro <cm>	3.00
Normativa di riferimento	No
-Relativa alle travi	
-Relativa ai pilastri	
-Relativa solo al controllo sulle tensioni	
Verifiche secondo Circ. 65 del 10/04/97	No

Verifiche e sollecitazioni

Passo di verifica <m>	0.50
Integrare lo scorrimento lungo il tratto	Si
-Lunghezza del tratto <m>	1.00
Verifiche a pressoflessione	Si
Verifiche a flessione/pressoflessione retta	No
-Considera My	
-Considera Mz	
Verifiche di stabilità in direzione Z locale	No
-Coeff. ωb	
Integrare lo scorrimento lungo il tratto	No
-Coeff. β	
Tipo verifica di stabilità	
-Per N*ω-M e per N-c*M (standard)	Si
-Per N*ω-c*M (doppia)	No
-Per N*ω (sforzo normale e momento nullo)	No
-Per c*M (momento e sforzo normale nullo)	No

Verifiche a taglio

Modalità di calcolo Vrdu	
-Considera Vrdu minimo	x
-Considera Vrdu calcolato in corrispondenza di bw minimo	

-Considera Vrdu in corrispondenza di bw medio
-Considera Vrdu in corrispondenza di bw massimo
-Considera sempre Af Staffe non proiettata in direzione del taglio No

Dati per progettazione agli stati limite
Gruppo di esigenza
-Ambiente poco aggressivo x
-Ambiente moderatamente aggressivo
-Ambiente molto aggressivo
Usa dominio N-M per flessioni rette No
-Ricerca della sicurezza con sforzo normale costante
-Ricerca della sicurezza con eccentricità costante
Controllo rapporto X/D No
Barre da considerare tese per verifiche a taglio
-Solo le barre con deformazione percentuale rispetto
alla barra più tesa non inferiore al <%> 30.00
-Tutte le barre in trazione

Dati per verifiche di resistenza al fuoco
-Tempo di verifica (REI) <minuti> 120.00
Dimensione MESH <cm> 2.00
-Passo di calcolo <secondi> 10.00
-Temperatura ambiente <C°> 20.00
-Coeff. di convezione a temperatura ambiente <W/mq K> 9.00
-Tipo di aggregati SILICEI
Massa volumica a secco <daN/mc> 2300.00
-Umidità iniziale 3.00
-Fattore di interpolazione conducibilità 0.50

Aste in acciaio

Generali

Verifica aste in acciaio
Numero punti interni per controllo Sigma 10.00
Numero CC da considerare di tipo I 99.00
Sigma max amm. senza verifiche di stabilità <%> 2.00
Trascura sisma per verifiche di deformazione alle T.A. No

Stampe
Verifiche da riportare in relazione Tutte

1

Specifici

Verifiche di resistenza e deformabilità
Tipo di acciaio CNR 10011 e altre normative FE510
Tipo di acciaio D.M. 08 per profilati a sezione aperta S355 UNI EN 10025-2
Tipo di acciaio D.M. 08 per profilati a sezione cava S355H UNI EN 10210-1
-Considera come elemento esistente No
-Livello di conoscenza LC1
-Fattore di confidenza 1.35
Considera prescrizioni D.M. 08 relative ai ponti No
Rapporto fra area effettiva e area nominale 1.00
Rapporto fra area netta e area nominale 1.00
Coeff. di forma intorno all'asse Y 1.00
Coeff. di forma intorno all'asse Z 1.00
Valutare la τ per torsione nei punti di spigolo Si
Massimo valore del rapporto tra la luce e la freccia (totale) 500.00
Massimo valore del rapporto tra la luce e la freccia (solo accidentali) 400.00

Verifiche ai sensi D.M. 08
Fai sempre verifiche in campo elastico Si
Usa prescrizioni EC3 quando più dettagliate Si
Effettua verifiche previste nel capitolo 7 No
Verifiche di stabilità laterale per flessione
-Parametri statici di calcolo
-Utilizza classificazione e parametri minimi x
-Riclassifica e rivaluta parametri con sollecitazioni di verifica
-Coeff.
-Valuta in base ai momenti dell'asta x
-Utilizza valore imposto

-Fattore correttivo di distribuzione K_c	0.94
-Snellezza di riferimento $\lambda_{LT,0}$	0.40
-Coeff. β	0.75
Verifiche di stabilità laterale per pressoflessione	
-Considera come molto deformabile a torsione	No
-Fattore correttivo di distribuzione α_{mY}	0.95
-Fattore correttivo di distribuzione α_{mZ}	0.95
-Fattore correttivo di distribuzione α_{mLT}	0.95

Verifiche di stabilità asta

Riduzione lunghezza libera d'inflessione	
-Distanza fra i nodi dell'asta	x
-Distanza ridotta delle zone rigide moltiplicate per il valore	
Verifiche di stabilità globale in dir. Y locale	Si
-Coeff. β intorno all'asse Y	1.00
Verifiche di stabilità globale in dir. Z locale	Si
-Coeff. β intorno all'asse Z	1.00
Tipo di accoppiamento aste composte	
-Separate	
-Calastrellate	
-Imbottite	
-Automatico	x
Calcolo momento medio usando valori assoluti	Si
Interasse calastrelli o imbottiture	
-Distanza pari a <m>	
-Interasse da normativa moltiplicato per il valore	0.80
-Aste rigidamente collegate	
Aste laminate	Si
Verifiche di stabilità laterale	Si
-Coeff. per calcolo interasse ritegni torsionali	1.00
Eseguire anche le verifiche al punto 7.3.2	Si
Carichi sull'estradosso	Si
Numero irrigidimenti orizzontali anima	0.00
Interasse irrigidimenti verticali anima	
-Numero di suddivisioni	
-Distanza non inferiore a <cm>	
-Pari alla lunghezza dell'asta	x
Modalità di calcolo σ cr,id	
-Normativa	
-Massonet	x
-Ballio	

Verifiche di stabilità membratura

Massimo numero aste costituenti unica membratura	1.00
Sforzo normale di verifica	
-Massimo valore fra tutte le aste	x
-Media aritmetica dei valori di tutte le aste	
-Media pesata di tutte le aste	
Contributo eventuali sforzi di trazione	No
Verifica nei piani principali	Si
Incremento snellezza	Si
Verifiche di stabilità globale in dir. Y locale	Si
-Coeff. β calcolato in funzione dello sforzo normale	
-Coeff. β	1.00
Verifiche di stabilità globale in dir. Z locale	Si
-Coeff. β calcolato in funzione dello sforzo normale	
-Coeff. β	1.00

Verifiche aste in acciaio

Simbologia

Sez. = Numero della sezione
Cod. = Codice
Tipo = Tipologia
- 2C = Doppia C lato labbri
- 2Cdx = Doppia C lato costola
- 2I = Doppia I
- 2L = Doppia L lato labbri
- 2Ldx = Doppia L lato costole
- C = C
- Cdx = C destra
- Cir. = Circolare
- Cir.c = Circolare cava
- I = I
- L = L
- Ldx = L destra
- Om. = Omega
- Pg = Pi greco

Pr = Poligono regolare
Prc = Poligono regolare cavo
Pc = Per coordinate
Ia = Inerzie assegnate
R = Rettangolare
Rc = Rettangolare cava
T = T
U = U
Ur = U rovescia
V = V
Vr = V rovescia
Z = Z
Zdx = Z destra
Ts = T stondata
Ls = L stondata
Cs = C stondata
Is = I stondata
Dis. = Disegnata

D	<cm>	= Distanza
Area	<cmq>	= Area
Anet	<cmq>	= Area netta per compressione
Aeff	<cmq>	= Area effettiva per trazione
Jy	<cm4>	= Momento d'inerzia rispetto all'asse Y
Jz	<cm4>	= Momento d'inerzia rispetto all'asse Z
Iy	<cm>	= Raggio giratorio d'inerzia rispetto all'asse Y
Iz	<cm>	= Raggio giratorio d'inerzia rispetto all'asse Z
Wymin	<cmc>	= Modulo di resistenza minimo rispetto all'asse Y
Wzmin	<cmc>	= Modulo di resistenza minimo rispetto all'asse Z
Wy,plas	<cmc>	= Modulo di resistenza plastico intorno all'asse y
Wz,plas	<cmc>	= Modulo di resistenza plastico intorno all'asse z
Atag,y	<cmq>	= Area resistente a taglio in direz y
Atag,z	<cmq>	= Area resistente a taglio in direz y
Jω	<cm6>	= Costante di ingobbamento
CC		= Numero della combinazione delle condizioni di carico elementari
N,Ed	<daN>	= Forza assiale di calcolo
My,Ed	<daNm>	= Momento flettente di calcolo intorno all'asse Y
Mz,Ed	<daNm>	= Momento flettente di calcolo intorno all'asse Z
Nc,Rd	<daN>	= Resistenza a compressione
My,c,Rd	<daNm>	= Resistenza di calcolo a flessione intorno all'asse Y
Mz,c,Rd	<daNm>	= Resistenza di calcolo a flessione intorno all'asse Z
L		= lunghezza dell'asta
αmy, αmz, αLT		= Coefficienti correttivi per il momento flettente
L_{cr}	<m>	= Lunghezza di libera inflessione laterale fra ritegni torsionali
α-imp		= Coefficiente di imperfezione
k_c		= Coeff. di correzione momento flettente per stabiiltà laterale membrature inflesse
ψ		= Coeff. di correzione momento critico per stabilità laterale membrature inflesse
M,cr	<daNm>	= Momento critico per instabilità flesso torsionale
λ_{LT}		= Coefficiente di imperfezione per stabilità laterale membrature inflesse
$\lambda_{LT,0}$		= Coefficiente di imperfezione di confronto per stabilità laterale membrature inflesse
β_{LT}		= Coefficiente per calcolo Φ_{LT}
Φ_{LT}		= Coefficiente Φ per stabilità laterale membrature inflesse
f		= Fattore di modifica per il coefficiente di riduzione
χ_{LT}		= Coefficiente di riduzione per stabilità laterale membrature inflesse
λ_y		= Snellezza per inflessione intorno all'asse y(c)
Ncr,y	<daN>	= Sforzo normale critico euleriano per inflessione intorno all'asse y(c)
λ^*_y		= Snellezza adimensionale per inflessione intorno all'asse y(c)
Curva		= Curva di instabilità adottata
Φ_y		= Coefficiente Φ per inflessione intorno all'asse y(c)
χ_y		= Coefficiente χ di riduzione per instabilità intorno all'asse y(c)
λ_z		= Snellezza per inflessione intorno all'asse z(e)
Ncr,z	<daN>	= Sforzo normale critico euleriano per inflessione intorno all'asse z(e)
λ^*_z		= Snellezza adimensionale per inflessione intorno all'asse z(e)
Φ_z		= Coefficiente Φ per inflessione intorno all'asse z(e)
χ_z		= Coefficiente χ di riduzione per instabilità intorno all'asse z(e)
Kyy, Kyz, Kzy, Kzz		= Coefficienti di interazione
Xl	<m>	= Coordinata progressiva (dal nodo iniziale dell'asta) in cui viene effettuato il progetto/verifica
N	<daN>	= Sforzo normale
Tz	<daN>	= Taglio in dir. Z
My	<daNm>	= Momento flettente intorno all'asse Y
Ty	<daN>	= Taglio in dir. Y
Mz	<daNm>	= Momento flettente intorno all'asse Z
σ_N	<daN/cmq>	= Tensione normale per sforzo normale
σ_M	<daN/cmq>	= Tensione normale per momento flettente
τ	<daN/cmq>	= Tensione tangenziale per taglio e/o torsione
Mx	<daNm>	= Momento torcente intorno all'asse X
λ		= Snellezza per inflessione
Ncr	<daN>	= Sforzo normale critico euleriano
λ^*		= Snellezza adimensionale
Φ		= Coefficiente Φ
χ,min		= Coefficiente χ di riduzione per instabilità
Nb,Rd	<daN>	= Resistenza all'instabilità
M,Ed	<daNm>	= Momento flettente di calcolo
M	<daNm>	= Momento agente
My,b,Rd	<daNm>	= Resistenza di calcolo a flessione ridotta per stabilità laterale membrature inflesse
T	<daN>	= Taglio agente
$f_{z,L}$	<cm>	= Freccia in direzione Z locale
$f_{z,G}$	<cm>	= Freccia in direzione Z globale

Caratteristiche profilati utilizzati

Sez.	Cod.	Tipo	D <cm>	Area <cmq>	Anet <cmq>	Aeff <cmq>	Jy <cm4>	Jz <cm4>	Iy <cm>	Iz <cm>	Wymin <cmc>	Wzmin <cmc>
2	Cir.c D=120/6	Cir.c	--	21.49	21.49	21.49	350.05	350.05	4.04	4.04	58.34	58.34
4	Cir. D=4	Cir.	--	12.57	12.57	12.57	12.57	12.57	1.00	1.00	6.28	6.28
6	Is 175x250x18x12x0x0x10000	Is	--	85.09	85.09	85.09	4349.74	2318.00	7.15	5.22	497.11	185.44
8	Is 146x215x13x10x0x0x10000	Is	--	58.07	58.07	58.07	2134.48	1213.37	6.06	4.57	292.39	112.87

Caratteristiche profilati utilizzati

Sez.	Cod.	Wy,plas <cmc>	Wz,plas <cmc>	Atag,y <cmq>	Atag,z <cmq>	Jω <cm6>
2	Cir.c D=120/6	76.14	76.14	13.68	13.68	
4	Cir. D=4	10.41	10.41	8.00	8.00	
6	Is 175x250x18x12x0x0x10000	573.19	321.21	57.91	27.25	207570.00
8	Is 146x215x13x10x0x0x10000	333.99	194.62	41.69	16.37	76591.70

Asta n. 1 (7 8) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-6827.64 My,Ed=-37.47 Mz,Ed=3461.35
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=700.73
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.01 Curva b: α-imp=0.34 k_c=0.94 ψ=1.71 M,cr=39722.80 λ_{LT}=0.67
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.71 β_{LT}=0.75 f=0.97 χ_{LT}=0.91
  λ_Y=98.01 Ncr,y=183603.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.44
  λ_Z=134.26 Ncr,z=97842.80 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 0.98, 1.01, 0.78, 1.01
  Verifica YY: 0.05 + 0.00 + 0.56 = 0.61
  Verifica ZZ: 0.10 + 0.00 + 0.56 = 0.65

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/96680) $f_{Z,L}$=0.00 (L/386720)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.04 (L/16891) $f_{Z,L}$=0.01 (L/66797)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.01 - Classe 3
  Sollecitazioni: N=-6219.78 T_z=-5.15 M_y=-1.41 T_y=860.68 M_z=3461.35
  Tensioni: σ_N=-73.09 σ_M=-1866.85 τ=0.00 σ_{max}=-1939.94
  Tensioni: σ_N=-73.09 σ_M=134.62 τ=16.43 τ_{max}=16.43
  Tensioni: σ_N=-73.09 σ_M=-1866.85 τ=0.00 $\sigma_{ID,max}$=1939.94

Asta n. 2 (1 2) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-19167.50 My,Ed=-514.38 Mz,Ed=-1799.67
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=702.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.02 Curva b: α-imp=0.34 k_c=0.94 ψ=1.58 M,cr=36520.40 λ_{LT}=0.70
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.73 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
  λ_Y=98.21 Ncr,y=182868.00 λ^*_y=1.29 Curva b: Φ_y=1.51 χ_y=0.43
  λ_Z=134.53 Ncr,z=97451.20 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 1.04, 1.11, 0.83, 1.11
  Verifica YY: 0.15 + 0.04 + 0.32 = 0.51
  Verifica ZZ: 0.27 + 0.03 + 0.32 = 0.62

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.02 (L/35227) $f_{Z,G}$=0.01 (L/76692)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.11 (L/6218) $f_{Z,G}$=0.05 (L/13100)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.02 - Classe 3
  Sollecitazioni: N=-18559.60 T_z=-85.99 M_y=89.39 T_y=-487.33 M_z=-1799.67 M_x=6.87
  Tensioni: σ_N=-218.11 σ_M=-988.47 τ=6.89 σ_{max}=-1206.58
  Tensioni: σ_N=-218.11 σ_M=-84.29 τ=25.95 τ_{max}=25.95
  Tensioni: σ_N=-218.11 σ_M=-988.47 τ=6.89 $\sigma_{ID,max}$=1206.64

Asta n. 4 (3 4) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-19824.60 My,Ed=-257.43 Mz,Ed=-2027.39
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=702.06
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.02 Curva b: α-imp=0.34 k_c=0.94 ψ=1.56 M,cr=36040.40 λ_{LT}=0.70
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.73 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
  λ_Y=98.19 Ncr,y=182908.00 λ^*_y=1.29 Curva b: Φ_y=1.51 χ_y=0.43
  λ_Z=134.51 Ncr,z=97472.40 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 1.04, 1.11, 0.83, 1.11
  Verifica YY: 0.16 + 0.02 + 0.36 = 0.54
  Verifica ZZ: 0.28 + 0.01 + 0.36 = 0.66

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.01 (L/73616)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.06 (L/12670)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.02 - Classe 3
  Sollecitazioni: N=-19216.80 T_z=-43.86 M_y=50.47 T_y=-548.83 M_z=-2027.39 M_x=3.00
  Tensioni: σ_N=-225.84 σ_M=-1103.44 τ=3.00 σ_{max}=-1329.28
  Tensioni: σ_N=-225.84 σ_M=-86.86 τ=15.02 τ_{max}=15.02
  Tensioni: σ_N=-225.84 σ_M=-1103.44 τ=3.00 $\sigma_{ID,max}$=1329.29

Asta n. 5 (-11 -4) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/25614)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.07 (L/4647)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-13011.20
  N,Ed=-13011.20 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.18

- Verifica di stabilità (4.2.4.1.3.1) - CC 25
  Sollecitazioni: N=-13011.20 L=320.00
  λ=79.28 Ncr=70851.00 λ^*=1.04
  Curva a: Φ=1.13 χ,min=0.64 N,Ed=-13011.20 Nb,Rd=46443.40 N,Ed/Nb,Rd=0.28

Asta n. 6 (-9 -8) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/22671)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.04 (L/4122)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-14781.80
  N,Ed=-14781.80 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.20

- Verifica di stabilità (4.2.4.1.3.1) - CC 25
  Sollecitazioni: N=-14781.80 L=160.00
  λ=39.64 Ncr=283404.00 λ^*=0.52
  Curva a: Φ=0.67 χ,min=0.92 N,Ed=-14781.80 Nb,Rd=66718.00 N,Ed/Nb,Rd=0.22

Asta n. 7 (17 76) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.00 (L/33764)

- Verifica a compressione (4.2.10) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-2172.05
  N,Ed=-2172.05 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.03

Asta n. 8 (18 72) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/120586)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/22213)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-2739.31
  N,Ed=-2739.31 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.04

Asta n. 9 (72 17) Cir. D=4 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-1838.41 M,Ed=4.05
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=259.36
  λ=259.36 Ncr=3872.04 λ^*=3.39 Curva c: Φ=7.04 χ,min=0.08
  χ,min=0.08
  Verifica: 0.57 + 0.04 = 0.61

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/226627)

- Verifica Freccia massima carichi totali - CC 26

$f_{Z,L}$=0.14 (L/1814) $f_{Z,G}$=0.09 (L/2877)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.30 - Classe 3
  Sollecitazioni: N=-1828.70 M=5.39
  Tensioni: σ_N=-145.52 σ_M=-85.86 τ=0.00 σ_{max}=-231.38
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-145.52 σ_M=-85.86 τ=0.00 $\sigma_{ID,max}$=231.38

Asta n. 10 (76 18) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 25 - Classe 3
  L_{cr}=2.10 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
  $\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
  CC 25 My,Ed=-5.68 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.08 (L/2765) $f_{Z,G}$=0.06 (L/3371)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.05 - Classe 3
  Sollecitazioni: N=2195.28 M=4.37
  Tensioni: σ_N=174.69 σ_M=69.51 τ=0.00 σ_{max}=244.20
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=174.69 σ_M=69.51 τ=0.00 $\sigma_{ID,max}$=244.20

Asta n. 11 (14 63) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/120586)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/24117)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.61 - Classe 3
  Sollecitazioni: N=5627.62
  Tensioni: σ_N=261.89 σ_M=0.00 τ=0.00 σ_{max}=261.89
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=261.89 σ_M=0.00 τ=0.00 $\sigma_{ID,max}$=261.89

Asta n. 12 (15 64) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-6504.46 M,Ed=0.00
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=161.00
  αmy, αmz, αLT = 0.95, ----, ----
  λ=39.89 Ncr=279894.00 λ^*=0.52
  Curva a: Φ=0.67 χ,min=0.92
  Kyy, Kyz, Kzy, Kzz = 0.98, ----, ----, ----
  Verifica: 0.09 = 0.09

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/93789)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/16551)

- Verifica a compressione (4.2.10) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-6504.46
  N,Ed=-6504.46 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.09

Asta n. 13 (14 64) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 3
  L_{cr}=2.59 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
  $\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
  CC 19 My,Ed=-5.39 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 1 - Classe 3
  Sollecitazioni: N,Ed=-3511.22 M,Ed=4.05
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=259.36
  λ=259.36 Ncr=3872.04 λ^*=3.39 Curva c: Φ=7.04 χ,min=0.08
  χ,min=0.08
  Verifica: 1.09 + 0.20 = 1.30

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.14 (L/1816) $f_{Z,G}$=0.10 (L/2724)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.30 - Classe 3
  Sollecitazioni: N=-5181.39 M=5.39
  Tensioni: σ_N=-412.32 σ_M=-85.86 τ=0.00 σ_{max}=-498.18
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-412.32 σ_M=-85.86 τ=0.00 $\sigma_{ID,max}$=498.18

Asta n. 14 (15 63) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 25 - Classe 3
  L_{cr}=2.10 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
  $\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
  CC 25 My,Ed=-5.68 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 23 - Classe 3
  Sollecitazioni: N,Ed=-1867.25 M,Ed=3.28
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=209.96
  λ=209.96 Ncr=5908.50 λ^*=2.75 Curva c: Φ=4.90 χ,min=0.11
  χ,min=0.11
  Verifica: 0.39 + 0.02 = 0.42

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.08 (L/2765) $f_{Z,G}$=0.06 (L/3522)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.05 - Classe 3
  Sollecitazioni: N=7488.33 M=4.37
  Tensioni: σ_N=595.90 σ_M=69.51 τ=0.00 σ_{max}=665.41
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=595.90 σ_M=69.51 τ=0.00 $\sigma_{ID,max}$=665.41

Asta n. 15 (8 4) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2362.31 M,Ed=2.86
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=102.22
  αmy, αmz, αLT = 0.95, ----, ----
  λ=25.33 Ncr=694405.00 λ^*=0.33
  Curva a: Φ=0.57 χ,min=0.97
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.03 + 0.00 = 0.03

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.51 - Classe 3
  Sollecitazioni: N=-2362.31 M=2.86
  Tensioni: σ_N=-109.93 σ_M=-4.91 τ=0.00 σ_{max}=-114.84
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-109.93 σ_M=-4.91 τ=0.00 $\sigma_{ID,max}$=114.84

Asta n. 16 (4 6) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2803.79 M,Ed=4.01
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=120.97
  αmy, αmz, αLT = 0.95, ----, ----
  λ=29.97 Ncr=495807.00 λ^*=0.39
  Curva a: Φ=0.60 χ,min=0.95
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.60 - Classe 3
  Sollecitazioni: N=-2803.79 M=4.01
  Tensioni: σ_N=-130.48 σ_M=-6.88 τ=0.00 σ_{max}=-137.35
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-130.48 σ_M=-6.88 τ=0.00 $\sigma_{ID,max}$=137.35

Asta n. 17 (6 2) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2377.55 M,Ed=2.89
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=102.73
  αmy, αmz, αLT = 0.95, ----, ----
  λ=25.45 Ncr=687496.00 λ^*=0.33
  Curva a: Φ=0.57 χ,min=0.97
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.03 + 0.00 = 0.03

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.51 - Classe 3

Sollecitazioni: N=-2377.55 M=2.89
Tensioni: σ_N=-110.64 σ_M=-4.96 τ=0.00 σ_{max}=-115.60
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=-110.64 σ_M=-4.96 τ=0.00 $\sigma_{ID,max}$=115.60

Asta n. 18 (2 8) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-2710.76 M,Ed=3.97
Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=120.28
αmy, αmz, αLT = 0.95, ----, ----
λ=29.80 Ncr=501461.00 λ^*=0.39
Curva a: Φ=0.60 χ,min=0.96
Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.60 - Classe 3
Sollecitazioni: N=-2710.76 M=3.97
Tensioni: σ_N=-126.15 σ_M=-6.80 τ=0.00 σ_{max}=-132.95
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=-126.15 σ_M=-6.80 τ=0.00 $\sigma_{ID,max}$=132.95

Asta n. 101 (8 16) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-5971.14 My,Ed=372.24 Mz,Ed=-4472.91
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=526.58
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=5.27 Curva b: α-imp=0.34 k_c=0.94 ψ=1.50 M,cr=49048.90 λ_{LT}=0.60
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.67 β_{LT}=0.75 f=0.97 χ_{LT}=0.94
λ_Y=73.65 Ncr,y=325125.00 λ^*_y=0.96 Curva b: Φ_y=1.09 χ_y=0.62
λ_Z=100.89 Ncr,z=173260.00 λ^*_z=1.32 Curva c: Φ_z=1.65 χ_z=0.38
Kyy, Kyz, Kzy, Kzz = 0.97, 0.98, 0.77, 0.98
Verifica YY: 0.02 + 0.02 + 0.70 = 0.74
Verifica ZZ: 0.02 + 0.02 + 0.70 = 0.74

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/48863) $f_{Z,L}$=0.01 (L/70789)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.07 (L/7401) $f_{Z,L}$=0.04 (L/12492)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=5.27 - Classe 3
Sollecitazioni: N=-5623.79 T_z=-85.86 M_y=372.24 T_y=-1385.91 M_z=-4472.91 M_x=-6.56
Tensioni: σ_N=-66.09 σ_M=-2486.94 τ=6.58 σ_{max}=-2553.03
Tensioni: σ_N=-66.09 σ_M=-113.64 τ=35.21 τ_{max}=35.21
Tensioni: σ_N=-66.09 σ_M=-2486.94 τ=6.58 $\sigma_{ID,max}$=2553.05

Asta n. 102 (2 19) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-19378.60 My,Ed=-182.39 Mz,Ed=-1800.72
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=553.99
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=5.54 Curva b: α-imp=0.34 k_c=0.94 ψ=1.42 M,cr=43508.90 λ_{LT}=0.64
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.69 β_{LT}=0.75 f=0.97 χ_{LT}=0.93
λ_Y=77.48 Ncr,y=293755.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
λ_Z=106.14 Ncr,z=156543.00 λ^*_z=1.39 Curva c: Φ_z=1.76 χ_z=0.35
Kyy, Kyz, Kzy, Kzz = 1.02, 1.06, 0.81, 1.06
Verifica YY: 0.11 + 0.01 + 0.30 = 0.43
Verifica ZZ: 0.19 + 0.01 + 0.30 = 0.50

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.02 (L/36765) $f_{Z,L}$=0.00 (L/165970)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.09 (L/6447) $f_{Z,L}$=0.02 (L/27927)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=5.54 - Classe 3
Sollecitazioni: N=-18927.10 T_z=44.59 M_y=-182.39 T_y=561.49 M_z=1769.37 M_x=-9.03
Tensioni: σ_N=-222.43 σ_M=-990.84 τ=9.05 σ_{max}=-1213.27
Tensioni: σ_N=-222.43 σ_M=98.11 τ=31.59 τ_{max}=31.59
Tensioni: σ_N=-222.43 σ_M=-990.84 τ=9.05 $\sigma_{ID,max}$=1213.37

Asta n. 103 (6 13) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-6948.24 My,Ed=112.59 Mz,Ed=-4840.37
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=526.43
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.26 Curva b: α-imp=0.34 k_c=0.94 ψ=1.49 M,cr=48777.90 λ_{LT}=0.60
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.67 β_{LT}=0.75 f=0.97 χ_{LT}=0.94
  λ_Y=73.63 Ncr,y=325318.00 λ^*_y=0.96 Curva b: Φ_y=1.09 χ_y=0.62
  λ_Z=100.86 Ncr,z=173363.00 λ^*_z=1.32 Curva c: Φ_z=1.65 χ_z=0.38
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
  Verifica YY: 0.04 + 0.01 + 0.76 = 0.81
  Verifica ZZ: 0.06 + 0.01 + 0.76 = 0.83

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/39712) $f_{Z,L}$=0.00 (L/250907)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.09 (L/6153) $f_{Z,L}$=0.01 (L/36556)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=5.26 - Classe 3
  Sollecitazioni: N=-6496.69 T_z=-27.13 M_y=112.59 T_y=-1619.68 M_z=-4840.37 M_x=4.26
  Tensioni: σ_N=-76.35 σ_M=-2632.86 τ=4.27 σ_{max}=-2709.21
  Tensioni: σ_N=-76.35 σ_M=-206.09 τ=35.19 τ_{max}=35.19
  Tensioni: σ_N=-76.35 σ_M=-2632.86 τ=4.27 $\sigma_{ID,max}$=2709.22

Asta n. 104 (4 9) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-20045.50 My,Ed=72.17 Mz,Ed=-2027.81
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=553.99
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.54 Curva b: α-imp=0.34 k_c=0.94 ψ=1.38 M,cr=42311.20 λ_{LT}=0.65
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.70 β_{LT}=0.75 f=0.97 χ_{LT}=0.92
  λ_Y=77.48 Ncr,y=293755.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
  λ_Z=106.14 Ncr,z=156543.00 λ^*_z=1.39 Curva c: Φ_z=1.76 χ_z=0.35
  Kyy, Kyz, Kzy, Kzz = 1.02, 1.06, 0.81, 1.06
  Verifica YY: 0.12 + 0.00 + 0.34 = 0.47
  Verifica ZZ: 0.20 + 0.00 + 0.34 = 0.54

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.02 (L/34170) $f_{Z,L}$=0.00 (L/176029)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.09 (L/6069) $f_{Z,L}$=0.02 (L/34372)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-20045.50 T_z=-7.79 M_y=29.00 T_y=806.47 M_z=-2027.81 M_x=-3.35
  Tensioni: σ_N=-235.57 σ_M=-1099.35 τ=3.36 σ_{max}=-1334.92
  Tensioni: σ_N=-235.57 σ_M=-74.06 τ=18.78 τ_{max}=18.78
  Tensioni: σ_N=-235.57 σ_M=-1099.35 τ=3.36 $\sigma_{ID,max}$=1334.94

Asta n. 105 (-4 37) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-11458.00 M,Ed=0.12
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=78.22
  αmy, αmz, αLT = 0.95, ----, ----
  λ=19.38 Ncr=1185880.00 λ^*=0.25
  Curva a: Φ=0.54 χ,min=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
  Verifica: 0.16 + 0.00 = 0.16

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/29291)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/5291)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-11458.00
  N,Ed=-11458.00 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.16

Asta n. 106 (-8 126) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-11719.80 M,Ed=0.29

Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=66.17
αmy, αmz, αLT = 0.95, ----, ----
λ=16.39 Ncr=1657040.00 λ^*=0.21
Curva a: Φ=0.52 χ,min=1.00
Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
Verifica: 0.16 + 0.00 = 0.16

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/28909)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.01 (L/5506)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-11719.80 T=1.76
N,Ed=-11719.80 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.16

Asta n. 211 (16 18) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3127.14 My,Ed=1131.67 Mz,Ed=-1883.23
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=379.60
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.80 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=39930.60 λ_{LT}=0.51
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.62 β_{LT}=0.75 f=0.98 χ_{LT}=0.98
λ_y=62.61 Ncr,y=307021.00 λ^*_y=0.82 Curva b: Φ_y=0.94 χ_y=0.71
λ_z=83.04 Ncr,z=174529.00 λ^*_z=1.09 Curva c: Φ_z=1.31 χ_z=0.49
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.11 + 0.48 = 0.61
Verifica ZZ: 0.02 + 0.09 + 0.48 = 0.58

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.05 (L/7057) $f_{Z,L}$=0.03 (L/12247)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.30 (L/1265) $f_{Z,L}$=0.18 (L/2166)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3127.14 T_z=298.13 M_y=1131.67 T_y=565.78 M_z=-1883.23
Tensioni: σ_N=-53.85 σ_M=-2055.51 τ=0.00 σ_{max}=-2109.36
Tensioni: σ_N=-53.85 σ_M=-409.85 τ=21.56 τ_{max}=21.56
Tensioni: σ_N=-53.85 σ_M=-2055.51 τ=0.00 $\sigma_{ID,max}$=2109.36

Asta n. 212 (16 17) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-3059.04 My,Ed=-1060.67 Mz,Ed=-2296.02
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=334.12
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.34 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=47739.80 λ_{LT}=0.47
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.59 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=55.11 Ncr,y=396295.00 λ^*_y=0.72 Curva b: Φ_y=0.85 χ_y=0.77
λ_z=73.09 Ncr,z=225278.00 λ^*_z=0.96 Curva c: Φ_z=1.14 χ_z=0.57
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.10 + 0.58 = 0.70
Verifica ZZ: 0.02 + 0.08 + 0.58 = 0.68

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.05 (L/6776) $f_{Z,L}$=0.02 (L/14845)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.28 (L/1201) $f_{Z,L}$=0.13 (L/2634)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-3059.04 T_z=-317.46 M_y=-1060.67 T_y=734.45 M_z=-2296.02
Tensioni: σ_N=-52.68 σ_M=-2396.95 τ=0.00 σ_{max}=-2449.63
Tensioni: σ_N=-52.68 σ_M=166.58 τ=25.49 τ_{max}=25.49
Tensioni: σ_N=-52.68 σ_M=-2396.95 τ=0.00 $\sigma_{ID,max}$=2449.63

Asta n. 212 (19 21) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-11140.30 My,Ed=604.44 Mz,Ed=220.54
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=437.01
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.37 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=33075.30 λ_{LT}=0.56

$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_Y=72.08 Ncr,y=231652.00 λ^*_y=0.94 Curva b: Φ_y=1.07 χ_y=0.63
λ_Z=95.60 Ncr,z=131685.00 λ^*_z=1.25 Curva c: Φ_z=1.54 χ_z=0.41
Kyy, Kyz, Kzy, Kzz = 1.00, 1.03, 0.80, 1.03
Verifica YY: 0.09 + 0.06 + 0.06 = 0.21
Verifica ZZ: 0.14 + 0.05 + 0.06 = 0.25

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.02 (L/21614) $f_{Z,G}$=0.01 (L/37254)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.12 (L/3496) $f_{Z,G}$=0.08 (L/5636)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-8930.45 T_z=121.72 M_y=531.91 T_y=63.85 M_z=284.34
Tensioni: σ_N=-153.80 σ_M=-433.83 τ=0.00 σ_{max}=-587.63
Tensioni: σ_N=-153.80 σ_M=15.23 τ=7.33 τ_{max}=7.33
Tensioni: σ_N=-153.80 σ_M=-433.83 τ=0.00 $\sigma_{ID,max}$=587.63

Asta n. 213 (13 14) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3154.92 My,Ed=1042.29 Mz,Ed=-2037.92
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=352.04
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.52 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=44330.50 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=58.06 Ncr,y=356964.00 λ^*_y=0.76 Curva b: Φ_y=0.88 χ_y=0.75
λ_Z=77.01 Ncr,z=202920.00 λ^*_z=1.01 Curva c: Φ_z=1.21 χ_z=0.54
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.10 + 0.52 = 0.63
Verifica ZZ: 0.02 + 0.08 + 0.52 = 0.61

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.05 (L/6476) $f_{Z,L}$=0.02 (L/14197)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.31 (L/1152) $f_{Z,L}$=0.14 (L/2554)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3154.92 T_z=296.07 M_y=1042.29 T_y=648.55 M_z=-2037.92
Tensioni: σ_N=-54.33 σ_M=-2161.99 τ=0.00 σ_{max}=-2216.33
Tensioni: σ_N=-54.33 σ_M=-393.74 τ=23.06 τ_{max}=23.06
Tensioni: σ_N=-54.33 σ_M=-2161.99 τ=0.00 $\sigma_{ID,max}$=2216.33

Asta n. 214 (9 11) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-7599.58 My,Ed=-858.04 Mz,Ed=-251.54
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=448.31
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.48 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=31994.10 λ_{LT}=0.57
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.65 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_Y=73.94 Ncr,y=220115.00 λ^*_y=0.97 Curva b: Φ_y=1.10 χ_y=0.62
λ_Z=98.07 Ncr,z=125127.00 λ^*_z=1.28 Curva c: Φ_z=1.59 χ_z=0.40
Kyy, Kyz, Kzy, Kzz = 0.98, 1.01, 0.79, 1.01
Verifica YY: 0.06 + 0.09 + 0.07 = 0.22
Verifica ZZ: 0.10 + 0.07 + 0.07 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.03 (L/12879) $f_{Z,G}$=0.00 (L/130580)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.21 (L/2149) $f_{Z,G}$=0.02 (L/21175)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-7599.58 T_z=-191.39 M_y=-858.04 T_y=118.80 M_z=-251.54
Tensioni: σ_N=-130.88 σ_M=-516.30 τ=0.00 σ_{max}=-647.18
Tensioni: σ_N=-130.88 σ_M=-13.47 τ=11.54 τ_{max}=11.54
Tensioni: σ_N=-130.88 σ_M=-516.30 τ=0.00 $\sigma_{ID,max}$=647.18

Asta n. 222 (19 20) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-9184.28 My,Ed=-670.49 Mz,Ed=-171.95
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=458.65

αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.59 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=31066.50 λ_{LT}=0.58
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
λ_Y=75.65 Ncr,y=210307.00 λ^*_y=0.99 Curva b: Φ_y=1.12 χ_y=0.60
λ_Z=100.33 Ncr,z=119551.00 λ^*_z=1.31 Curva c: Φ_z=1.63 χ_z=0.38
Kyy, Kyz, Kzy, Kzz = 0.99, 1.02, 0.80, 1.02
Verifica YY: 0.08 + 0.07 + 0.05 = 0.19
Verifica ZZ: 0.12 + 0.06 + 0.05 = 0.22

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.02 (L/18373) $f_{Z,G}$=0.00 (L/123314)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.15 (L/3011) $f_{Z,G}$=0.02 (L/22578)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-7442.59 T_z=-130.26 M_y=-597.45 T_y=118.84 M_z=-257.50
Tensioni: σ_N=-128.17 σ_M=-432.46 τ=0.00 σ_{max}=-560.64
Tensioni: σ_N=-128.17 σ_M=-13.79 τ=7.86 τ_{max}=7.86
Tensioni: σ_N=-128.17 σ_M=-432.46 τ=0.00 $\sigma_{ID,max}$=560.64

Asta n. 223 (13 15) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3604.54 My,Ed=-1180.87 Mz,Ed=-2479.09
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=363.03
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.63 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=42465.80 λ_{LT}=0.49
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.61 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=59.88 Ncr,y=335675.00 λ^*_y=0.78 Curva b: Φ_y=0.91 χ_y=0.73
λ_Z=79.42 Ncr,z=190818.00 λ^*_z=1.04 Curva c: Φ_z=1.25 χ_z=0.52
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.12 + 0.63 = 0.77
Verifica ZZ: 0.02 + 0.09 + 0.63 = 0.74

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.06 (L/5994) $f_{Z,L}$=0.03 (L/12230)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.34 (L/1063) $f_{Z,L}$=0.17 (L/2162)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3604.54 T_z=-325.28 M_y=-1180.87 T_y=744.32 M_z=-2479.09
Tensioni: σ_N=-62.08 σ_M=-2600.25 τ=0.00 σ_{max}=-2662.33
Tensioni: σ_N=-62.08 σ_M=189.59 τ=25.96 τ_{max}=25.96
Tensioni: σ_N=-62.08 σ_M=-2600.25 τ=0.00 $\sigma_{ID,max}$=2662.33

Asta n. 224 (9 10) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-11178.80 My,Ed=633.69 Mz,Ed=234.45
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=426.15
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.26 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=34185.30 λ_{LT}=0.55
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_Y=70.29 Ncr,y=243609.00 λ^*_y=0.92 Curva b: Φ_y=1.05 χ_y=0.65
λ_Z=93.22 Ncr,z=138482.00 λ^*_z=1.22 Curva c: Φ_z=1.49 χ_z=0.42
Kyy, Kyz, Kzy, Kzz = 1.00, 1.03, 0.80, 1.03
Verifica YY: 0.09 + 0.07 + 0.06 = 0.22
Verifica ZZ: 0.13 + 0.05 + 0.06 = 0.25

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.02 (L/21691) $f_{Z,G}$=0.01 (L/35747)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.12 (L/3418) $f_{Z,G}$=0.08 (L/5429)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-9679.36 T_z=182.14 M_y=776.19 T_y=46.42 M_z=232.30
Tensioni: σ_N=-166.69 σ_M=-471.27 τ=0.00 σ_{max}=-637.96
Tensioni: σ_N=-166.69 σ_M=12.44 τ=10.96 τ_{max}=10.96
Tensioni: σ_N=-166.69 σ_M=-471.27 τ=0.00 $\sigma_{ID,max}$=637.96

Asta n. 232 (-4 22) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-4389.86 My,Ed=-87.21 Mz,Ed=-703.10
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=248865.00 λ_{LT}=0.20
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.01 + 0.18 = 0.21
  Verifica ZZ: 0.02 + 0.01 + 0.18 = 0.21

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/41796)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/6928) $f_{Z,L}$=0.00 (L/76216)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-4389.86 T_z=-70.57 M_y=-87.21 T_y=602.22 M_z=-703.10
  Tensioni: σ_N=-75.60 σ_M=-652.75 τ=0.00 σ_{max}=-728.35
  Tensioni: σ_N=-75.60 σ_M=-13.86 τ=16.30 τ_{max}=16.30
  Tensioni: σ_N=-75.60 σ_M=-652.75 τ=0.00 $\sigma_{ID,max}$=728.35

Asta n. 232 (-3 -4) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3014.06 My,Ed=-87.21 Mz,Ed=-703.10
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.14 M,cr=161582.00 λ_{LT}=0.25
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.01 + 0.18 = 0.20
  Verifica ZZ: 0.02 + 0.01 + 0.18 = 0.20

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/30849)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/5398) $f_{Z,L}$=0.00 (L/49833)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.24 - Classe 3
  Sollecitazioni: N=-2983.25 T_z=18.23 M_y=-87.21 T_y=-415.05 M_z=-703.10
  Tensioni: σ_N=-51.38 σ_M=-652.75 τ=0.00 σ_{max}=-704.12
  Tensioni: σ_N=-51.38 σ_M=-13.86 τ=10.99 τ_{max}=10.99
  Tensioni: σ_N=-51.38 σ_M=-652.75 τ=0.00 $\sigma_{ID,max}$=704.12

Asta n. 232 (-2 -3) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 - Classe 3
  Sollecitazioni: N,Ed=-2360.79 My,Ed=-296.67 Mz,Ed=-167.38
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.10 M,cr=156811.00 λ_{LT}=0.26
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.01 + 0.03 + 0.04 = 0.08
  Verifica ZZ: 0.01 + 0.02 + 0.04 = 0.08

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.00 (L/71982) $f_{Z,G}$=0.00 (L/80980)

- Verifica in termini tensionali (4.2.5) - CC 1 Xl=1.24 - Classe 3
  Sollecitazioni: N=-2337.09 T_z=51.88 M_y=-296.67 T_y=-256.15 M_z=-167.38
  Tensioni: σ_N=-40.25 σ_M=-249.75 τ=0.00 σ_{max}=-290.00
  Tensioni: σ_N=-40.25 σ_M=72.03 τ=7.28 τ_{max}=7.28
  Tensioni: σ_N=-40.25 σ_M=-249.75 τ=0.00 $\sigma_{ID,max}$=290.00

Asta n. 232 (-1 -2) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3075.69 My,Ed=-42.16 Mz,Ed=466.16
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.33 M,cr=188566.00 λ_{LT}=0.23
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.00 + 0.12 = 0.14
  Verifica ZZ: 0.02 + 0.00 + 0.12 = 0.14

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/49833)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/7279) $f_{Z,L}$=0.00 (L/117789)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3075.69 T_z=18.23 M_y=-19.64 T_y=-215.79 M_z=466.16
  Tensioni: σ_N=-52.97 σ_M=-419.71 τ=0.00 σ_{max}=-472.68
  Tensioni: σ_N=-52.97 σ_M=30.33 τ=5.77 τ_{max}=5.77
  Tensioni: σ_N=-52.97 σ_M=-419.71 τ=0.00 $\sigma_{ID,max}$=472.68

Asta n. 232 (19 -1) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3106.50 My,Ed=-19.64 Mz,Ed=691.76
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.60 M,cr=227877.00 λ_{LT}=0.21
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.00 + 0.17 = 0.19
  Verifica ZZ: 0.02 + 0.00 + 0.17 = 0.19

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/21594)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.03 (L/4074)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3106.50 T_z=18.23 M_y=2.88 T_y=-149.36 M_z=691.76
  Tensioni: σ_N=-53.50 σ_M=-613.86 τ=0.00 σ_{max}=-667.36
  Tensioni: σ_N=-53.50 σ_M=36.27 τ=4.05 τ_{max}=4.05
  Tensioni: σ_N=-53.50 σ_M=-613.86 τ=0.00 $\sigma_{ID,max}$=667.36

Asta n. 234 (9 -5) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3657.03 My,Ed=334.69 Mz,Ed=655.49
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.56 M,cr=165553.00 λ_{LT}=0.25
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.03 + 0.16 = 0.21
  Verifica ZZ: 0.02 + 0.03 + 0.16 = 0.21

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/21741) $f_{Z,L}$=0.00 (L/89523)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.04 (L/4102) $f_{Z,L}$=0.01 (L/16019)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3657.03 T_z=186.79 M_y=334.69 T_y=-96.53 M_z=655.49
  Tensioni: σ_N=-62.98 σ_M=-695.20 τ=0.00 σ_{max}=-758.18
  Tensioni: σ_N=-62.98 σ_M=35.11 τ=11.25 τ_{max}=11.25
  Tensioni: σ_N=-62.98 σ_M=-695.20 τ=0.00 $\sigma_{ID,max}$=758.18

Asta n. 234 (-5 -6) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3602.39 My,Ed=-207.53 Mz,Ed=467.18
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.46 M,cr=154432.00 λ_{LT}=0.26
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.02 + 0.12 = 0.16
  Verifica ZZ: 0.02 + 0.02 + 0.12 = 0.15

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/50729)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/6917) $f_{Z,L}$=0.00 (L/44761)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3602.39 T_z=186.79 M_y=63.58 T_y=-162.95 M_z=467.18
  Tensioni: σ_N=-62.04 σ_M=-435.65 τ=0.00 σ_{max}=-497.69
  Tensioni: σ_N=-62.04 σ_M=25.03 τ=11.27 τ_{max}=11.27
  Tensioni: σ_N=-62.04 σ_M=-435.65 τ=0.00 $\sigma_{ID,max}$=497.69

Asta n. 234 (-6 -7) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3547.76 My,Ed=-478.64 Mz,Ed=-198.65
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.35 M,cr=143263.00 λ_{LT}=0.27
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.05 + 0.05 = 0.11
  Verifica ZZ: 0.02 + 0.04 + 0.05 = 0.10

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.00 (L/50729)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.02 (L/9632) $f_{Z,G}$=0.00 (L/69176)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.45 - Classe 3
  Sollecitazioni: N=-3493.12 T_z=186.79 M_y=-478.64 T_y=-295.80 M_z=-198.65
  Tensioni: σ_N=-60.16 σ_M=-339.69 τ=0.00 σ_{max}=-399.85
  Tensioni: σ_N=-60.16 σ_M=120.04 τ=12.49 τ_{max}=12.49
  Tensioni: σ_N=-60.16 σ_M=-339.69 τ=0.00 $\sigma_{ID,max}$=399.85

Asta n. 234 (-7 -8) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3493.12 My,Ed=-749.75 Mz,Ed=-676.17
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.20 M,cr=127444.00 λ_{LT}=0.29
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.07 + 0.17 = 0.26
  Verifica ZZ: 0.02 + 0.06 + 0.17 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.00 (L/29267) $f_{Z,G}$=0.00 (L/33819)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.03 (L/5435) $f_{Z,G}$=0.02 (L/5898)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.45 - Classe 3
  Sollecitazioni: N=-3438.49 T_z=186.79 M_y=-749.75 T_y=-362.22 M_z=-676.17
  Tensioni: σ_N=-59.22 σ_M=-855.48 τ=0.00 σ_{max}=-914.70

Tensioni: σ_N=-59.22 σ_M=168.47 τ=13.65 τ_{max}=13.65
Tensioni: σ_N=-59.22 σ_M=-855.48 τ=0.00 $\sigma_{ID,max}$=914.70

Asta n. 234 (-8 12) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-7704.59 My,Ed=-749.75 Mz,Ed=-676.17
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=185554.00 λ_{LT}=0.24
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.96, 0.96, 0.77, 0.96
Verifica YY: 0.04 + 0.07 + 0.17 = 0.28
Verifica ZZ: 0.04 + 0.06 + 0.17 = 0.27

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.00 (L/43482) $f_{Z,G}$=0.00 (L/47559)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/7686) $f_{Z,L}$=0.02 (L/8095)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-7704.59 T_z=-516.57 M_y=-749.75 T_y=499.09 M_z=-676.17
Tensioni: σ_N=-132.69 σ_M=-855.48 τ=0.00 σ_{max}=-988.17
Tensioni: σ_N=-132.69 σ_M=-36.22 τ=31.20 τ_{max}=31.20
Tensioni: σ_N=-132.69 σ_M=-855.48 τ=0.00 $\sigma_{ID,max}$=988.17

Asta n. 1001 (1850 1851) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-7421.36 My,Ed=-140.08 Mz,Ed=3603.62
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=700.73
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=7.01 Curva b: α-imp=0.34 k_c=0.94 ψ=1.66 M,cr=38445.30 λ_{LT}=0.68
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.72 β_{LT}=0.75 f=0.97 χ_{LT}=0.91
λ_Y=98.01 Ncr,y=183603.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.44
λ_Z=134.26 Ncr,z=97842.80 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
Kyy, Kyz, Kzy, Kzz = 0.98, 1.01, 0.79, 1.01
Verifica YY: 0.06 + 0.01 + 0.58 = 0.65
Verifica ZZ: 0.11 + 0.01 + 0.58 = 0.69

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/87472) $f_{Z,L}$=0.01 (L/118511)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.05 (L/15149) $f_{Z,L}$=0.03 (L/20075)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.01 - Classe 3
Sollecitazioni: N=-6813.50 T_z=-21.83 M_y=12.90 T_y=878.14 M_z=3603.62
Tensioni: σ_N=-80.07 σ_M=-1945.88 τ=0.00 σ_{max}=-2025.95
Tensioni: σ_N=-80.07 σ_M=137.84 τ=16.77 τ_{max}=16.77
Tensioni: σ_N=-80.07 σ_M=-1945.88 τ=0.00 $\sigma_{ID,max}$=2025.95

Asta n. 1002 (1844 1845) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-18023.60 My,Ed=-450.34 Mz,Ed=2525.11
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=702.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=7.02 Curva b: α-imp=0.34 k_c=0.94 ψ=1.55 M,cr=35932.60 λ_{LT}=0.70
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.74 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
λ_Y=98.21 Ncr,y=182868.00 λ^*_y=1.29 Curva b: Φ_y=1.51 χ_y=0.43
λ_Z=134.53 Ncr,z=97451.20 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
Kyy, Kyz, Kzy, Kzz = 1.03, 1.10, 0.83, 1.10
Verifica YY: 0.14 + 0.03 + 0.44 = 0.62
Verifica ZZ: 0.26 + 0.02 + 0.44 = 0.72

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.01 (L/57519) $f_{Z,G}$=0.01 (L/71828)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.07 (L/10169) $f_{Z,G}$=0.06 (L/12322)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-18023.60 T_z=-73.44 M_y=-450.34 T_y=-664.89 M_z=2525.11 M_x=6.78
  Tensioni: σ_N=-211.81 σ_M=-1452.28 τ=6.80 σ_{max}=-1664.09
  Tensioni: σ_N=-211.81 σ_M=170.67 τ=26.75 τ_{max}=26.75
  Tensioni: σ_N=-211.81 σ_M=-1452.28 τ=6.80 $\sigma_{ID,max}$=1664.13

Asta n. 1004 (1846 1847) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-20217.10 My,Ed=-437.97 Mz,Ed=-1901.97
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=702.06
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.02 Curva b: α-imp=0.34 k_c=0.94 ψ=1.58 M,cr=36636.50 λ_{LT}=0.69
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.73 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
  λ_Y=98.19 Ncr,y=182908.00 λ^*_y=1.29 Curva b: Φ_y=1.51 χ_y=0.43
  λ_Z=134.51 Ncr,z=97472.40 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 1.04, 1.11, 0.83, 1.11
  Verifica YY: 0.16 + 0.03 + 0.34 = 0.53
  Verifica ZZ: 0.29 + 0.02 + 0.34 = 0.65

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.02 (L/41357) $f_{Z,G}$=0.01 (L/72528)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.10 (L/7245) $f_{Z,G}$=0.06 (L/12445)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-14828.30 T_z=-97.83 M_y=-613.96 T_y=-571.33 M_z=2226.21 M_x=7.69
  Tensioni: σ_N=-174.26 σ_M=-1324.01 τ=7.71 σ_{max}=-1498.27
  Tensioni: σ_N=-174.26 σ_M=185.45 τ=29.27 τ_{max}=29.27
  Tensioni: σ_N=-174.26 σ_M=-1324.01 τ=7.71 $\sigma_{ID,max}$=1498.33

Asta n. 1005 (-872 -828) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/25228)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.07 (L/4571)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-13257.00
  N,Ed=-13257.00 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.18

- Verifica di stabilità (4.2.4.1.3.1) - CC 25
  Sollecitazioni: N=-13257.00 L=320.00
  λ=79.28 Ncr=70851.00 λ^*=1.04
  Curva a: Φ=1.13 χ,min=0.64 N,Ed=-13257.00 Nb,Rd=46443.40 N,Ed/Nb,Rd=0.29

Asta n. 1006 (-873 -831) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/24672)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.04 (L/4485)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-13606.70
  N,Ed=-13606.70 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.19

- Verifica di stabilità (4.2.4.1.3.1) - CC 25
  Sollecitazioni: N=-13606.70 L=160.00
  λ=39.64 Ncr=283404.00 λ^*=0.52
  Curva a: Φ=0.67 χ,min=0.92 N,Ed=-13606.70 Nb,Rd=66718.00 N,Ed/Nb,Rd=0.20

Asta n. 1007 (1859 1978) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/25578)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.61 - Classe 3
  Sollecitazioni: N=4722.85
  Tensioni: σ_N=219.79 σ_M=0.00 τ=0.00 σ_{max}=219.79
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=219.79 σ_M=0.00 τ=0.00 $\sigma_{ID,max}$=219.79

Asta n. 1008 (1860 1979) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/52756)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/9175)

- Verifica a compressione (4.2.10) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-8352.27
  N,Ed=-8352.27 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.11

Asta n. 1009 (1979 1859) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 23 - Classe 3
  L_{cr}=2.59 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
  $\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
  CC 23 My,Ed=-5.39 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-3430.60 M,Ed=4.05
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=259.36
  λ=259.36 Ncr=3872.04 λ^*=3.39 Curva c: Φ=7.04 χ,min=0.08
  χ,min=0.08
  Verifica: 1.07 + 0.17 = 1.23

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/118240)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.14 (L/1814) $f_{Z,G}$=0.09 (L/2991)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.30 - Classe 3
  Sollecitazioni: N=-6535.00 M=5.39
  Tensioni: σ_N=-520.04 σ_M=-85.86 τ=0.00 σ_{max}=-605.90
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-520.04 σ_M=-85.86 τ=0.00 $\sigma_{ID,max}$=605.90

Asta n. 1010 (1978 1860) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 25 - Classe 3
  L_{cr}=2.10 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
  $\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
  CC 25 My,Ed=-5.68 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 23 - Classe 3
  Sollecitazioni: N,Ed=-838.62 M,Ed=3.28
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=209.96
  λ=209.96 Ncr=5908.50 λ^*=2.75 Curva c: Φ=4.90 χ,min=0.11
  χ,min=0.11
  Verifica: 0.18 + 0.02 = 0.19

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/146769)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.08 (L/2765) $f_{Z,G}$=0.07 (L/3223)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.05 - Classe 3
  Sollecitazioni: N=8800.39 M=4.37
  Tensioni: σ_N=700.31 σ_M=69.51 τ=0.00 σ_{max}=769.82
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=700.31 σ_M=69.51 τ=0.00 $\sigma_{ID,max}$=769.82

Asta n. 1011 (1856 1976) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/140684)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/23447)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.61 - Classe 3
  Sollecitazioni: N=5257.42
  Tensioni: σ_N=244.66 σ_M=0.00 τ=0.00 σ_{max}=244.66

Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=244.66 σ_M=0.00 τ=0.00 $\sigma_{ID,max}$=244.66

Asta n. 1012 (1857 1977) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-5706.90 M,Ed=0.00
Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=161.00
αmy, αmz, αLT = 0.95, ----, ----
λ=39.89 Ncr=279894.00 λ^*=0.52
Curva a: Φ=0.67 χ,min=0.92
Kyy, Kyz, Kzy, Kzz = 0.98, ----, ----, ----
Verifica: 0.08 = 0.08

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/93789)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.01 (L/15631)

- Verifica a compressione (4.2.10) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-5706.90
N,Ed=-5706.90 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.08

Asta n. 1013 (1856 1977) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 23 - Classe 3
L_{cr}=2.59 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
$\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
CC 23 My,Ed=-5.39 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 13 - Classe 3
Sollecitazioni: N,Ed=-3765.27 M,Ed=4.05
Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=259.36
λ=259.36 Ncr=3872.04 λ^*=3.39 Curva c: Φ=7.04 χ,min=0.08
χ,min=0.08
Verifica: 1.17 + 0.69 = 1.86

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/151085)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.14 (L/1810) $f_{Z,G}$=0.10 (L/2648)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.29 - Classe 3
Sollecitazioni: N=-4529.64 M=5.39
Tensioni: σ_N=-360.46 σ_M=-85.86 τ=0.00 σ_{max}=-446.32
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=-360.46 σ_M=-85.86 τ=0.00 $\sigma_{ID,max}$=446.32

Asta n. 1014 (1857 1976) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 25 - Classe 3
L_{cr}=2.10 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
$\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
CC 25 My,Ed=-5.68 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 23 - Classe 3
Sollecitazioni: N,Ed=-368.17 M,Ed=3.28
Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=209.96
λ=209.96 Ncr=5908.50 λ^*=2.75 Curva c: Φ=4.90 χ,min=0.11
χ,min=0.11
Verifica: 0.08 + 0.02 = 0.09

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/157252)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.08 (L/2772) $f_{Z,G}$=0.06 (L/3675)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.05 - Classe 3
Sollecitazioni: N=6685.35 M=4.37
Tensioni: σ_N=532.00 σ_M=69.51 τ=0.00 σ_{max}=601.51
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=532.00 σ_M=69.51 τ=0.00 $\sigma_{ID,max}$=601.51

Asta n. 1015 (1851 1847) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2528.72 M,Ed=2.86
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=102.22
  αmy, αmz, αLT = 0.95, ----, ----
  λ=25.33 Ncr=694405.00 λ*=0.33
  Curva a: Φ=0.57 χ,min=0.97
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.03 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.51 - Classe 3
  Sollecitazioni: N=-2528.72 M=2.86
  Tensioni: σ_N=-117.68 σ_M=-4.91 τ=0.00 σ_{max}=-122.59
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-117.68 σ_M=-4.91 τ=0.00 $\sigma_{ID,max}$=122.59

Asta n. 1016 (1847 1849) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2888.47 M,Ed=4.01
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=120.97
  αmy, αmz, αLT = 0.95, ----, ----
  λ=29.97 Ncr=495807.00 λ*=0.39
  Curva a: Φ=0.60 χ,min=0.95
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.60 - Classe 3
  Sollecitazioni: N=-2888.47 M=4.01
  Tensioni: σ_N=-134.42 σ_M=-6.88 τ=0.00 σ_{max}=-141.29
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-134.42 σ_M=-6.88 τ=0.00 $\sigma_{ID,max}$=141.29

Asta n. 1017 (1849 1845) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2488.40 M,Ed=2.89
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=102.73
  αmy, αmz, αLT = 0.95, ----, ----
  λ=25.45 Ncr=687495.00 λ*=0.33
  Curva a: Φ=0.57 χ,min=0.97
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.03 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.51 - Classe 3
  Sollecitazioni: N=-2488.40 M=2.89
  Tensioni: σ_N=-115.80 σ_M=-4.96 τ=0.00 σ_{max}=-120.76
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-115.80 σ_M=-4.96 τ=0.00 $\sigma_{ID,max}$=120.76

Asta n. 1018 (1845 1851) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2909.50 M,Ed=3.97
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=120.28
  αmy, αmz, αLT = 0.95, ----, ----
  λ=29.80 Ncr=501462.00 λ*=0.39
  Curva a: Φ=0.60 χ,min=0.96
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.60 - Classe 3
  Sollecitazioni: N=-2909.50 M=3.97
  Tensioni: σ_N=-135.40 σ_M=-6.80 τ=0.00 σ_{max}=-142.20
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-135.40 σ_M=-6.80 τ=0.00 $\sigma_{ID,max}$=142.20

Asta n. 1101 (1851 1858) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7163.00 My,Ed=382.80 Mz,Ed=-4983.76
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=526.58
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.27 Curva b: α-imp=0.34 k_c=0.94 ψ=1.72 M,cr=56147.20 λ_{LT}=0.56

$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.65 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_Y=73.65 Ncr,y=325125.00 λ^*_y=0.96 Curva b: Φ_y=1.09 χ_y=0.62
λ_Z=100.89 Ncr,z=173260.00 λ^*_z=1.32 Curva c: Φ_z=1.65 χ_z=0.38
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
Verifica YY: 0.04 + 0.02 + 0.78 = 0.85
Verifica ZZ: 0.07 + 0.02 + 0.78 = 0.87

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/38080) $f_{Z,L}$=0.01 (L/51603)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.09 (L/5886) $f_{Z,L}$=0.06 (L/9141)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=5.27 - Classe 3
Sollecitazioni: N=-6711.46 T_z=-70.26 M_y=382.80 T_y=-1666.81 M_z=-4983.76 M_x=-1.45
Tensioni: σ_N=-78.87 σ_M=-2764.54 τ=1.45 σ_{max}=-2843.42
Tensioni: σ_N=-78.87 σ_M=255.24 τ=33.34 τ_{max}=33.34
Tensioni: σ_N=-78.87 σ_M=-2764.54 τ=1.45 $\sigma_{ID,max}$=2843.42

Asta n. 1102 (1845 1861) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-18310.40 My,Ed=-397.58 Mz,Ed=-2273.71
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=553.99
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=5.54 Curva b: α-imp=0.34 k_c=0.94 ψ=1.59 M,cr=48872.90 λ_{LT}=0.60
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.67 β_{LT}=0.75 f=0.97 χ_{LT}=0.94
λ_Y=77.48 Ncr,y=293755.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
λ_Z=106.14 Ncr,z=156543.00 λ^*_z=1.39 Curva c: Φ_z=1.76 χ_z=0.35
Kyy, Kyz, Kzy, Kzz = 1.01, 1.05, 0.81, 1.05
Verifica YY: 0.11 + 0.03 + 0.38 = 0.52
Verifica ZZ: 0.18 + 0.02 + 0.38 = 0.58

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.02 (L/33577) $f_{Z,L}$=0.00 (L/138308)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.09 (L/5909) $f_{Z,L}$=0.02 (L/25477)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-18310.40 T_z=82.28 M_y=63.48 T_y=737.71 M_z=-2273.71 M_x=-8.81
Tensioni: σ_N=-215.18 σ_M=-1238.89 τ=8.83 σ_{max}=-1454.07
Tensioni: σ_N=-215.18 σ_M=-98.52 τ=33.31 τ_{max}=33.31
Tensioni: σ_N=-215.18 σ_M=-1238.89 τ=8.83 $\sigma_{ID,max}$=1454.15

Asta n. 1103 (1849 1855) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-7115.35 My,Ed=108.44 Mz,Ed=-4941.81
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=526.43
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=5.26 Curva b: α-imp=0.34 k_c=0.94 ψ=1.14 M,cr=37333.00 λ_{LT}=0.69
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.73 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
λ_Y=73.63 Ncr,y=325318.00 λ^*_y=0.96 Curva b: Φ_y=1.09 χ_y=0.62
λ_Z=100.86 Ncr,z=173363.00 λ^*_z=1.32 Curva c: Φ_z=1.65 χ_z=0.38
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
Verifica YY: 0.04 + 0.01 + 0.78 = 0.82
Verifica ZZ: 0.07 + 0.01 + 0.78 = 0.85

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/40291) $f_{Z,L}$=0.00 (L/367998)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.09 (L/6140) $f_{Z,L}$=0.01 (L/57499)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=5.26 - Classe 3
Sollecitazioni: N=-6663.80 T_z=-35.75 M_y=108.44 T_y=-1670.30 M_z=-4941.81 M_x=7.32
Tensioni: σ_N=-78.31 σ_M=-2686.73 τ=7.34 σ_{max}=-2765.04
Tensioni: σ_N=-78.31 σ_M=-209.36 τ=39.96 τ_{max}=39.96
Tensioni: σ_N=-78.31 σ_M=-2686.73 τ=7.34 $\sigma_{ID,max}$=2765.07

Asta n. 1104 (1847 1852) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-20482.30 My,Ed=-88.91 Mz,Ed=-1902.65
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=553.99

αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=5.54 Curva b: α-imp=0.34 k_c=0.94 ψ=1.23 M,cr=37682.30 λ_{LT}=0.68
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.72 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
λ_Y=77.48 Ncr,y=293755.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
λ_Z=106.14 Ncr,z=156543.00 λ^*_z=1.39 Curva c: Φ_z=1.76 χ_z=0.35
Kyy, Kyz, Kzy, Kzz = 1.02, 1.06, 0.82, 1.06
Verifica YY: 0.12 + 0.01 + 0.32 = 0.45
Verifica ZZ: 0.20 + 0.00 + 0.32 = 0.53

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.02 (L/35420)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.09 (L/6273) $f_{Z,L}$=0.01 (L/82985)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-20482.30 T_z=25.73 M_y=53.61 T_y=759.57 M_z=-1902.65 M_x=-7.29
Tensioni: σ_N=-240.71 σ_M=-1036.80 τ=7.31 σ_{max}=-1277.51
Tensioni: σ_N=-240.71 σ_M=-82.52 τ=27.76 τ_{max}=27.76
Tensioni: σ_N=-240.71 σ_M=-1036.80 τ=7.31 $\sigma_{ID,max}$=1277.57

Asta n. 1105 (-828 1980) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-11664.80 M,Ed=0.12
Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=78.22
αmy, αmz, αLT = 0.95, ----, ----
λ=19.38 Ncr=1185880.00 λ^*=0.25
Curva a: Φ=0.54 χ,min=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
Verifica: 0.16 + 0.00 = 0.16

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/29291)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.01 (L/5257)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-11664.80
N,Ed=-11664.80 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.16

Asta n. 1106 (-831 1981) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-10735.20 M,Ed=0.29
Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=66.17
αmy, αmz, αLT = 0.95, ----, ----
λ=16.39 Ncr=1657040.00 λ^*=0.21
Curva a: Φ=0.52 χ,min=1.00
Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
Verifica: 0.15 + 0.00 = 0.15

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/31537)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.01 (L/6086)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-10735.20 T=1.76
N,Ed=-10735.20 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.15

Asta n. 1211 (1858 1860) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3392.90 My,Ed=1285.96 Mz,Ed=-2061.88
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=379.60
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.80 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=39930.60 λ_{LT}=0.51
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.62 β_{LT}=0.75 f=0.98 χ_{LT}=0.98
λ_Y=62.61 Ncr,y=307021.00 λ^*_y=0.82 Curva b: Φ_y=0.94 χ_y=0.71
λ_Z=83.04 Ncr,z=174529.00 λ^*_z=1.09 Curva c: Φ_z=1.31 χ_z=0.49
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.13 + 0.52 = 0.67
Verifica ZZ: 0.02 + 0.10 + 0.52 = 0.64

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.06 (L/6389) $f_{Z,L}$=0.04 (L/10699)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.33 (L/1146) $f_{Z,L}$=0.20 (L/1909)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3392.90 T_z=338.77 M_y=1285.96 T_y=612.84 M_z=-2061.88
  Tensioni: σ_N=-58.43 σ_M=-2266.55 τ=0.00 σ_{max}=-2324.98
  Tensioni: σ_N=-58.43 σ_M=-461.54 τ=23.96 τ_{max}=23.96
  Tensioni: σ_N=-58.43 σ_M=-2266.55 τ=0.00 $\sigma_{ID,max}$=2324.98

Asta n. 1212 (1858 1859) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3586.33 My,Ed=-1188.71 Mz,Ed=-2537.28
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=334.12
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=3.34 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=47739.80 λ_{LT}=0.47
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.59 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=55.11 Ncr,y=396295.00 λ^*_y=0.72 Curva b: Φ_y=0.85 χ_y=0.77
  λ_Z=73.09 Ncr,z=225278.00 λ^*_z=0.96 Curva c: Φ_z=1.14 χ_z=0.57
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
  Verifica YY: 0.02 + 0.12 + 0.64 = 0.78
  Verifica ZZ: 0.02 + 0.09 + 0.64 = 0.75

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.06 (L/5848) $f_{Z,L}$=0.03 (L/13170)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.32 (L/1033) $f_{Z,L}$=0.14 (L/2346)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3586.33 T_z=-355.78 M_y=-1188.71 T_y=820.84 M_z=-2537.28
  Tensioni: σ_N=-61.76 σ_M=-2654.49 τ=0.00 σ_{max}=-2716.25
  Tensioni: σ_N=-61.76 σ_M=188.62 τ=28.53 τ_{max}=28.53
  Tensioni: σ_N=-61.76 σ_M=-2654.49 τ=0.00 $\sigma_{ID,max}$=2716.25

Asta n. 1212 (1861 1863) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-11906.00 My,Ed=675.45 Mz,Ed=240.88
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=437.01
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=4.37 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=33075.30 λ_{LT}=0.56
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
  λ_Y=72.08 Ncr,y=231652.00 λ^*_y=0.94 Curva b: Φ_y=1.07 χ_y=0.63
  λ_Z=95.60 Ncr,z=131685.00 λ^*_z=1.25 Curva c: Φ_z=1.54 χ_z=0.41
  Kyy, Kyz, Kzy, Kzz = 1.00, 1.03, 0.80, 1.03
  Verifica YY: 0.10 + 0.07 + 0.07 = 0.23
  Verifica ZZ: 0.15 + 0.06 + 0.07 = 0.27

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.02 (L/19093) $f_{Z,G}$=0.01 (L/34453)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.14 (L/3125) $f_{Z,G}$=0.08 (L/5273)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-11906.00 T_z=154.56 M_y=675.45 T_y=16.05 M_z=237.04
  Tensioni: σ_N=-205.04 σ_M=-441.01 τ=0.00 σ_{max}=-646.05
  Tensioni: σ_N=-205.04 σ_M=12.70 τ=9.30 τ_{max}=9.30
  Tensioni: σ_N=-205.04 σ_M=-441.01 τ=0.00 $\sigma_{ID,max}$=646.05

Asta n. 1213 (1855 1856) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3224.36 My,Ed=1069.82 Mz,Ed=-2090.17
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=352.04
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=3.52 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=44330.50 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=58.06 Ncr,y=356964.00 λ^*_y=0.76 Curva b: Φ_y=0.88 χ_y=0.75
  λ_Z=77.01 Ncr,z=202920.00 λ^*_z=1.01 Curva c: Φ_z=1.21 χ_z=0.54

Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.10 + 0.53 = 0.65
Verifica ZZ: 0.02 + 0.08 + 0.53 = 0.63

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.06 (L/6299) $f_{Z,L}$=0.03 (L/13929)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.31 (L/1122) $f_{Z,L}$=0.14 (L/2489)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3224.36 T_z=303.89 M_y=1069.82 T_y=663.39 M_z=-2090.17
Tensioni: σ_N=-55.53 σ_M=-2217.70 τ=0.00 σ_{max}=-2273.22
Tensioni: σ_N=-55.53 σ_M=-404.05 τ=23.62 τ_{max}=23.62
Tensioni: σ_N=-55.53 σ_M=-2217.70 τ=0.00 $\sigma_{ID,max}$=2273.22

Asta n. 1214 (1852 1854) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-9055.43 My,Ed=-901.03 Mz,Ed=-181.03
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=448.31
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.48 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=31994.10 λ_{LT}=0.57
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.65 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_Y=73.94 Ncr,y=220115.00 λ^*_y=0.97 Curva b: Φ_y=1.10 χ_y=0.62
λ_Z=98.07 Ncr,z=125127.00 λ^*_z=1.28 Curva c: Φ_z=1.59 χ_z=0.40
Kyy, Kyz, Kzy, Kzz = 0.99, 1.02, 0.79, 1.02
Verifica YY: 0.07 + 0.09 + 0.05 = 0.22
Verifica ZZ: 0.12 + 0.08 + 0.05 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.03 (L/13745) $f_{Z,G}$=0.00 (L/127051)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.20 (L/2291) $f_{Z,G}$=0.02 (L/23043)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-9055.43 T_z=-200.98 M_y=-901.03 T_y=121.88 M_z=-181.03
Tensioni: σ_N=-155.95 σ_M=-468.55 τ=0.00 σ_{max}=-624.49
Tensioni: σ_N=-155.95 σ_M=-9.70 τ=12.11 τ_{max}=12.11
Tensioni: σ_N=-155.95 σ_M=-468.55 τ=0.00 $\sigma_{ID,max}$=624.49

Asta n. 1222 (1861 1862) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-9798.01 My,Ed=-734.43 Mz,Ed=-172.78
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=458.65
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.59 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=31066.50 λ_{LT}=0.58
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
λ_Y=75.65 Ncr,y=210307.00 λ^*_y=0.99 Curva b: Φ_y=1.12 χ_y=0.60
λ_Z=100.33 Ncr,z=119551.00 λ^*_z=1.31 Curva c: Φ_z=1.63 χ_z=0.38
Kyy, Kyz, Kzy, Kzz = 1.00, 1.02, 0.80, 1.02
Verifica YY: 0.08 + 0.08 + 0.05 = 0.21
Verifica ZZ: 0.13 + 0.06 + 0.05 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.03 (L/16727) $f_{Z,G}$=0.00 (L/117299)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.17 (L/2750) $f_{Z,G}$=0.02 (L/21279)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-9798.01 T_z=-160.13 M_y=-734.43 T_y=119.17 M_z=-172.78
Tensioni: σ_N=-168.74 σ_M=-404.25 τ=0.00 σ_{max}=-572.99
Tensioni: σ_N=-168.74 σ_M=-9.26 τ=9.66 τ_{max}=9.66
Tensioni: σ_N=-168.74 σ_M=-404.25 τ=0.00 $\sigma_{ID,max}$=572.99

Asta n. 1223 (1855 1857) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3713.44 My,Ed=-1208.89 Mz,Ed=-2518.51
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=363.03
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.63 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=42465.80 λ_{LT}=0.49
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.61 β_{LT}=0.75 f=0.98 χ_{LT}=0.99

λ_Y=59.88 Ncr,y=335675.00 λ^*_y=0.78 Curva b: Φ_y=0.91 χ_y=0.73
λ_Z=79.42 Ncr,z=190818.00 λ^*_z=1.04 Curva c: Φ_z=1.25 χ_z=0.52
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.12 + 0.64 = 0.78
Verifica ZZ: 0.02 + 0.10 + 0.64 = 0.75

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.06 (L/5901) $f_{Z,L}$=0.03 (L/11919)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.35 (L/1046) $f_{Z,L}$=0.17 (L/2113)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3713.44 T_z=-333.00 M_y=-1208.89 T_y=755.17 M_z=-2518.51
Tensioni: σ_N=-63.95 σ_M=-2644.75 τ=0.00 σ_{max}=-2708.70
Tensioni: σ_N=-63.95 σ_M=195.13 τ=26.44 τ_{max}=26.44
Tensioni: σ_N=-63.95 σ_M=-2644.75 τ=0.00 $\sigma_{ID,max}$=2708.70

Asta n. 1224 (1852 1853) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-11258.10 My,Ed=556.27 Mz,Ed=262.60
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=426.15
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.26 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=34185.30 λ_{LT}=0.55
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_Y=70.29 Ncr,y=243609.00 λ^*_y=0.92 Curva b: Φ_y=1.05 χ_y=0.65
λ_Z=93.22 Ncr,z=138482.00 λ^*_z=1.22 Curva c: Φ_z=1.49 χ_z=0.42
Kyy, Kyz, Kzy, Kzz = 1.00, 1.03, 0.80, 1.03
Verifica YY: 0.09 + 0.06 + 0.07 = 0.22
Verifica ZZ: 0.14 + 0.05 + 0.07 = 0.25

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.02 (L/24963) $f_{Z,G}$=0.01 (L/33099)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.11 (L/3892) $f_{Z,G}$=0.08 (L/5072)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-11258.10 T_z=130.53 M_y=556.27 T_y=8.96 M_z=261.38
Tensioni: σ_N=-193.88 σ_M=-421.82 τ=0.00 σ_{max}=-615.70
Tensioni: σ_N=-193.88 σ_M=14.00 τ=7.86 τ_{max}=7.86
Tensioni: σ_N=-193.88 σ_M=-421.82 τ=0.00 $\sigma_{ID,max}$=615.70

Asta n. 1232 (-828 1864) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-4579.06 My,Ed=-87.91 Mz,Ed=-721.64
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=248865.00 λ_{LT}=0.20
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.01 + 0.18 = 0.21
Verifica ZZ: 0.02 + 0.01 + 0.18 = 0.21

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/41796)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/6748) $f_{Z,L}$=0.00 (L/71982)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-4579.06 T_z=-71.14 M_y=-87.91 T_y=617.22 M_z=-721.64
Tensioni: σ_N=-78.86 σ_M=-669.41 τ=0.00 σ_{max}=-748.27
Tensioni: σ_N=-78.86 σ_M=-14.66 τ=16.69 τ_{max}=16.69
Tensioni: σ_N=-78.86 σ_M=-669.41 τ=0.00 $\sigma_{ID,max}$=748.27

Asta n. 1232 (-827 -828) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3172.68 My,Ed=-87.91 Mz,Ed=-721.64
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95

L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.14 M,cr=162662.00 λ_{LT}=0.25
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.02 + 0.01 + 0.18 = 0.20
Verifica ZZ: 0.02 + 0.01 + 0.18 = 0.20

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/30132)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/5266) $f_{Z,L}$=0.00 (L/53986)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.24 - Classe 3
Sollecitazioni: N=-3141.86 T_z=19.26 M_y=-87.91 T_y=-429.60 M_z=-721.64
Tensioni: σ_N=-54.11 σ_M=-669.41 τ=0.00 σ_{max}=-723.52
Tensioni: σ_N=-54.11 σ_M=-14.66 τ=11.37 τ_{max}=11.37
Tensioni: σ_N=-54.11 σ_M=-669.41 τ=0.00 $\sigma_{ID,max}$=723.52

Asta n. 1232 (-826 -827) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 - Classe 3
Sollecitazioni: N,Ed=-2477.98 My,Ed=-304.83 Mz,Ed=-167.05
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.11 M,cr=157437.00 λ_{LT}=0.26
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01 + 0.03 + 0.04 = 0.08
Verifica ZZ: 0.01 + 0.02 + 0.04 = 0.08

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.00 (L/64784) $f_{Z,G}$=0.00 (L/86378)

- Verifica in termini tensionali (4.2.5) - CC 1 Xl=1.24 - Classe 3
Sollecitazioni: N=-2454.28 T_z=56.04 M_y=-304.83 T_y=-268.19 M_z=-167.05
Tensioni: σ_N=-42.27 σ_M=-252.26 τ=0.00 σ_{max}=-294.52
Tensioni: σ_N=-42.27 σ_M=74.28 τ=7.65 τ_{max}=7.65
Tensioni: σ_N=-42.27 σ_M=-252.26 τ=0.00 $\sigma_{ID,max}$=294.52

Asta n. 1232 (-825 -826) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3234.30 My,Ed=-40.31 Mz,Ed=501.55
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.37 M,cr=194871.00 λ_{LT}=0.23
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.02 + 0.00 + 0.13 = 0.15
Verifica ZZ: 0.02 + 0.00 + 0.13 = 0.14

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/46274)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/6748)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3234.30 T_z=19.26 M_y=-16.51 T_y=-230.34 M_z=501.55
Tensioni: σ_N=-55.70 σ_M=-450.00 τ=0.00 σ_{max}=-505.70
Tensioni: σ_N=-55.70 σ_M=31.37 τ=6.16 τ_{max}=6.16
Tensioni: σ_N=-55.70 σ_M=-450.00 τ=0.00 $\sigma_{ID,max}$=505.70

Asta n. 1232 (1861 -825) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3265.12 My,Ed=-16.51 Mz,Ed=745.13
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95

L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.34 M,cr=191218.00 λ_{LT}=0.23
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.02 + 0.00 + 0.19 = 0.20
Verifica ZZ: 0.02 + 0.00 + 0.19 = 0.20

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/20566)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.03 (L/3766)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3265.12 T_z=19.26 M_y=7.29 T_y=-163.91 M_z=745.13
Tensioni: σ_N=-56.23 σ_M=-662.65 τ=0.00 σ_{max}=-718.88
Tensioni: σ_N=-56.23 σ_M=37.93 τ=4.44 τ_{max}=4.44
Tensioni: σ_N=-56.23 σ_M=-662.65 τ=0.00 $\sigma_{ID,max}$=718.88

Asta n. 1234 (1852 -824) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3921.26 My,Ed=266.31 Mz,Ed=615.13
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.65 M,cr=174974.00 λ_{LT}=0.24
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.03 + 0.15 = 0.20
Verifica ZZ: 0.02 + 0.02 + 0.15 = 0.19

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/23058) $f_{Z,L}$=0.00 (L/108706)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.03 (L/4373) $f_{Z,L}$=0.01 (L/21137)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3921.26 T_z=165.54 M_y=266.31 T_y=-86.36 M_z=615.13
Tensioni: σ_N=-67.53 σ_M=-636.06 τ=0.00 σ_{max}=-703.59
Tensioni: σ_N=-67.53 σ_M=32.95 τ=9.97 τ_{max}=9.97
Tensioni: σ_N=-67.53 σ_M=-636.06 τ=0.00 $\sigma_{ID,max}$=703.59

Asta n. 1234 (-824 -829) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3866.62 My,Ed=-214.24 Mz,Ed=441.59
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.63 M,cr=172494.00 λ_{LT}=0.25
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.02 + 0.11 = 0.15
Verifica ZZ: 0.02 + 0.02 + 0.11 = 0.15

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/52479)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/7212) $f_{Z,L}$=0.00 (L/36235)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3866.62 T_z=165.54 M_y=26.04 T_y=-152.78 M_z=441.59
Tensioni: σ_N=-66.59 σ_M=-400.14 τ=0.00 σ_{max}=-466.73
Tensioni: σ_N=-66.59 σ_M=23.66 τ=10.00 τ_{max}=10.00
Tensioni: σ_N=-66.59 σ_M=-400.14 τ=0.00 $\sigma_{ID,max}$=466.73

Asta n. 1234 (-829 -830) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3

Sollecitazioni: N,Ed=-3811.99 My,Ed=-454.51 Mz,Ed=-194.70
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.32 M,cr=140144.00 λ_{LT}=0.27
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.04 + 0.05 = 0.11
Verifica ZZ: 0.02 + 0.04 + 0.05 = 0.10

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.00 (L/54353)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.01 (L/9882) $f_{Z,G}$=0.00 (L/76094)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.45 - Classe 3
Sollecitazioni: N=-3757.35 T_z=165.54 M_y=-454.51 T_y=-285.62 M_z=-194.70
Tensioni: σ_N=-64.71 σ_M=-327.94 τ=0.00 σ_{max}=-392.65
Tensioni: σ_N=-64.71 σ_M=113.66 τ=11.47 τ_{max}=11.47
Tensioni: σ_N=-64.71 σ_M=-327.94 τ=0.00 $\sigma_{ID,max}$=392.65

Asta n. 1234 (-830 -831) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3757.35 My,Ed=-694.77 Mz,Ed=-657.46
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.19 M,cr=126336.00 λ_{LT}=0.29
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.07 + 0.16 = 0.25
Verifica ZZ: 0.02 + 0.05 + 0.16 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.00 (L/31706) $f_{Z,G}$=0.00 (L/33819)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.02 (L/5853) $f_{Z,G}$=0.02 (L/6039)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.45 - Classe 3
Sollecitazioni: N=-3702.71 T_z=165.54 M_y=-694.77 T_y=-352.05 M_z=-657.46
Tensioni: σ_N=-63.77 σ_M=-820.10 τ=0.00 σ_{max}=-883.87
Tensioni: σ_N=-63.77 σ_M=154.47 τ=12.69 τ_{max}=12.69
Tensioni: σ_N=-63.77 σ_M=-820.10 τ=0.00 $\sigma_{ID,max}$=883.87

Asta n. 1234 (-831 1865) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-7650.79 My,Ed=-694.78 Mz,Ed=-657.46
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=185555.00 λ_{LT}=0.24
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.96, 0.96, 0.77, 0.96
Verifica YY: 0.04 + 0.07 + 0.17 = 0.27
Verifica ZZ: 0.04 + 0.05 + 0.17 = 0.26

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.00 (L/47559) $f_{Z,G}$=0.00 (L/50729)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/7926) $f_{Z,L}$=0.02 (L/8746)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-7650.79 T_z=-478.70 M_y=-694.78 T_y=486.19 M_z=-657.46
Tensioni: σ_N=-131.76 σ_M=-820.10 τ=0.00 σ_{max}=-951.86
Tensioni: σ_N=-131.76 σ_M=-35.22 τ=28.92 τ_{max}=28.92
Tensioni: σ_N=-131.76 σ_M=-820.10 τ=0.00 $\sigma_{ID,max}$=951.86

Asta n. 2001 (1872 1873) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-5190.74 My,Ed=-3564.30 Mz,Ed=2731.53
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=700.73
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.01 Curva b: α-imp=0.34 k_c=0.94 ψ=1.46 M,cr=33864.60 λ_{LT}=0.72
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.75 β_{LT}=0.75 f=0.97 χ_{LT}=0.88
  λ_Y=98.01 Ncr,y=183603.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.44
  λ_Z=134.26 Ncr,z=97842.80 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
  Verifica YY: 0.04 + 0.23 + 0.43 = 0.71
  Verifica ZZ: 0.07 + 0.19 + 0.43 = 0.69

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/89606) $f_{Z,L}$=0.01 (L/114807)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.05 (L/15436) $f_{Z,L}$=0.03 (L/20130)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.01 - Classe 3
  Sollecitazioni: N=-6703.87 T_z=-19.30 M_y=4.25 T_y=866.74 M_z=3551.76
  Tensioni: σ_N=-78.78 σ_M=-1916.17 τ=0.00 σ_{max}=-1994.96
  Tensioni: σ_N=-78.78 σ_M=137.22 τ=16.55 τ_{max}=16.55
  Tensioni: σ_N=-78.78 σ_M=-1916.17 τ=0.00 $\sigma_{ID,max}$=1994.96

Asta n. 2002 (1866 1867) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-18501.60 My,Ed=-498.06 Mz,Ed=3265.72
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=702.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.02 Curva b: α-imp=0.34 k_c=0.94 ψ=1.57 M,cr=36266.80 λ_{LT}=0.70
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.73 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
  λ_Y=98.21 Ncr,y=182868.00 λ^*_y=1.29 Curva b: Φ_y=1.51 χ_y=0.43
  λ_Z=134.53 Ncr,z=97451.20 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 1.03, 1.10, 0.83, 1.10
  Verifica YY: 0.15 + 0.03 + 0.57 = 0.76
  Verifica ZZ: 0.26 + 0.03 + 0.57 = 0.86

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.01 (L/52588) $f_{Z,G}$=0.01 (L/73258)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.08 (L/9319) $f_{Z,G}$=0.06 (L/12499)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-18501.60 T_z=-77.12 M_y=-498.06 T_y=-824.55 M_z=3265.72 M_x=6.30
  Tensioni: σ_N=-217.43 σ_M=-1861.26 τ=6.32 σ_{max}=-2078.69
  Tensioni: σ_N=-217.43 σ_M=207.12 τ=27.18 τ_{max}=27.18
  Tensioni: σ_N=-217.43 σ_M=-1861.26 τ=6.32 $\sigma_{ID,max}$=2078.72

Asta n. 2004 (1868 1869) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-17803.60 My,Ed=-595.53 Mz,Ed=3217.03
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=702.06
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.02 Curva b: α-imp=0.34 k_c=0.94 ψ=1.62 M,cr=37497.70 λ_{LT}=0.69
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.73 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
  λ_Y=98.19 Ncr,y=182908.00 λ^*_y=1.29 Curva b: Φ_y=1.51 χ_y=0.43
  λ_Z=134.51 Ncr,z=97472.40 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 1.03, 1.09, 0.82, 1.09
  Verifica YY: 0.14 + 0.04 + 0.56 = 0.74
  Verifica ZZ: 0.25 + 0.03 + 0.56 = 0.85

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.02 (L/44888) $f_{Z,G}$=0.01 (L/73986)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.09 (L/7765) $f_{Z,G}$=0.06 (L/12638)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-17803.60 T_z=-91.94 M_y=-595.53 T_y=-810.09 M_z=3217.03 M_x=6.75
  Tensioni: σ_N=-209.23 σ_M=-1854.61 τ=6.76 σ_{max}=-2063.84

Tensioni: σ_N=-209.23 σ_M=220.95 τ=28.56 τ_{max}=28.56
Tensioni: σ_N=-209.23 σ_M=-1854.61 τ=6.76 $\sigma_{ID,max}$=2063.87

Asta n. 2005 (-874 -836) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/25040)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.07 (L/4552)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-13281.10
N,Ed=-13281.10 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.18

- Verifica di stabilità (4.2.4.1.3.1) - CC 25
Sollecitazioni: N=-13281.10 L=320.00
λ=79.28 Ncr=70851.00 λ^*=1.04
Curva a: Φ=1.13 χ,min=0.64 N,Ed=-13281.10 Nb,Rd=46443.40 N,Ed/Nb,Rd=0.29

Asta n. 2006 (-875 -839) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/24314)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.04 (L/4450)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-13704.40
N,Ed=-13704.40 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.19

- Verifica di stabilità (4.2.4.1.3.1) - CC 25
Sollecitazioni: N=-13704.40 L=160.00
λ=39.64 Ncr=283404.00 λ^*=0.52
Curva a: Φ=0.67 χ,min=0.92 N,Ed=-13704.40 Nb,Rd=66718.00 N,Ed/Nb,Rd=0.21

Asta n. 2007 (1881 1984) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/140684)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.01 (L/28136)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.61 - Classe 3
Sollecitazioni: N=3107.93
Tensioni: σ_N=144.63 σ_M=0.00 τ=0.00 σ_{max}=144.63
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=144.63 σ_M=0.00 τ=0.00 $\sigma_{ID,max}$=144.63

Asta n. 2008 (1882 1985) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/52756)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/9702)

- Verifica a compressione (4.2.10) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-7138.08
N,Ed=-7138.08 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.10

Asta n. 2009 (1985 1881) Cir. D=4 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 1 - Classe 3
Sollecitazioni: N,Ed=-3358.16 M,Ed=4.05
Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=259.36
λ=259.36 Ncr=3872.04 λ^*=3.39 Curva c: Φ=7.04 χ,min=0.08
χ,min=0.08
Verifica: 1.04 + 0.14 = 1.19

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/118240)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.14 (L/1811) $f_{Z,G}$=0.09 (L/2978)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.29 - Classe 3
  Sollecitazioni: N=-5228.54 M=5.39
  Tensioni: σ_N=-416.07 σ_M=-85.86 τ=0.00 σ_{max}=-501.93
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-416.07 σ_M=-85.86 τ=0.00 $\sigma_{ID,max}$=501.93

Asta n. 2010 (1984 1882) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 25 - Classe 3
  L_{cr}=2.10 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
  $\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
  CC 25 My,Ed=-5.68 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 23 - Classe 3
  Sollecitazioni: N,Ed=-469.48 M,Ed=3.28
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=209.96
  λ=209.96 Ncr=5908.50 λ^*=2.75 Curva c: Φ=4.90 χ,min=0.11
  χ,min=0.11
  Verifica: 0.10 + 0.02 = 0.12

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/183461)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.08 (L/2762) $f_{Z,G}$=0.06 (L/3256)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.05 - Classe 3
  Sollecitazioni: N=6747.00 M=4.37
  Tensioni: σ_N=536.91 σ_M=69.51 τ=0.00 σ_{max}=606.41
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=536.91 σ_M=69.51 τ=0.00 $\sigma_{ID,max}$=606.41

Asta n. 2011 (1878 1982) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/140684)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/23447)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.61 - Classe 3
  Sollecitazioni: N=4002.19
  Tensioni: σ_N=186.25 σ_M=0.00 τ=0.00 σ_{max}=186.25
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=186.25 σ_M=0.00 τ=0.00 $\sigma_{ID,max}$=186.25

Asta n. 2012 (1879 1983) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3993.95 M,Ed=0.00
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=161.00
  αmy, αmz, αLT = 0.95, ----, ----
  λ=39.89 Ncr=279894.00 λ^*=0.52
  Curva a: Φ=0.67 χ,min=0.92
  Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
  Verifica: 0.05 = 0.05

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/84410)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/15073)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3993.95
  N,Ed=-3993.95 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.05

Asta n. 2013 (1878 1983) Cir. D=4 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 1 - Classe 3
  Sollecitazioni: N,Ed=-2565.39 M,Ed=4.05
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=259.36
  λ=259.36 Ncr=3872.04 λ^*=3.39 Curva c: Φ=7.04 χ,min=0.08
  χ,min=0.08
  Verifica: 0.80 + 0.06 = 0.85

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/135976)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.14 (L/1810) $f_{Z,G}$=0.10 (L/2627)

- Verifica in termini tensionali (4.2.5) - CC 1 Xl=1.29 - Classe 3
  Sollecitazioni: N=-2555.72 M=5.39
  Tensioni: σ_N=-203.38 σ_M=-85.86 τ=0.00 σ_{max}=-289.24
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-203.38 σ_M=-85.86 τ=0.00 $\sigma_{ID,max}$=289.24

Asta n. 2014 (1879 1982) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 25 - Classe 3
  L_{cr}=2.10 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
  $\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
  CC 25 My,Ed=-5.68 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/137595)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.08 (L/2765) $f_{Z,G}$=0.06 (L/3706)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.05 - Classe 3
  Sollecitazioni: N=3865.88 M=4.37
  Tensioni: σ_N=307.64 σ_M=69.51 τ=0.00 σ_{max}=377.14
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=307.64 σ_M=69.51 τ=0.00 $\sigma_{ID,max}$=377.14

Asta n. 2015 (1873 1869) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2493.25 M,Ed=2.86
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=102.22
  αmy, αmz, αLT = 0.95, ----, ----
  λ=25.33 Ncr=694405.00 λ^*=0.33
  Curva a: Φ=0.57 χ,min=0.97
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.03 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.51 - Classe 3
  Sollecitazioni: N=-2493.25 M=2.86
  Tensioni: σ_N=-116.03 σ_M=-4.91 τ=0.00 σ_{max}=-120.94
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-116.03 σ_M=-4.91 τ=0.00 $\sigma_{ID,max}$=120.94

Asta n. 2016 (1869 1871) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2848.85 M,Ed=4.01
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=120.97
  αmy, αmz, αLT = 0.95, ----, ----
  λ=29.97 Ncr=495807.00 λ^*=0.39
  Curva a: Φ=0.60 χ,min=0.95
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.60 - Classe 3
  Sollecitazioni: N=-2848.85 M=4.01
  Tensioni: σ_N=-132.58 σ_M=-6.88 τ=0.00 σ_{max}=-139.45
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-132.58 σ_M=-6.88 τ=0.00 $\sigma_{ID,max}$=139.45

Asta n. 2017 (1871 1867) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2447.50 M,Ed=2.89
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=102.73
  αmy, αmz, αLT = 0.95, ----, ----
  λ=25.45 Ncr=687495.00 λ^*=0.33
  Curva a: Φ=0.57 χ,min=0.97
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----

Verifica: 0.03 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.51 - Classe 3
  Sollecitazioni: N=-2447.50 M=2.89
  Tensioni: σ_N=-113.90 σ_M=-4.96 τ=0.00 σ_{max}=-118.86
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-113.90 σ_M=-4.96 τ=0.00 $\sigma_{ID,max}$=118.86

Asta n. 2018 (1867 1873) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2858.62 M,Ed=3.97
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=120.28
  αmy, αmz, αLT = 0.95, ----, ----
  λ=29.80 Ncr=501462.00 λ^*=0.39
  Curva a: Φ=0.60 χ,min=0.96
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.60 - Classe 3
  Sollecitazioni: N=-2858.62 M=3.97
  Tensioni: σ_N=-133.03 σ_M=-6.80 τ=0.00 σ_{max}=-139.83
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-133.03 σ_M=-6.80 τ=0.00 $\sigma_{ID,max}$=139.83

Asta n. 2101 (1873 1880) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7047.04 My,Ed=396.01 Mz,Ed=-4885.96
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=526.58
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.27 Curva b: α-imp=0.34 k_c=0.94 ψ=1.74 M,cr=56924.60 λ_{LT}=0.56
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
  λ_Y=73.65 Ncr,y=325125.00 λ^*_y=0.96 Curva b: Φ_y=1.09 χ_y=0.62
  λ_Z=100.89 Ncr,z=173260.00 λ^*_z=1.32 Curva c: Φ_z=1.65 χ_z=0.38
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
  Verifica YY: 0.04 + 0.02 + 0.77 = 0.83
  Verifica ZZ: 0.06 + 0.02 + 0.77 = 0.85

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/39160) $f_{Z,L}$=0.01 (L/52090)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.09 (L/6067) $f_{Z,L}$=0.06 (L/9051)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=5.27 - Classe 3
  Sollecitazioni: N=-6595.49 T_z=-74.41 M_y=396.01 T_y=-1638.39 M_z=-4885.96
  Tensioni: σ_N=-77.51 σ_M=-2714.46 τ=0.00 σ_{max}=-2791.97
  Tensioni: σ_N=-77.51 σ_M=-253.57 τ=31.36 τ_{max}=31.36
  Tensioni: σ_N=-77.51 σ_M=-2714.46 τ=0.00 $\sigma_{ID,max}$=2791.97

Asta n. 2102 (1867 1883) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-18793.20 My,Ed=-380.80 Mz,Ed=-2653.48
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=553.99
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.54 Curva b: α-imp=0.34 k_c=0.94 ψ=1.59 M,cr=48907.50 λ_{LT}=0.60
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.67 β_{LT}=0.75 f=0.97 χ_{LT}=0.94
  λ_Y=77.48 Ncr,y=293755.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
  λ_Z=106.14 Ncr,z=156543.00 λ^*_z=1.39 Curva c: Φ_z=1.76 χ_z=0.35
  Kyy, Kyz, Kzy, Kzz = 1.01, 1.06, 0.81, 1.06
  Verifica YY: 0.11 + 0.02 + 0.45 = 0.58
  Verifica ZZ: 0.18 + 0.02 + 0.45 = 0.65

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.02 (L/33577) $f_{Z,L}$=0.00 (L/161359)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.09 (L/5909) $f_{Z,L}$=0.02 (L/29943)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-18793.20 T_z=78.97 M_y=60.35 T_y=778.41 M_z=-2653.48 M_x=-8.17
  Tensioni: σ_N=-220.86 σ_M=-1443.05 τ=8.19 σ_{max}=-1663.91
  Tensioni: σ_N=-220.86 σ_M=-112.76 τ=31.76 τ_{max}=31.76

Tensioni: σ_N=-220.86 σ_M=-1443.05 τ=8.19 $\sigma_{ID,max}$=1663.97

Asta n. 2103 (1871 1877) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7037.17 My,Ed=97.18 Mz,Ed=-4891.25
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=526.43
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.26 Curva b: α-imp=0.34 k_c=0.94 ψ=1.13 M,cr=37158.80 λ_{LT}=0.69
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.73 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
  λ_Y=73.63 Ncr,y=325318.00 λ^*_y=0.96 Curva b: Φ_y=1.09 χ_y=0.62
  λ_Z=100.86 Ncr,z=173363.00 λ^*_z=1.32 Curva c: Φ_z=1.65 χ_z=0.38
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
  Verifica YY: 0.04 + 0.01 + 0.77 = 0.82
  Verifica ZZ: 0.06 + 0.00 + 0.77 = 0.84

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/39999)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.09 (L/6160) $f_{Z,L}$=0.01 (L/62726)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=5.26 - Classe 3
  Sollecitazioni: N=-6585.62 T_z=-32.20 M_y=97.18 T_y=-1648.33 M_z=-4891.25 M_x=6.79
  Tensioni: σ_N=-77.39 σ_M=-2657.20 τ=6.81 σ_{max}=-2734.59
  Tensioni: σ_N=-77.39 σ_M=-205.58 τ=38.57 τ_{max}=38.57
  Tensioni: σ_N=-77.39 σ_M=-2657.20 τ=6.81 $\sigma_{ID,max}$=2734.62

Asta n. 2104 (1869 1874) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-18064.80 My,Ed=-276.58 Mz,Ed=-2597.32
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=553.99
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.54 Curva b: α-imp=0.34 k_c=0.94 ψ=1.54 M,cr=47430.70 λ_{LT}=0.61
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.68 β_{LT}=0.75 f=0.97 χ_{LT}=0.94
  λ_Y=77.48 Ncr,y=293755.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
  λ_Z=106.14 Ncr,z=156543.00 λ^*_z=1.39 Curva c: Φ_z=1.76 χ_z=0.35
  Kyy, Kyz, Kzy, Kzz = 1.01, 1.05, 0.81, 1.05
  Verifica YY: 0.11 + 0.02 + 0.44 = 0.56
  Verifica ZZ: 0.18 + 0.01 + 0.44 = 0.63

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.02 (L/36765)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.09 (L/6483) $f_{Z,L}$=0.01 (L/58089)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-18064.80 T_z=58.68 M_y=57.97 T_y=756.24 M_z=-2597.32 M_x=-8.42
  Tensioni: σ_N=-212.30 σ_M=-1412.29 τ=8.44 σ_{max}=-1624.59
  Tensioni: σ_N=-212.30 σ_M=-110.19 τ=31.72 τ_{max}=31.72
  Tensioni: σ_N=-212.30 σ_M=-1412.29 τ=8.44 $\sigma_{ID,max}$=1624.65

Asta n. 2105 (-836 1986) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-11687.60 M,Ed=0.12
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=78.22
  αmy, αmz, αLT = 0.95, ----, ----
  λ=19.38 Ncr=1185880.00 λ^*=0.25
  Curva a: Φ=0.54 χ,min=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
  Verifica: 0.16 + 0.00 = 0.16

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/27338)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/5126)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-11687.60
  N,Ed=-11687.60 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.16

Asta n. 2106 (-839 1987) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-10826.70 M,Ed=0.29
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=66.17
  αmy, αmz, αLT = 0.95, ----, ----
  λ=16.39 Ncr=1657040.00 λ^*=0.21
  Curva a: Φ=0.52 χ,min=1.00
  Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
  Verifica: 0.15 + 0.00 = 0.15

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/31537)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/5981)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-10826.70 T=1.76
  N,Ed=-10826.70 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.15

Asta n. 2211 (1880 1882) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3311.94 My,Ed=1262.78 Mz,Ed=-2001.13
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=379.60
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=3.80 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=39930.60 λ_{LT}=0.51
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.62 β_{LT}=0.75 f=0.98 χ_{LT}=0.98
  λ_Y=62.61 Ncr,y=307021.00 λ^*_y=0.82 Curva b: Φ_y=0.94 χ_y=0.71
  λ_Z=83.04 Ncr,z=174529.00 λ^*_z=1.09 Curva c: Φ_z=1.31 χ_z=0.49
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
  Verifica YY: 0.02 + 0.13 + 0.51 = 0.65
  Verifica ZZ: 0.02 + 0.10 + 0.51 = 0.63

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.06 (L/6611) $f_{Z,L}$=0.03 (L/10935)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.32 (L/1184) $f_{Z,L}$=0.20 (L/1945)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3311.94 T_z=332.66 M_y=1262.78 T_y=596.84 M_z=-2001.13
  Tensioni: σ_N=-57.04 σ_M=-2204.81 τ=0.00 σ_{max}=-2261.84
  Tensioni: σ_N=-57.04 σ_M=-451.96 τ=23.44 τ_{max}=23.44
  Tensioni: σ_N=-57.04 σ_M=-2204.81 τ=0.00 $\sigma_{ID,max}$=2261.84

Asta n. 2212 (1880 1881) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3546.39 My,Ed=-1161.13 Mz,Ed=-2509.04
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=334.12
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=3.34 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=47739.80 λ_{LT}=0.47
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.59 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=55.11 Ncr,y=396295.00 λ^*_y=0.72 Curva b: Φ_y=0.85 χ_y=0.77
  λ_Z=73.09 Ncr,z=225278.00 λ^*_z=0.96 Curva c: Φ_z=1.14 χ_z=0.57
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
  Verifica YY: 0.02 + 0.11 + 0.64 = 0.77
  Verifica ZZ: 0.02 + 0.09 + 0.64 = 0.74

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.06 (L/5917) $f_{Z,L}$=0.02 (L/13429)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.32 (L/1045) $f_{Z,L}$=0.14 (L/2397)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3546.39 T_z=-347.52 M_y=-1161.13 T_y=812.38 M_z=-2509.04
  Tensioni: σ_N=-61.07 σ_M=-2620.03 τ=0.00 σ_{max}=-2681.10
  Tensioni: σ_N=-61.07 σ_M=182.60 τ=28.08 τ_{max}=28.08
  Tensioni: σ_N=-61.07 σ_M=-2620.03 τ=0.00 $\sigma_{ID,max}$=2681.10

Asta n. 2212 (1883 1885) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-11748.90 My,Ed=680.80 Mz,Ed=234.28

Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=437.01
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.37 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=33075.30 λ_{LT}=0.56
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_y=72.08 Ncr,y=231652.00 λ^*_y=0.94 Curva b: Φ_y=1.07 χ_y=0.63
λ_z=95.60 Ncr,z=131685.00 λ^*_z=1.25 Curva c: Φ_z=1.54 χ_z=0.41
Kyy, Kyz, Kzy, Kzz = 1.00, 1.03, 0.80, 1.03
Verifica YY: 0.09 + 0.07 + 0.06 = 0.23
Verifica ZZ: 0.15 + 0.06 + 0.06 = 0.27

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.02 (L/19093) $f_{Z,G}$=0.01 (L/34979)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.14 (L/3110) $f_{Z,G}$=0.08 (L/5353)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-11748.90 T_z=155.79 M_y=680.80 T_y=17.81 M_z=229.35
Tensioni: σ_N=-202.33 σ_M=-436.03 τ=0.00 σ_{max}=-638.36
Tensioni: σ_N=-202.33 σ_M=12.29 τ=9.38 τ_{max}=9.38
Tensioni: σ_N=-202.33 σ_M=-436.03 τ=0.00 $\sigma_{ID,max}$=638.36

Asta n. 2213 (1877 1878) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3197.92 My,Ed=1059.83 Mz,Ed=-2077.08
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=352.04
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.52 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=44330.50 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_y=58.06 Ncr,y=356964.00 λ^*_y=0.76 Curva b: Φ_y=0.88 χ_y=0.75
λ_z=77.01 Ncr,z=202920.00 λ^*_z=1.01 Curva c: Φ_z=1.21 χ_z=0.54
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.10 + 0.53 = 0.65
Verifica ZZ: 0.02 + 0.08 + 0.53 = 0.63

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.06 (L/6353) $f_{Z,L}$=0.03 (L/13982)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.31 (L/1130) $f_{Z,L}$=0.14 (L/2514)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3197.92 T_z=301.05 M_y=1059.83 T_y=659.68 M_z=-2077.08
Tensioni: σ_N=-55.07 σ_M=-2202.69 τ=0.00 σ_{max}=-2257.76
Tensioni: σ_N=-55.07 σ_M=-400.62 τ=23.45 τ_{max}=23.45
Tensioni: σ_N=-55.07 σ_M=-2202.69 τ=0.00 $\sigma_{ID,max}$=2257.76

Asta n. 2214 (1874 1876) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-8889.56 My,Ed=-876.50 Mz,Ed=-186.53
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=448.31
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.48 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=31994.10 λ_{LT}=0.57
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.65 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_y=73.94 Ncr,y=220115.00 λ^*_y=0.97 Curva b: Φ_y=1.10 χ_y=0.62
λ_z=98.07 Ncr,z=125127.00 λ^*_z=1.28 Curva c: Φ_z=1.59 χ_z=0.40
Kyy, Kyz, Kzy, Kzz = 0.99, 1.02, 0.79, 1.02
Verifica YY: 0.07 + 0.09 + 0.05 = 0.21
Verifica ZZ: 0.11 + 0.07 + 0.05 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.03 (L/14138) $f_{Z,G}$=0.00 (L/134311)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.19 (L/2356) $f_{Z,G}$=0.02 (L/23504)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-8889.56 T_z=-195.51 M_y=-876.50 T_y=123.11 M_z=-186.53
Tensioni: σ_N=-153.09 σ_M=-465.02 τ=0.00 σ_{max}=-618.12
Tensioni: σ_N=-153.09 σ_M=-9.99 τ=11.78 τ_{max}=11.78
Tensioni: σ_N=-153.09 σ_M=-465.02 τ=0.00 $\sigma_{ID,max}$=618.12

Asta n. 2222 (1883 1884) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-9657.34 My,Ed=-734.33 Mz,Ed=-164.30
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=458.65
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=4.59 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=31066.50 λ_{LT}=0.58
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
  λ_Y=75.65 Ncr,y=210307.00 λ^*_y=0.99 Curva b: Φ_y=1.12 χ_y=0.60
  λ_Z=100.33 Ncr,z=119551.00 λ^*_z=1.31 Curva c: Φ_z=1.63 χ_z=0.38
  Kyy, Kyz, Kzy, Kzz = 1.00, 1.02, 0.80, 1.02
  Verifica YY: 0.08 + 0.08 + 0.04 = 0.20
  Verifica ZZ: 0.13 + 0.06 + 0.04 = 0.23

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.03 (L/16703) $f_{Z,G}$=0.00 (L/114506)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.17 (L/2755) $f_{Z,G}$=0.02 (L/21469)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-9657.34 T_z=-160.11 M_y=-734.33 T_y=117.33 M_z=-164.30
  Tensioni: σ_N=-166.31 σ_M=-396.71 τ=0.00 σ_{max}=-563.02
  Tensioni: σ_N=-166.31 σ_M=-8.80 τ=9.66 τ_{max}=9.66
  Tensioni: σ_N=-166.31 σ_M=-396.71 τ=0.00 $\sigma_{ID,max}$=563.02

Asta n. 2223 (1877 1879) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3657.46 My,Ed=-1201.20 Mz,Ed=-2482.30
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=363.03
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=3.63 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=42465.80 λ_{LT}=0.49
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.61 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=59.88 Ncr,y=335675.00 λ^*_y=0.78 Curva b: Φ_y=0.91 χ_y=0.73
  λ_Z=79.42 Ncr,z=190818.00 λ^*_z=1.04 Curva c: Φ_z=1.25 χ_z=0.52
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
  Verifica YY: 0.02 + 0.12 + 0.63 = 0.77
  Verifica ZZ: 0.02 + 0.09 + 0.63 = 0.74

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.06 (L/5985) $f_{Z,L}$=0.03 (L/11989)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.34 (L/1062) $f_{Z,L}$=0.17 (L/2126)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3657.46 T_z=-330.88 M_y=-1201.20 T_y=745.20 M_z=-2482.30
  Tensioni: σ_N=-62.99 σ_M=-2610.05 τ=0.00 σ_{max}=-2673.04
  Tensioni: σ_N=-62.99 σ_M=194.97 τ=26.17 τ_{max}=26.17
  Tensioni: σ_N=-62.99 σ_M=-2610.05 τ=0.00 $\sigma_{ID,max}$=2673.04

Asta n. 2224 (1874 1875) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-11046.50 My,Ed=522.92 Mz,Ed=258.63
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=426.15
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=4.26 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=34185.30 λ_{LT}=0.55
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
  λ_Y=70.29 Ncr,y=243609.00 λ^*_y=0.92 Curva b: Φ_y=1.05 χ_y=0.65
  λ_Z=93.22 Ncr,z=138482.00 λ^*_z=1.22 Curva c: Φ_z=1.49 χ_z=0.42
  Kyy, Kyz, Kzy, Kzz = 1.00, 1.03, 0.80, 1.03
  Verifica YY: 0.09 + 0.05 + 0.07 = 0.21
  Verifica ZZ: 0.13 + 0.04 + 0.07 = 0.25

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.02 (L/26285) $f_{Z,G}$=0.01 (L/33597)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.10 (L/4137) $f_{Z,G}$=0.08 (L/5124)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-11046.50 T_z=122.71 M_y=522.92 T_y=9.96 M_z=257.12
  Tensioni: σ_N=-190.24 σ_M=-406.64 τ=0.00 σ_{max}=-596.88
  Tensioni: σ_N=-190.24 σ_M=13.77 τ=7.39 τ_{max}=7.39

Tensioni: σ_N=-190.24 σ_M=-406.64 τ=0.00 $\sigma_{ID,max}$=596.88

Asta n. 2232 (-836 1886) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-4516.80 My,Ed=-87.24 Mz,Ed=-722.05
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=248865.00 λ_{LT}=0.20
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.01 + 0.18 = 0.21
Verifica ZZ: 0.02 + 0.01 + 0.18 = 0.21

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/43189)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/6819) $f_{Z,L}$=0.00 (L/71982)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-4516.80 T_z=-70.60 M_y=-87.24 T_y=617.56 M_z=-722.05
Tensioni: σ_N=-77.79 σ_M=-669.55 τ=0.00 σ_{max}=-747.33
Tensioni: σ_N=-77.79 σ_M=-14.86 τ=16.70 τ_{max}=16.70
Tensioni: σ_N=-77.79 σ_M=-669.55 τ=0.00 $\sigma_{ID,max}$=747.33

Asta n. 2232 (-835 -836) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3108.30 My,Ed=-87.24 Mz,Ed=-722.05
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.15 M,cr=163740.00 λ_{LT}=0.25
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.02 + 0.01 + 0.18 = 0.20
Verifica ZZ: 0.02 + 0.01 + 0.18 = 0.20

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/30132)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/5332) $f_{Z,L}$=0.00 (L/46274)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.24 - Classe 3
Sollecitazioni: N=-3077.49 T_z=19.98 M_y=-87.24 T_y=-429.80 M_z=-722.05
Tensioni: σ_N=-53.00 σ_M=-669.55 τ=0.00 σ_{max}=-722.55
Tensioni: σ_N=-53.00 σ_M=-14.86 τ=11.38 τ_{max}=11.38
Tensioni: σ_N=-53.00 σ_M=-669.55 τ=0.00 $\sigma_{ID,max}$=722.55

Asta n. 2232 (-834 -835) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 - Classe 3
Sollecitazioni: N,Ed=-2433.56 My,Ed=-257.23 Mz,Ed=-172.02
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.10 M,cr=156771.00 λ_{LT}=0.26
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01 + 0.02 + 0.04 = 0.08
Verifica ZZ: 0.01 + 0.02 + 0.04 = 0.08

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.00 (L/64784) $f_{Z,G}$=0.00 (L/92548)

- Verifica in termini tensionali (4.2.5) - CC 1 Xl=1.24 - Classe 3
Sollecitazioni: N=-2409.86 T_z=48.51 M_y=-257.23 T_y=-267.77 M_z=-172.02
Tensioni: σ_N=-41.50 σ_M=-240.38 τ=0.00 σ_{max}=-281.88
Tensioni: σ_N=-41.50 σ_M=61.01 τ=7.50 τ_{max}=7.50

Tensioni: σ_N=-41.50 σ_M=-240.38 τ=0.00 $\sigma_{ID,max}$=281.88

Asta n. 2232 (-833 -834) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3169.93 My,Ed=-37.85 Mz,Ed=501.87
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.42 M,cr=202110.00 λ_{LT}=0.23
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.00 + 0.13 = 0.15
  Verifica ZZ: 0.02 + 0.00 + 0.13 = 0.14

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/44678)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/6678)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3169.93 T_z=19.98 M_y=-13.16 T_y=-230.54 M_z=501.87
  Tensioni: σ_N=-54.59 σ_M=-449.14 τ=0.00 σ_{max}=-503.73
  Tensioni: σ_N=-54.59 σ_M=30.48 τ=6.17 τ_{max}=6.17
  Tensioni: σ_N=-54.59 σ_M=-449.14 τ=0.00 $\sigma_{ID,max}$=503.73

Asta n. 2232 (1883 -833) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3200.74 My,Ed=-13.16 Mz,Ed=745.70
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.06 M,cr=150772.00 λ_{LT}=0.26
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.00 + 0.19 = 0.20
  Verifica ZZ: 0.02 + 0.00 + 0.19 = 0.20

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/20245)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.03 (L/3777)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3200.74 T_z=19.98 M_y=11.53 T_y=-164.11 M_z=745.70
  Tensioni: σ_N=-55.12 σ_M=-664.61 τ=0.00 σ_{max}=-719.73
  Tensioni: σ_N=-55.12 σ_M=36.80 τ=4.45 τ_{max}=4.45
  Tensioni: σ_N=-55.12 σ_M=-664.61 τ=0.00 $\sigma_{ID,max}$=719.73

Asta n. 2234 (1874 -832) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3886.90 My,Ed=264.83 Mz,Ed=598.14
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.66 M,cr=176022.00 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.02 + 0.03 + 0.15 = 0.20
  Verifica ZZ: 0.02 + 0.02 + 0.15 = 0.19

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/23779) $f_{Z,L}$=0.00 (L/126824)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.03 (L/4489) $f_{Z,L}$=0.01 (L/22380)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3886.90 T_z=166.44 M_y=264.83 T_y=-82.68 M_z=598.14

Tensioni: σ_N=-66.94 σ_M=-620.50 τ=0.00 σ_{max}=-687.44
Tensioni: σ_N=-66.94 σ_M=32.04 τ=10.03 τ_{max}=10.03
Tensioni: σ_N=-66.94 σ_M=-620.50 τ=0.00 $\sigma_{ID,max}$=687.44

Asta n. 2234 (-832 -837) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3832.27 My,Ed=-218.31 Mz,Ed=429.93
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.64 M,cr=174054.00 λ_{LT}=0.24
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.02 + 0.11 = 0.15
Verifica ZZ: 0.02 + 0.02 + 0.11 = 0.14

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/54353)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/7387) $f_{Z,L}$=0.00 (L/33084)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3832.27 T_z=166.44 M_y=23.26 T_y=-149.10 M_z=429.93
Tensioni: σ_N=-66.00 σ_M=-388.86 τ=0.00 σ_{max}=-454.86
Tensioni: σ_N=-66.00 σ_M=23.03 τ=10.05 τ_{max}=10.05
Tensioni: σ_N=-66.00 σ_M=-388.86 τ=0.00 $\sigma_{ID,max}$=454.86

Asta n. 2234 (-837 -838) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3777.63 My,Ed=-459.88 Mz,Ed=-195.70
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.32 M,cr=139872.00 λ_{LT}=0.27
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.04 + 0.05 = 0.11
Verifica ZZ: 0.02 + 0.04 + 0.05 = 0.10

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.00 (L/54353)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.01 (L/9882) $f_{Z,G}$=0.00 (L/76094)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.45 - Classe 3
Sollecitazioni: N=-3723.00 T_z=166.44 M_y=-459.88 T_y=-281.95 M_z=-195.70
Tensioni: σ_N=-64.12 σ_M=-330.66 τ=0.00 σ_{max}=-394.78
Tensioni: σ_N=-64.12 σ_M=115.07 τ=11.44 τ_{max}=11.44
Tensioni: σ_N=-64.12 σ_M=-330.66 τ=0.00 $\sigma_{ID,max}$=394.78

Asta n. 2234 (-838 -839) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3723.00 My,Ed=-701.45 Mz,Ed=-653.12
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.19 M,cr=126236.00 λ_{LT}=0.29
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.07 + 0.16 = 0.25
Verifica ZZ: 0.02 + 0.05 + 0.16 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.00 (L/31706) $f_{Z,G}$=0.00 (L/36235)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.03 (L/5764) $f_{Z,G}$=0.02 (L/6112)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.45 - Classe 3
  Sollecitazioni: N=-3668.36 T_z=166.44 M_y=-701.45 T_y=-348.37 M_z=-653.12
  Tensioni: σ_N=-63.17 σ_M=-818.54 τ=0.00 σ_{max}=-881.71
  Tensioni: σ_N=-63.17 σ_M=156.52 τ=12.65 τ_{max}=12.65
  Tensioni: σ_N=-63.17 σ_M=-818.54 τ=0.00 $\sigma_{ID,max}$=881.71

Asta n. 2234 (-839 1887) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7638.74 My,Ed=-701.45 Mz,Ed=-653.12
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=185554.00 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.96, 0.77, 0.96
  Verifica YY: 0.04 + 0.07 + 0.16 = 0.27
  Verifica ZZ: 0.04 + 0.05 + 0.16 = 0.26

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.00 (L/44761) $f_{Z,G}$=0.00 (L/50729)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/8009) $f_{Z,L}$=0.02 (L/8549)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-7638.74 T_z=-483.29 M_y=-701.45 T_y=483.21 M_z=-653.12
  Tensioni: σ_N=-131.55 σ_M=-818.54 τ=0.00 σ_{max}=-950.09
  Tensioni: σ_N=-131.55 σ_M=-34.99 τ=29.20 τ_{max}=29.20
  Tensioni: σ_N=-131.55 σ_M=-818.54 τ=0.00 $\sigma_{ID,max}$=950.09

Asta n. 3001 (1894 1895) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-5415.91 My,Ed=-4122.03 Mz,Ed=2800.89
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=700.73
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.01 Curva b: α-imp=0.34 k_c=0.94 ψ=1.46 M,cr=33849.90 λ_{LT}=0.72
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.75 β_{LT}=0.75 f=0.97 χ_{LT}=0.88
  λ_Y=98.01 Ncr,y=183603.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.44
  λ_Z=134.26 Ncr,z=97842.80 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
  Verifica YY: 0.04 + 0.27 + 0.44 = 0.76
  Verifica ZZ: 0.08 + 0.22 + 0.44 = 0.74

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/89606) $f_{Z,L}$=0.01 (L/116630)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.05 (L/15403) $f_{Z,L}$=0.03 (L/20297)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-5415.91 T_z=-767.44 M_y=-4122.03 T_y=715.00 M_z=-2134.64 M_x=-58.78
  Tensioni: σ_N=-63.65 σ_M=-1980.31 τ=58.91 σ_{max}=-2043.96
  Tensioni: σ_N=-63.65 σ_M=-747.66 τ=208.62 τ_{max}=208.62
  Tensioni: σ_N=-63.65 σ_M=-1980.31 τ=58.91 $\sigma_{ID,max}$=2046.51

Asta n. 3002 (1888 1889) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-19741.50 My,Ed=-628.58 Mz,Ed=3651.13
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=702.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.02 Curva b: α-imp=0.34 k_c=0.94 ψ=1.61 M,cr=37347.70 λ_{LT}=0.69
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.73 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
  λ_Y=98.21 Ncr,y=182868.00 λ^*_y=1.29 Curva b: Φ_y=1.51 χ_y=0.43
  λ_Z=134.53 Ncr,z=97451.20 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 1.04, 1.11, 0.83, 1.11
  Verifica YY: 0.16 + 0.04 + 0.65 = 0.85
  Verifica ZZ: 0.28 + 0.03 + 0.65 = 0.96

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.01 (L/54135) $f_{Z,G}$=0.01 (L/73258)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.07 (L/9439) $f_{Z,G}$=0.06 (L/12457)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-19741.50 T_z=-94.49 M_y=-628.58 T_y=-917.16 M_z=3651.13 M_x=5.56
  Tensioni: σ_N=-232.00 σ_M=-2095.35 τ=5.57 σ_{max}=-2327.35
  Tensioni: σ_N=-232.00 σ_M=243.13 τ=26.85 τ_{max}=26.85
  Tensioni: σ_N=-232.00 σ_M=-2095.35 τ=5.57 $\sigma_{ID,max}$=2327.37

Asta n. 3004 (5 6) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7221.88 My,Ed=-241.62 Mz,Ed=3498.60
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=700.78
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.01 Curva b: α-imp=0.34 k_c=0.94 ψ=1.62 M,cr=37658.90 λ_{LT}=0.68
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.72 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
  λ_Y=98.02 Ncr,y=183579.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.44
  λ_Z=134.27 Ncr,z=97829.90 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 0.98, 1.01, 0.79, 1.01
  Verifica YY: 0.06 + 0.02 + 0.56 = 0.64
  Verifica ZZ: 0.10 + 0.01 + 0.56 = 0.68

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.01 (L/57407) $f_{Z,G}$=0.01 (L/89068)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.07 (L/9543) $f_{Z,G}$=0.05 (L/15229)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.01 - Classe 3
  Sollecitazioni: N=-6614.02 T_z=-30.12 M_y=-30.54 T_y=850.95 M_z=3498.60
  Tensioni: σ_N=-77.73 σ_M=-1892.80 τ=0.00 σ_{max}=-1970.52
  Tensioni: σ_N=-77.73 σ_M=140.76 τ=16.27 τ_{max}=16.27
  Tensioni: σ_N=-77.73 σ_M=-1892.80 τ=0.00 $\sigma_{ID,max}$=1970.52

Asta n. 3004 (1890 1891) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-18168.10 My,Ed=-782.56 Mz,Ed=3493.19
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=702.06
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.02 Curva b: α-imp=0.34 k_c=0.94 ψ=1.66 M,cr=38473.30 λ_{LT}=0.68
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.72 β_{LT}=0.75 f=0.97 χ_{LT}=0.91
  λ_Y=98.19 Ncr,y=182908.00 λ^*_y=1.29 Curva b: Φ_y=1.51 χ_y=0.43
  λ_Z=134.51 Ncr,z=97472.40 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 1.03, 1.10, 0.83, 1.10
  Verifica YY: 0.15 + 0.05 + 0.61 = 0.81
  Verifica ZZ: 0.26 + 0.04 + 0.61 = 0.91

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.02 (L/43819) $f_{Z,G}$=0.01 (L/73986)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.09 (L/7668) $f_{Z,G}$=0.06 (L/12605)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-18168.10 T_z=-119.10 M_y=-782.56 T_y=-868.00 M_z=3493.19 M_x=7.29
  Tensioni: σ_N=-213.51 σ_M=-2041.15 τ=7.31 σ_{max}=-2254.66
  Tensioni: σ_N=-213.51 σ_M=261.83 τ=31.31 τ_{max}=31.31
  Tensioni: σ_N=-213.51 σ_M=-2041.15 τ=7.31 $\sigma_{ID,max}$=2254.70

Asta n. 3005 (-876 -844) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/25040)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.07 (L/4546)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-13309.90
  N,Ed=-13309.90 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.18

- Verifica di stabilità (4.2.4.1.3.1) - CC 25
  Sollecitazioni: N=-13309.90 L=320.00

λ=79.28 Ncr=70851.00 λ^*=1.04
Curva a: Φ=1.13 χ,min=0.64 N,Ed=-13309.90 Nb,Rd=46443.40 N,Ed/Nb,Rd=0.29

Asta n. 3006 (-877 -847) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/24314)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.04 (L/4462)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-13678.70
N,Ed=-13678.70 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.19

- Verifica di stabilità (4.2.4.1.3.1) - CC 25
Sollecitazioni: N=-13678.70 L=160.00
λ=39.64 Ncr=283404.00 λ^*=0.52
Curva a: Φ=0.67 χ,min=0.92 N,Ed=-13678.70 Nb,Rd=66718.00 N,Ed/Nb,Rd=0.21

Asta n. 3007 (1903 1990) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/140684)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.01 (L/29107)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.61 - Classe 3
Sollecitazioni: N=2089.72
Tensioni: σ_N=97.25 σ_M=0.00 τ=0.00 σ_{max}=97.25
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=97.25 σ_M=0.00 τ=0.00 $\sigma_{ID,max}$=97.25

Asta n. 3008 (1904 1991) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/52756)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/9815)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-6178.15
N,Ed=-6178.15 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.09

Asta n. 3009 (1991 1903) Cir. D=4 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-3295.47 M,Ed=4.05
Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=259.36
λ=259.36 Ncr=3872.04 λ^*=3.39 Curva c: Φ=7.04 χ,min=0.08
χ,min=0.08
Verifica: 1.02 + 0.13 = 1.15

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/135976)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.14 (L/1810) $f_{Z,G}$=0.09 (L/2965)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.29 - Classe 3
Sollecitazioni: N=-3285.70 M=5.39
Tensioni: σ_N=-261.47 σ_M=-85.86 τ=0.00 σ_{max}=-347.32
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=-261.47 σ_M=-85.86 τ=0.00 $\sigma_{ID,max}$=347.32

Asta n. 3010 (1990 1904) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 25 - Classe 3
L_{cr}=2.10 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
$\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
CC 25 My,Ed=-5.68 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/183461)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.08 (L/2758) $f_{Z,G}$=0.06 (L/3256)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.05 - Classe 3
  Sollecitazioni: N=3903.82 M=4.37
  Tensioni: σ_N=310.66 σ_M=69.51 τ=0.00 σ_{max}=380.16
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=310.66 σ_M=69.51 τ=0.00 $\sigma_{ID,max}$=380.16

Asta n. 3011 (1900 1988) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/120586)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/22813)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.61 - Classe 3
  Sollecitazioni: N=2666.03
  Tensioni: σ_N=124.07 σ_M=0.00 τ=0.00 σ_{max}=124.07
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=124.07 σ_M=0.00 τ=0.00 $\sigma_{ID,max}$=124.07

Asta n. 3012 (1901 1989) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-4298.44 M,Ed=0.00
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=161.00
  αmy, αmz, αLT = 0.95, ----, ----
  λ=39.89 Ncr=279894.00 λ^*=0.52
  Curva a: Φ=0.67 χ,min=0.92
  Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
  Verifica: 0.06 = 0.06

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/93789)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/15347)

- Verifica a compressione (4.2.10) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-4298.44
  N,Ed=-4298.44 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.06

Asta n. 3013 (1900 1989) Cir. D=4 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-3461.10 M,Ed=4.05
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=259.36
  λ=259.36 Ncr=3872.04 λ^*=3.39 Curva c: Φ=7.04 χ,min=0.08
  χ,min=0.08
  Verifica: 1.08 + 0.18 = 1.26

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/135976)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.14 (L/1815) $f_{Z,G}$=0.10 (L/2625)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.30 - Classe 3
  Sollecitazioni: N=-3451.39 M=5.39
  Tensioni: σ_N=-274.65 σ_M=-85.86 τ=0.00 σ_{max}=-360.51
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-274.65 σ_M=-85.86 τ=0.00 $\sigma_{ID,max}$=360.51

Asta n. 3014 (1901 1988) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 25 - Classe 3
  L_{cr}=2.10 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
  $\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
  CC 25 My,Ed=-5.68 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/110076)

- Verifica Freccia massima carichi totali - CC 26

$f_{Z,L}$=0.08 (L/2769) $f_{Z,G}$=0.06 (L/3725)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.05 - Classe 3
  Sollecitazioni: N=4385.51 M=4.37
  Tensioni: σ_N=348.99 σ_M=69.51 τ=0.00 σ_{max}=418.49
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=348.99 σ_M=69.51 τ=0.00 $\sigma_{ID,max}$=418.49

Asta n. 3015 (1895 1891) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2502.19 M,Ed=2.86
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=102.22
  αmy, αmz, αLT = 0.95, ----, ----
  λ=25.33 Ncr=694405.00 λ^*=0.33
  Curva a: Φ=0.57 χ,min=0.97
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.03 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.51 - Classe 3
  Sollecitazioni: N=-2502.19 M=2.86
  Tensioni: σ_N=-116.44 σ_M=-4.91 τ=0.00 σ_{max}=-121.35
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-116.44 σ_M=-4.91 τ=0.00 $\sigma_{ID,max}$=121.35

Asta n. 3016 (1891 1893) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2856.52 M,Ed=4.01
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=120.97
  αmy, αmz, αLT = 0.95, ----, ----
  λ=29.97 Ncr=495807.00 λ^*=0.39
  Curva a: Φ=0.60 χ,min=0.95
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.60 - Classe 3
  Sollecitazioni: N=-2856.52 M=4.01
  Tensioni: σ_N=-132.93 σ_M=-6.88 τ=0.00 σ_{max}=-139.81
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-132.93 σ_M=-6.88 τ=0.00 $\sigma_{ID,max}$=139.81

Asta n. 3017 (1893 1889) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2453.59 M,Ed=2.89
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=102.73
  αmy, αmz, αLT = 0.95, ----, ----
  λ=25.45 Ncr=687495.00 λ^*=0.33
  Curva a: Φ=0.57 χ,min=0.97
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.03 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.51 - Classe 3
  Sollecitazioni: N=-2453.59 M=2.89
  Tensioni: σ_N=-114.18 σ_M=-4.96 τ=0.00 σ_{max}=-119.14
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-114.18 σ_M=-4.96 τ=0.00 $\sigma_{ID,max}$=119.14

Asta n. 3018 (1889 1895) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2863.89 M,Ed=3.97
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=120.28
  αmy, αmz, αLT = 0.95, ----, ----
  λ=29.80 Ncr=501462.00 λ^*=0.39
  Curva a: Φ=0.60 χ,min=0.96
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.60 - Classe 3
  Sollecitazioni: N=-2863.89 M=3.97
  Tensioni: σ_N=-133.28 σ_M=-6.80 τ=0.00 σ_{max}=-140.07
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-133.28 σ_M=-6.80 τ=0.00 $\sigma_{ID,max}$=140.07

Asta n. 3101 (1895 1902) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7066.43 My,Ed=405.49 Mz,Ed=-4901.65
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=526.58
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.27 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=57274.10 λ_{LT}=0.56
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
  λ_Y=73.65 Ncr,y=325125.00 λ^*_y=0.96 Curva b: Φ_y=1.09 χ_y=0.62
  λ_z=100.89 Ncr,z=173260.00 λ^*_z=1.32 Curva c: Φ_z=1.65 χ_z=0.38
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
  Verifica YY: 0.04 + 0.02 + 0.77 = 0.84
  Verifica ZZ: 0.06 + 0.02 + 0.77 = 0.86

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/38884) $f_{Z,L}$=0.01 (L/50657)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.09 (L/6034) $f_{Z,L}$=0.06 (L/8905)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=5.27 - Classe 3
  Sollecitazioni: N=-6614.88 T_z=-76.97 M_y=405.49 T_y=-1642.79 M_z=-4901.65
  Tensioni: σ_N=-77.74 σ_M=-2724.83 τ=0.00 σ_{max}=-2802.56
  Tensioni: σ_N=-77.74 σ_M=-255.71 τ=31.44 τ_{max}=31.44
  Tensioni: σ_N=-77.74 σ_M=-2724.83 τ=0.00 $\sigma_{ID,max}$=2802.56

Asta n. 3102 (1889 1905) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-20078.80 My,Ed=-462.65 Mz,Ed=-2918.25
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=553.99
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.54 Curva b: α-imp=0.34 k_c=0.94 ψ=1.64 M,cr=50305.20 λ_{LT}=0.59
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
  λ_Y=77.48 Ncr,y=293755.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
  λ_z=106.14 Ncr,z=156543.00 λ^*_z=1.39 Curva c: Φ_z=1.76 χ_z=0.35
  Kyy, Kyz, Kzy, Kzz = 1.02, 1.06, 0.81, 1.06
  Verifica YY: 0.12 + 0.03 + 0.49 = 0.64
  Verifica ZZ: 0.20 + 0.02 + 0.49 = 0.72

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.02 (L/32818) $f_{Z,L}$=0.00 (L/161359)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.10 (L/5826) $f_{Z,L}$=0.02 (L/29044)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-20078.80 T_z=92.04 M_y=51.61 T_y=839.40 M_z=-2918.25 M_x=-7.31
  Tensioni: σ_N=-235.97 σ_M=-1584.08 τ=7.33 σ_{max}=-1820.04
  Tensioni: σ_N=-235.97 σ_M=-121.63 τ=30.37 τ_{max}=30.37
  Tensioni: σ_N=-235.97 σ_M=-1584.08 τ=7.33 $\sigma_{ID,max}$=1820.09

Asta n. 3103 (1893 1899) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7051.48 My,Ed=97.24 Mz,Ed=-4901.64
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=526.43
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.26 Curva b: α-imp=0.34 k_c=0.94 ψ=1.13 M,cr=37115.80 λ_{LT}=0.69
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.73 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
  λ_Y=73.63 Ncr,y=325318.00 λ^*_y=0.96 Curva b: Φ_y=1.09 χ_y=0.62
  λ_z=100.86 Ncr,z=173363.00 λ^*_z=1.32 Curva c: Φ_z=1.65 χ_z=0.38
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
  Verifica YY: 0.04 + 0.01 + 0.77 = 0.82
  Verifica ZZ: 0.06 + 0.00 + 0.77 = 0.84

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/39999)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.09 (L/6160) $f_{Z,L}$=0.01 (L/71687)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=5.26 - Classe 3
  Sollecitazioni: N=-6599.93 T_z=-32.26 M_y=97.24 T_y=-1652.35 M_z=-4901.64 M_x=6.81
  Tensioni: σ_N=-77.56 σ_M=-2662.82 τ=6.83 σ_{max}=-2740.38

Tensioni: σ_N=-77.56 σ_M=-206.00 τ=38.67 τ_{max}=38.67
Tensioni: σ_N=-77.56 σ_M=-2662.82 τ=6.83 $\sigma_{ID,max}$=2740.40

Asta n. 3104 (1891 1896) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-18441.50 My,Ed=-406.24 Mz,Ed=-2727.69
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=553.99
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=5.54 Curva b: α-imp=0.34 k_c=0.94 ψ=1.60 M,cr=49292.10 λ_{LT}=0.60
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.67 β_{LT}=0.75 f=0.97 χ_{LT}=0.94
λ_Y=77.48 Ncr,y=293755.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
λ_Z=106.14 Ncr,z=156543.00 λ^*_z=1.39 Curva c: Φ_z=1.76 χ_z=0.35
Kyy, Kyz, Kzy, Kzz = 1.01, 1.05, 0.81, 1.05
Verifica YY: 0.11 + 0.03 + 0.46 = 0.59
Verifica ZZ: 0.18 + 0.02 + 0.46 = 0.66

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/36999) $f_{Z,L}$=0.00 (L/363059)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.09 (L/6497) $f_{Z,L}$=0.01 (L/53786)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-18441.50 T_z=79.78 M_y=59.08 T_y=766.17 M_z=-2727.69 M_x=-9.15
Tensioni: σ_N=-216.72 σ_M=-1482.82 τ=9.17 σ_{max}=-1699.54
Tensioni: σ_N=-216.72 σ_M=-115.44 τ=34.43 τ_{max}=34.43
Tensioni: σ_N=-216.72 σ_M=-1482.82 τ=9.17 $\sigma_{ID,max}$=1699.62

Asta n. 3105 (-844 1992) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-11712.50 M,Ed=0.12
Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=78.22
αmy, αmz, αLT = 0.95, ----, ----
λ=19.38 Ncr=1185880.00 λ^*=0.25
Curva a: Φ=0.54 χ,min=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
Verifica: 0.16 + 0.00 = 0.16

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/28281)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/5158)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-11712.50
N,Ed=-11712.50 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.16

Asta n. 3106 (-847 1993) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-10805.20 M,Ed=0.29
Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=66.17
αmy, αmz, αLT = 0.95, ----, ----
λ=16.39 Ncr=1657040.00 λ^*=0.21
Curva a: Φ=0.52 χ,min=1.00
Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
Verifica: 0.15 + 0.00 = 0.15

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/31537)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.01 (L/5981)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-10805.20 T=1.76
N,Ed=-10805.20 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.15

Asta n. 3211 (1902 1904) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3312.13 My,Ed=1267.98 Mz,Ed=-1999.49
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=379.60

αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.80 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=39930.60 λ_{LT}=0.51
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.62 β_{LT}=0.75 f=0.98 χ_{LT}=0.98
λ_Y=62.61 Ncr,y=307021.00 λ^*_y=0.82 Curva b: Φ_y=0.94 χ_y=0.71
λ_Z=83.04 Ncr,z=174529.00 λ^*_z=1.09 Curva c: Φ_z=1.31 χ_z=0.49
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.13 + 0.51 = 0.65
Verifica ZZ: 0.02 + 0.10 + 0.51 = 0.63

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.06 (L/6589) $f_{Z,L}$=0.04 (L/10816)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.32 (L/1184) $f_{Z,L}$=0.20 (L/1934)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3312.13 T_z=334.03 M_y=1267.98 T_y=596.41 M_z=-1999.49
Tensioni: σ_N=-57.04 σ_M=-2205.13 τ=0.00 σ_{max}=-2262.17
Tensioni: σ_N=-57.04 σ_M=-453.29 τ=23.49 τ_{max}=23.49
Tensioni: σ_N=-57.04 σ_M=-2205.13 τ=0.00 $\sigma_{ID,max}$=2262.17

Asta n. 3212 (1902 1903) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3566.19 My,Ed=-1163.44 Mz,Ed=-2525.46
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=334.12
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.34 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=47739.80 λ_{LT}=0.47
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.59 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=55.11 Ncr,y=396295.00 λ^*_y=0.72 Curva b: Φ_y=0.85 χ_y=0.77
λ_Z=73.09 Ncr,z=225278.00 λ^*_z=0.96 Curva c: Φ_z=1.14 χ_z=0.57
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.11 + 0.64 = 0.77
Verifica ZZ: 0.02 + 0.09 + 0.64 = 0.75

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.06 (L/5878) $f_{Z,L}$=0.02 (L/13474)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.32 (L/1038) $f_{Z,L}$=0.14 (L/2397)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3566.19 T_z=-348.21 M_y=-1163.44 T_y=817.30 M_z=-2525.46
Tensioni: σ_N=-61.42 σ_M=-2635.37 τ=0.00 σ_{max}=-2696.79
Tensioni: σ_N=-61.42 σ_M=182.35 τ=28.20 τ_{max}=28.20
Tensioni: σ_N=-61.42 σ_M=-2635.37 τ=0.00 $\sigma_{ID,max}$=2696.79

Asta n. 3212 (1905 1907) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-11786.60 My,Ed=686.47 Mz,Ed=239.57
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=437.01
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.37 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=33075.30 λ_{LT}=0.56
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_Y=72.08 Ncr,y=231653.00 λ^*_y=0.94 Curva b: Φ_y=1.07 χ_y=0.63
λ_Z=95.60 Ncr,z=131685.00 λ^*_z=1.25 Curva c: Φ_z=1.54 χ_z=0.41
Kyy, Kyz, Kzy, Kzz = 1.00, 1.03, 0.80, 1.03
Verifica YY: 0.09 + 0.07 + 0.06 = 0.23
Verifica ZZ: 0.15 + 0.06 + 0.06 = 0.27

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.02 (L/19093) $f_{Z,G}$=0.01 (L/34714)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.14 (L/3085) $f_{Z,G}$=0.08 (L/5309)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-11786.60 T_z=157.09 M_y=686.47 T_y=16.43 M_z=235.37
Tensioni: σ_N=-202.98 σ_M=-443.31 τ=0.00 σ_{max}=-646.29
Tensioni: σ_N=-202.98 σ_M=12.61 τ=9.45 τ_{max}=9.45
Tensioni: σ_N=-202.98 σ_M=-443.31 τ=0.00 $\sigma_{ID,max}$=646.29

Asta n. 3213 (1899 1900) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3205.09 My,Ed=1062.15 Mz,Ed=-2081.57
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=352.04
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=3.52 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=44330.50 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=58.06 Ncr,y=356964.00 λ^*_y=0.76 Curva b: Φ_y=0.88 χ_y=0.75
  λ_Z=77.01 Ncr,z=202920.00 λ^*_z=1.01 Curva c: Φ_z=1.21 χ_z=0.54
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
  Verifica YY: 0.02 + 0.10 + 0.53 = 0.65
  Verifica ZZ: 0.02 + 0.08 + 0.53 = 0.63

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.06 (L/6320) $f_{Z,L}$=0.02 (L/14197)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.31 (L/1127) $f_{Z,L}$=0.14 (L/2500)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3205.09 T_z=301.71 M_y=1062.15 T_y=660.95 M_z=-2081.57
  Tensioni: σ_N=-55.20 σ_M=-2207.46 τ=0.00 σ_{max}=-2262.65
  Tensioni: σ_N=-55.20 σ_M=-401.50 τ=23.50 τ_{max}=23.50
  Tensioni: σ_N=-55.20 σ_M=-2207.46 τ=0.00 $\sigma_{ID,max}$=2262.65

Asta n. 3214 (1896 1898) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-8910.68 My,Ed=-874.85 Mz,Ed=-188.24
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=448.31
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=4.48 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=31994.20 λ_{LT}=0.57
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.65 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
  λ_Y=73.94 Ncr,y=220115.00 λ^*_y=0.97 Curva b: Φ_y=1.10 χ_y=0.62
  λ_Z=98.07 Ncr,z=125127.00 λ^*_z=1.28 Curva c: Φ_z=1.59 χ_z=0.40
  Kyy, Kyz, Kzy, Kzz = 0.99, 1.02, 0.79, 1.02
  Verifica YY: 0.07 + 0.09 + 0.05 = 0.22
  Verifica ZZ: 0.11 + 0.07 + 0.05 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.03 (L/14180) $f_{Z,G}$=0.00 (L/130580)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.19 (L/2362) $f_{Z,G}$=0.02 (L/23741)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-8910.68 T_z=-195.14 M_y=-874.85 T_y=123.49 M_z=-188.24
  Tensioni: σ_N=-153.46 σ_M=-465.98 τ=0.00 σ_{max}=-619.43
  Tensioni: σ_N=-153.46 σ_M=-10.08 τ=11.76 τ_{max}=11.76
  Tensioni: σ_N=-153.46 σ_M=-465.98 τ=0.00 $\sigma_{ID,max}$=619.43

Asta n. 3222 (1905 1906) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-9704.72 My,Ed=-560.95 Mz,Ed=-264.06
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=458.65
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=4.59 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=31066.50 λ_{LT}=0.58
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
  λ_Y=75.65 Ncr,y=210307.00 λ^*_y=0.99 Curva b: Φ_y=1.12 χ_y=0.60
  λ_Z=100.33 Ncr,z=119551.00 λ^*_z=1.31 Curva c: Φ_z=1.63 χ_z=0.38
  Kyy, Kyz, Kzy, Kzz = 1.00, 1.02, 0.80, 1.02
  Verifica YY: 0.08 + 0.06 + 0.07 = 0.21
  Verifica ZZ: 0.13 + 0.05 + 0.07 = 0.25

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.03 (L/16757) $f_{Z,G}$=0.00 (L/111843)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.17 (L/2733) $f_{Z,G}$=0.02 (L/21279)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-9704.72 T_z=-122.30 M_y=-560.95 T_y=120.27 M_z=-264.06
  Tensioni: σ_N=-167.13 σ_M=-425.80 τ=0.00 σ_{max}=-592.92
  Tensioni: σ_N=-167.13 σ_M=-14.15 τ=7.39 τ_{max}=7.39
  Tensioni: σ_N=-167.13 σ_M=-425.80 τ=0.00 $\sigma_{ID,max}$=592.92

Asta n. 3223 (1899 1901) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3665.41 My,Ed=-1203.86 Mz,Ed=-2487.37
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=363.03
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=3.63 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=42465.80 λ_{LT}=0.49
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.61 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=59.88 Ncr,y=335675.00 λ^*_y=0.78 Curva b: Φ_y=0.91 χ_y=0.73
  λ_Z=79.42 Ncr,z=190818.00 λ^*_z=1.04 Curva c: Φ_z=1.25 χ_z=0.52
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
  Verifica YY: 0.02 + 0.12 + 0.63 = 0.77
  Verifica ZZ: 0.02 + 0.09 + 0.63 = 0.75

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.06 (L/5975) $f_{Z,L}$=0.03 (L/11877)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.34 (L/1060) $f_{Z,L}$=0.17 (L/2119)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3665.41 T_z=-331.61 M_y=-1203.86 T_y=746.59 M_z=-2487.37
  Tensioni: σ_N=-63.12 σ_M=-2615.45 τ=0.00 σ_{max}=-2678.57
  Tensioni: σ_N=-63.12 σ_M=195.43 τ=26.22 τ_{max}=26.22
  Tensioni: σ_N=-63.12 σ_M=-2615.45 τ=0.00 $\sigma_{ID,max}$=2678.57

Asta n. 3224 (1896 1897) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-11067.90 My,Ed=520.42 Mz,Ed=259.59
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=426.15
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=4.26 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=34185.30 λ_{LT}=0.55
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
  λ_Y=70.29 Ncr,y=243609.00 λ^*_y=0.92 Curva b: Φ_y=1.05 χ_y=0.65
  λ_Z=93.22 Ncr,z=138482.00 λ^*_z=1.22 Curva c: Φ_z=1.49 χ_z=0.42
  Kyy, Kyz, Kzy, Kzz = 1.00, 1.03, 0.80, 1.03
  Verifica YY: 0.09 + 0.05 + 0.07 = 0.21
  Verifica ZZ: 0.13 + 0.04 + 0.07 = 0.25

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.02 (L/26598) $f_{Z,G}$=0.01 (L/33346)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.10 (L/4145) $f_{Z,G}$=0.08 (L/5106)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-11067.90 T_z=122.12 M_y=520.42 T_y=9.71 M_z=258.17
  Tensioni: σ_N=-190.60 σ_M=-406.71 τ=0.00 σ_{max}=-597.32
  Tensioni: σ_N=-190.60 σ_M=13.83 τ=7.35 τ_{max}=7.35
  Tensioni: σ_N=-190.60 σ_M=-406.71 τ=0.00 $\sigma_{ID,max}$=597.32

Asta n. 3232 (-844 1908) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-4522.71 My,Ed=-87.73 Mz,Ed=-723.61
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=248865.00 λ_{LT}=0.20
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.02 + 0.01 + 0.18 = 0.21
  Verifica ZZ: 0.02 + 0.01 + 0.18 = 0.21

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/40490)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/6678) $f_{Z,L}$=0.00 (L/80980)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-4522.71 T_z=-71.00 M_y=-87.73 T_y=618.82 M_z=-723.61
  Tensioni: σ_N=-77.89 σ_M=-671.10 τ=0.00 σ_{max}=-748.99

Tensioni: σ_N=-77.89 σ_M=-14.81 τ=16.73 τ_{max}=16.73
Tensioni: σ_N=-77.89 σ_M=-671.10 τ=0.00 $\sigma_{ID,max}$=748.99

Asta n. 3232 (-843 -844) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3110.91 My,Ed=-87.73 Mz,Ed=-723.61
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.15 M,cr=163343.00 λ_{LT}=0.25
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.02 + 0.01 + 0.18 = 0.21
Verifica ZZ: 0.02 + 0.01 + 0.18 = 0.20

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/30849) $f_{Z,L}$=0.00 (L/107973)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/5310) $f_{Z,L}$=0.00 (L/40490)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.24 - Classe 3
Sollecitazioni: N=-3080.10 T_z=19.78 M_y=-87.73 T_y=-431.28 M_z=-723.61
Tensioni: σ_N=-53.04 σ_M=-671.10 τ=0.00 σ_{max}=-724.14
Tensioni: σ_N=-53.04 σ_M=-14.81 τ=11.42 τ_{max}=11.42
Tensioni: σ_N=-53.04 σ_M=-671.10 τ=0.00 $\sigma_{ID,max}$=724.14

Asta n. 3232 (-842 -843) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-3002.58 My,Ed=-138.25 Mz,Ed=-210.79
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.05 M,cr=149445.00 λ_{LT}=0.26
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.02 + 0.01 + 0.05 = 0.08
Verifica ZZ: 0.02 + 0.01 + 0.05 = 0.08

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.00 (L/64784) $f_{Z,G}$=0.00 (L/86378)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.24 - Classe 3
Sollecitazioni: N=-2978.88 T_z=36.40 M_y=-138.25 T_y=-278.91 M_z=-210.79
Tensioni: σ_N=-51.30 σ_M=-234.03 τ=0.00 σ_{max}=-285.33
Tensioni: σ_N=-51.30 σ_M=26.45 τ=7.60 τ_{max}=7.60
Tensioni: σ_N=-51.30 σ_M=-234.03 τ=0.00 $\sigma_{ID,max}$=285.33

Asta n. 3232 (-841 -842) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3172.54 My,Ed=-38.86 Mz,Ed=505.78
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.40 M,cr=199322.00 λ_{LT}=0.23
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.02 + 0.00 + 0.13 = 0.15
Verifica ZZ: 0.02 + 0.00 + 0.13 = 0.15

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/44678)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/6610) $f_{Z,L}$=0.00 (L/107973)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3172.54 T_z=19.78 M_y=-14.42 T_y=-232.01 M_z=505.78
Tensioni: σ_N=-54.64 σ_M=-453.03 τ=0.00 σ_{max}=-507.67

Tensioni: σ_N=-54.64 σ_M=31.03 τ=6.20 τ_{max}=6.20
Tensioni: σ_N=-54.64 σ_M=-453.03 τ=0.00 $\sigma_{ID,max}$=507.67

Asta n. 3232 (1905 -841) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3203.35 My,Ed=-14.42 Mz,Ed=751.42
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.17 M,cr=165763.00 λ_{LT}=0.25
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.02 + 0.00 + 0.19 = 0.21
Verifica ZZ: 0.02 + 0.00 + 0.19 = 0.21

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/20245)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.03 (L/3755)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3203.35 T_z=19.78 M_y=10.01 T_y=-165.59 M_z=751.42
Tensioni: σ_N=-55.17 σ_M=-669.16 τ=0.00 σ_{max}=-724.33
Tensioni: σ_N=-55.17 σ_M=37.52 τ=4.49 τ_{max}=4.49
Tensioni: σ_N=-55.17 σ_M=-669.16 τ=0.00 $\sigma_{ID,max}$=724.33

Asta n. 3234 (1896 -840) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3903.06 My,Ed=262.94 Mz,Ed=597.02
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.66 M,cr=176412.00 λ_{LT}=0.24
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.03 + 0.15 = 0.19
Verifica ZZ: 0.02 + 0.02 + 0.15 = 0.19

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/23779) $f_{Z,L}$=0.00 (L/95118)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.03 (L/4502) $f_{Z,L}$=0.01 (L/21137)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3903.06 T_z=165.92 M_y=262.94 T_y=-82.42 M_z=597.02
Tensioni: σ_N=-67.22 σ_M=-618.87 τ=0.00 σ_{max}=-686.08
Tensioni: σ_N=-67.22 σ_M=31.98 τ=10.00 τ_{max}=10.00
Tensioni: σ_N=-67.22 σ_M=-618.87 τ=0.00 $\sigma_{ID,max}$=686.08

Asta n. 3234 (-840 -845) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3848.43 My,Ed=-218.69 Mz,Ed=429.20
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.65 M,cr=174616.00 λ_{LT}=0.24
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.02 + 0.11 = 0.15
Verifica ZZ: 0.02 + 0.02 + 0.11 = 0.14

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/54353)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/7460) $f_{Z,L}$=0.00 (L/31706)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3848.43 T_z=165.92 M_y=22.13 T_y=-148.84 M_z=429.20
  Tensioni: σ_N=-66.28 σ_M=-387.82 τ=0.00 σ_{max}=-454.10
  Tensioni: σ_N=-66.28 σ_M=22.99 τ=10.02 τ_{max}=10.02
  Tensioni: σ_N=-66.28 σ_M=-387.82 τ=0.00 $\sigma_{ID,max}$=454.10

Asta n. 3234 (-845 -846) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3793.79 My,Ed=-459.51 Mz,Ed=-195.66
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.32 M,cr=139774.00 λ_{LT}=0.27
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.02 + 0.04 + 0.05 = 0.11
  Verifica ZZ: 0.02 + 0.04 + 0.05 = 0.10

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.00 (L/54353)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.01 (L/10012) $f_{Z,G}$=0.00 (L/80099)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.45 - Classe 3
  Sollecitazioni: N=-3739.16 T_z=165.92 M_y=-459.51 T_y=-281.69 M_z=-195.66
  Tensioni: σ_N=-64.39 σ_M=-330.51 τ=0.00 σ_{max}=-394.90
  Tensioni: σ_N=-64.39 σ_M=114.97 τ=11.41 τ_{max}=11.41
  Tensioni: σ_N=-64.39 σ_M=-330.51 τ=0.00 $\sigma_{ID,max}$=394.90

Asta n. 3234 (-846 -847) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3739.16 My,Ed=-700.33 Mz,Ed=-652.70
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.19 M,cr=126200.00 λ_{LT}=0.29
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.02 + 0.07 + 0.16 = 0.25
  Verifica ZZ: 0.02 + 0.05 + 0.16 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.00 (L/31706) $f_{Z,G}$=0.00 (L/34588)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.03 (L/5764) $f_{Z,G}$=0.02 (L/6087)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.45 - Classe 3
  Sollecitazioni: N=-3684.52 T_z=165.92 M_y=-700.33 T_y=-348.11 M_z=-652.70
  Tensioni: σ_N=-63.45 σ_M=-817.79 τ=0.00 σ_{max}=-881.24
  Tensioni: σ_N=-63.45 σ_M=156.24 τ=12.62 τ_{max}=12.62
  Tensioni: σ_N=-63.45 σ_M=-817.79 τ=0.00 $\sigma_{ID,max}$=881.24

Asta n. 3234 (-847 1909) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7647.92 My,Ed=-700.33 Mz,Ed=-652.70
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=185554.00 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.96, 0.77, 0.96
  Verifica YY: 0.04 + 0.07 + 0.16 = 0.27
  Verifica ZZ: 0.04 + 0.05 + 0.16 = 0.26

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.00 (L/47559) $f_{Z,G}$=0.00 (L/54353)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/8095) $f_{Z,L}$=0.02 (L/8647)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-7647.92 T_z=-482.52 M_y=-700.33 T_y=482.92 M_z=-652.70
  Tensioni: σ_N=-131.71 σ_M=-817.79 τ=0.00 σ_{max}=-949.50
  Tensioni: σ_N=-131.71 σ_M=-34.97 τ=29.15 τ_{max}=29.15
  Tensioni: σ_N=-131.71 σ_M=-817.79 τ=0.00 $\sigma_{ID,max}$=949.50

Asta n. 4001 (1916 1917) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-5325.53 My,Ed=-3673.98 Mz,Ed=2646.72
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=700.73
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.01 Curva b: α-imp=0.34 k_c=0.94 ψ=1.46 M,cr=33815.00 λ_{LT}=0.72
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.75 β_{LT}=0.75 f=0.97 χ_{LT}=0.88
  λ_Y=98.01 Ncr,y=183603.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.44
  λ_Z=134.26 Ncr,z=97842.80 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
  Verifica YY: 0.04 + 0.24 + 0.42 = 0.70
  Verifica ZZ: 0.08 + 0.19 + 0.42 = 0.69

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/90155) $f_{Z,L}$=0.01 (L/120454)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.05 (L/15387) $f_{Z,L}$=0.03 (L/21174)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.01 - Classe 3
  Sollecitazioni: N=-6728.65 T_z=-15.90 M_y=-3.81 T_y=870.13 M_z=3565.64
  Tensioni: σ_N=-79.08 σ_M=-1923.57 τ=0.00 σ_{max}=-2002.64
  Tensioni: σ_N=-79.08 σ_M=139.06 τ=16.61 τ_{max}=16.61
  Tensioni: σ_N=-79.08 σ_M=-1923.57 τ=0.00 $\sigma_{ID,max}$=2002.64

Asta n. 4002 (1910 1911) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-18493.60 My,Ed=-756.38 Mz,Ed=3290.47
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=702.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.02 Curva b: α-imp=0.34 k_c=0.94 ψ=1.65 M,cr=38168.70 λ_{LT}=0.68
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.72 β_{LT}=0.75 f=0.97 χ_{LT}=0.91
  λ_Y=98.21 Ncr,y=182868.00 λ^*_y=1.29 Curva b: Φ_y=1.51 χ_y=0.43
  λ_Z=134.53 Ncr,z=97451.20 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 1.03, 1.10, 0.83, 1.10
  Verifica YY: 0.15 + 0.05 + 0.58 = 0.78
  Verifica ZZ: 0.26 + 0.04 + 0.58 = 0.88

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.01 (L/51128) $f_{Z,G}$=0.01 (L/72536)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.08 (L/9203) $f_{Z,G}$=0.06 (L/12405)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-18493.60 T_z=-115.46 M_y=-756.38 T_y=-830.26 M_z=3290.47 M_x=6.99
  Tensioni: σ_N=-217.34 σ_M=-1926.57 τ=7.00 σ_{max}=-2143.90
  Tensioni: σ_N=-217.34 σ_M=249.74 τ=30.02 τ_{max}=30.02
  Tensioni: σ_N=-217.34 σ_M=-1926.57 τ=7.00 $\sigma_{ID,max}$=2143.94

Asta n. 4004 (1848 1849) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7377.04 My,Ed=-117.82 Mz,Ed=3663.67
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=700.78
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.01 Curva b: α-imp=0.34 k_c=0.94 ψ=1.17 M,cr=27277.40 λ_{LT}=0.80
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.81 β_{LT}=0.75 f=0.97 χ_{LT}=0.84
  λ_Y=98.02 Ncr,y=183579.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.44
  λ_Z=134.27 Ncr,z=97829.90 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 0.98, 1.01, 0.79, 1.01
  Verifica YY: 0.06 + 0.01 + 0.59 = 0.66
  Verifica ZZ: 0.11 + 0.01 + 0.59 = 0.70

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.01 (L/79871)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.05 (L/13360) $f_{Z,G}$=0.05 (L/14905)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.01 - Classe 3
  Sollecitazioni: N=-6769.18 T_z=-5.39 M_y=-80.08 T_y=897.56 M_z=3663.67 M_x=-1.42
  Tensioni: σ_N=-79.55 σ_M=-1991.77 τ=1.42 σ_{max}=-2071.33
  Tensioni: σ_N=-79.55 σ_M=155.16 τ=18.55 τ_{max}=18.55
  Tensioni: σ_N=-79.55 σ_M=-1991.77 τ=1.42 $\sigma_{ID,max}$=2071.33

Asta n. 4004 (1912 1913) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-18208.20 My,Ed=-871.09 Mz,Ed=3265.32
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=702.06
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.02 Curva b: α-imp=0.34 k_c=0.94 ψ=1.67 M,cr=38641.90 λ_{LT}=0.68
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.72 β_{LT}=0.75 f=0.97 χ_{LT}=0.91
  λ_Y=98.19 Ncr,y=182908.00 λ^*_y=1.29 Curva b: Φ_y=1.51 χ_y=0.43
  λ_Z=134.51 Ncr,z=97472.40 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 1.03, 1.10, 0.83, 1.10
  Verifica YY: 0.15 + 0.06 + 0.57 = 0.78
  Verifica ZZ: 0.26 + 0.05 + 0.57 = 0.88

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.02 (L/42800) $f_{Z,G}$=0.01 (L/73250)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.09 (L/7765) $f_{Z,G}$=0.06 (L/12584)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-18208.20 T_z=-133.03 M_y=-871.09 T_y=-821.99 M_z=3265.32 M_x=8.05
  Tensioni: σ_N=-213.98 σ_M=-1936.08 τ=8.07 σ_{max}=-2150.06
  Tensioni: σ_N=-213.98 σ_M=267.27 τ=33.31 τ_{max}=33.31
  Tensioni: σ_N=-213.98 σ_M=-1936.08 τ=8.07 $\sigma_{ID,max}$=2150.11

Asta n. 4005 (-878 -852) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/25040)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.07 (L/4540)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-13336.50
  N,Ed=-13336.50 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.18

- Verifica di stabilità (4.2.4.1.3.1) - CC 25
  Sollecitazioni: N=-13336.50 L=320.00
  λ=79.28 Ncr=70851.00 λ^*=1.04
  Curva a: Φ=1.13 χ,min=0.64 N,Ed=-13336.50 Nb,Rd=46443.40 N,Ed/Nb,Rd=0.29

Asta n. 4006 (-879 -855) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/24314)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.04 (L/4462)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-13689.30
  N,Ed=-13689.30 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.19

- Verifica di stabilità (4.2.4.1.3.1) - CC 25
  Sollecitazioni: N=-13689.30 L=160.00
  λ=39.64 Ncr=283404.00 λ^*=0.52
  Curva a: Φ=0.67 χ,min=0.92 N,Ed=-13689.30 Nb,Rd=66718.00 N,Ed/Nb,Rd=0.21

Asta n. 4007 (1925 1996) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/29107)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.61 - Classe 3
  Sollecitazioni: N=3742.65
  Tensioni: σ_N=174.17 σ_M=0.00 τ=0.00 σ_{max}=174.17
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=174.17 σ_M=0.00 τ=0.00 $\sigma_{ID,max}$=174.17

Asta n. 4008 (1926 1997) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/52756)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/9815)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-6148.29
  N,Ed=-6148.29 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.08

Asta n. 4009 (1997 1925) Cir. D=4 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-2596.85 M,Ed=4.05
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=259.36
  λ=259.36 Ncr=3872.04 λ^*=3.39 Curva c: Φ=7.04 χ,min=0.08
  χ,min=0.08
  Verifica: 0.81 + 0.06 = 0.87

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/123615)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.14 (L/1814) $f_{Z,G}$=0.09 (L/2959)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.30 - Classe 3
  Sollecitazioni: N=-2587.14 M=5.39
  Tensioni: σ_N=-205.88 σ_M=-85.86 τ=0.00 σ_{max}=-291.74
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-205.88 σ_M=-85.86 τ=0.00 $\sigma_{ID,max}$=291.74

Asta n. 4010 (1996 1926) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 25 - Classe 3
  L_{cr}=2.10 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
  $\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
  CC 25 My,Ed=-5.68 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/183461)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.08 (L/2765) $f_{Z,G}$=0.06 (L/3261)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.05 - Classe 3
  Sollecitazioni: N=3301.84 M=4.37
  Tensioni: σ_N=262.75 σ_M=69.51 τ=0.00 σ_{max}=332.26
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=262.75 σ_M=69.51 τ=0.00 $\sigma_{ID,max}$=332.26

Asta n. 4011 (1922 1994) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/120586)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/22213)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.61 - Classe 3
  Sollecitazioni: N=3515.28
  Tensioni: σ_N=163.59 σ_M=0.00 τ=0.00 σ_{max}=163.59
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=163.59 σ_M=0.00 τ=0.00 $\sigma_{ID,max}$=163.59

Asta n. 4012 (1923 1995) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-6152.45 M,Ed=0.00

Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=161.00
αmy, αmz, αLT = 0.95, ----, ----
λ=39.89 Ncr=279894.00 λ^*=0.52
Curva a: Φ=0.67 χ,min=0.92
Kyy, Kyz, Kzy, Kzz = 0.98, ----, ----, ----
Verifica: 0.08 = 0.08

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/84410)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.01 (L/14808)

- Verifica a compressione (4.2.10) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-6152.45
N,Ed=-6152.45 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.08

Asta n. 4013 (1922 1995) Cir. D=4 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 1 - Classe 3
Sollecitazioni: N,Ed=-3505.01 M,Ed=4.05
Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=259.36
λ=259.36 Ncr=3872.04 λ^*=3.39 Curva c: Φ=7.04 χ,min=0.08
χ,min=0.08
Verifica: 1.09 + 0.20 = 1.29

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/123615)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.14 (L/1814) $f_{Z,G}$=0.10 (L/2619)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.30 - Classe 3
Sollecitazioni: N=-5496.98 M=5.39
Tensioni: σ_N=-437.44 σ_M=-85.86 τ=0.00 σ_{max}=-523.30
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=-437.44 σ_M=-85.86 τ=0.00 $\sigma_{ID,max}$=523.30

Asta n. 4014 (1923 1994) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 25 - Classe 3
L_{cr}=2.10 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
$\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
CC 25 My,Ed=-5.68 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 23 - Classe 3
Sollecitazioni: N,Ed=-69.11 M,Ed=3.28
Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=209.96
λ=209.96 Ncr=5908.50 λ^*=2.75 Curva c: Φ=4.90 χ,min=0.11
χ,min=0.11
Verifica: 0.00 + 0.02 = 0.02

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/122307)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.08 (L/2769) $f_{Z,G}$=0.06 (L/3731)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.05 - Classe 3
Sollecitazioni: N=7466.93 M=4.37
Tensioni: σ_N=594.20 σ_M=69.51 τ=0.00 σ_{max}=663.71
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=594.20 σ_M=69.51 τ=0.00 $\sigma_{ID,max}$=663.71

Asta n. 4015 (1917 1913) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-2508.01 M,Ed=2.86
Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=102.22
αmy, αmz, αLT = 0.95, ----, ----
λ=25.33 Ncr=694405.00 λ^*=0.33
Curva a: Φ=0.57 χ,min=0.97
Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
Verifica: 0.03 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.51 - Classe 3

Sollecitazioni: N=-2508.01 M=2.86
Tensioni: σ_N=-116.71 σ_M=-4.91 τ=0.00 σ_{max}=-121.62
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=-116.71 σ_M=-4.91 τ=0.00 $\sigma_{ID,max}$=121.62

Asta n. 4016 (1913 1915) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-2861.87 M,Ed=4.01
Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=120.97
αmy, αmz, αLT = 0.95, ----, ----
λ=29.97 Ncr=495806.00 λ^*=0.39
Curva a: Φ=0.60 χ,min=0.95
Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.60 - Classe 3
Sollecitazioni: N=-2861.87 M=4.01
Tensioni: σ_N=-133.18 σ_M=-6.88 τ=0.00 σ_{max}=-140.06
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=-133.18 σ_M=-6.88 τ=0.00 $\sigma_{ID,max}$=140.06

Asta n. 4017 (1915 1911) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-2457.06 M,Ed=2.89
Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=102.73
αmy, αmz, αLT = 0.95, ----, ----
λ=25.45 Ncr=687497.00 λ^*=0.33
Curva a: Φ=0.57 χ,min=0.97
Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
Verifica: 0.03 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.51 - Classe 3
Sollecitazioni: N=-2457.06 M=2.89
Tensioni: σ_N=-114.34 σ_M=-4.96 τ=0.00 σ_{max}=-119.30
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=-114.34 σ_M=-4.96 τ=0.00 $\sigma_{ID,max}$=119.30

Asta n. 4018 (1911 1917) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-2866.29 M,Ed=3.97
Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=120.28
αmy, αmz, αLT = 0.95, ----, ----
λ=29.80 Ncr=501459.00 λ^*=0.39
Curva a: Φ=0.60 χ,min=0.96
Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.60 - Classe 3
Sollecitazioni: N=-2866.29 M=3.97
Tensioni: σ_N=-133.39 σ_M=-6.80 τ=0.00 σ_{max}=-140.19
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=-133.39 σ_M=-6.80 τ=0.00 $\sigma_{ID,max}$=140.19

Asta n. 4101 (1917 1924) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-7073.29 My,Ed=407.48 Mz,Ed=-4905.92
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=526.58
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=5.27 Curva b: α-imp=0.34 k_c=0.94 ψ=1.74 M,cr=56963.10 λ_{LT}=0.56
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_Y=73.65 Ncr,y=325125.00 λ^*_y=0.96 Curva b: Φ_y=1.09 χ_y=0.62
λ_Z=100.89 Ncr,z=173260.00 λ^*_z=1.32 Curva c: Φ_z=1.65 χ_z=0.38
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
Verifica YY: 0.04 + 0.02 + 0.77 = 0.84
Verifica ZZ: 0.06 + 0.02 + 0.77 = 0.86

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/38884) $f_{Z,L}$=0.01 (L/52586)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.09 (L/6047) $f_{Z,L}$=0.06 (L/8905)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=5.27 - Classe 3
  Sollecitazioni: N=-6621.74 T_z=-78.11 M_y=407.48 T_y=-1644.82 M_z=-4905.92
  Tensioni: σ_N=-77.82 σ_M=-2727.53 τ=0.00 σ_{max}=-2805.35
  Tensioni: σ_N=-77.82 σ_M=-256.20 τ=31.49 τ_{max}=31.49
  Tensioni: σ_N=-77.82 σ_M=-2727.53 τ=0.00 $\sigma_{ID,max}$=2805.35

Asta n. 4102 (1911 1927) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-18781.20 My,Ed=-476.62 Mz,Ed=-2668.47
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=553.99
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.54 Curva b: α-imp=0.34 k_c=0.94 ψ=1.62 M,cr=49893.20 λ_{LT}=0.59
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.67 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
  λ_Y=77.48 Ncr,y=293755.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
  λ_z=106.14 Ncr,z=156543.00 λ^*_z=1.39 Curva c: Φ_z=1.76 χ_z=0.35
  Kyy, Kyz, Kzy, Kzz = 1.01, 1.06, 0.81, 1.06
  Verifica YY: 0.11 + 0.03 + 0.45 = 0.59
  Verifica ZZ: 0.18 + 0.02 + 0.45 = 0.66

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.02 (L/33194) $f_{Z,L}$=0.00 (L/161359)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.10 (L/5826) $f_{Z,L}$=0.02 (L/29637)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-18781.20 T_z=92.39 M_y=59.69 T_y=781.81 M_z=-2668.47 M_x=-9.20
  Tensioni: σ_N=-220.72 σ_M=-1451.01 τ=9.22 σ_{max}=-1671.72
  Tensioni: σ_N=-220.72 σ_M=-113.24 τ=35.05 τ_{max}=35.05
  Tensioni: σ_N=-220.72 σ_M=-1451.01 τ=9.22 $\sigma_{ID,max}$=1671.80

Asta n. 4103 (1915 1921) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7064.46 My,Ed=102.41 Mz,Ed=-4911.54
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=526.43
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.26 Curva b: α-imp=0.34 k_c=0.94 ψ=1.16 M,cr=38107.20 λ_{LT}=0.68
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.72 β_{LT}=0.75 f=0.97 χ_{LT}=0.91
  λ_Y=73.63 Ncr,y=325318.00 λ^*_y=0.96 Curva b: Φ_y=1.09 χ_y=0.62
  λ_z=100.86 Ncr,z=173363.00 λ^*_z=1.32 Curva c: Φ_z=1.65 χ_z=0.38
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
  Verifica YY: 0.04 + 0.01 + 0.77 = 0.82
  Verifica ZZ: 0.06 + 0.01 + 0.77 = 0.84

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/40291)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.09 (L/6153) $f_{Z,L}$=0.01 (L/68147)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=5.26 - Classe 3
  Sollecitazioni: N=-6612.91 T_z=-33.02 M_y=102.41 T_y=-1655.24 M_z=-4911.54 M_x=6.77
  Tensioni: σ_N=-77.71 σ_M=-2669.19 τ=6.79 σ_{max}=-2746.91
  Tensioni: σ_N=-77.71 σ_M=-207.21 τ=38.65 τ_{max}=38.65
  Tensioni: σ_N=-77.71 σ_M=-2669.19 τ=6.79 $\sigma_{ID,max}$=2746.93

Asta n. 4104 (1913 1918) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-18487.60 My,Ed=-488.38 Mz,Ed=-2632.77
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=553.99
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.54 Curva b: α-imp=0.34 k_c=0.94 ψ=1.61 M,cr=49575.70 λ_{LT}=0.60
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.67 β_{LT}=0.75 f=0.97 χ_{LT}=0.94
  λ_Y=77.48 Ncr,y=293755.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
  λ_z=106.14 Ncr,z=156543.00 λ^*_z=1.39 Curva c: Φ_z=1.76 χ_z=0.35
  Kyy, Kyz, Kzy, Kzz = 1.01, 1.05, 0.81, 1.05
  Verifica YY: 0.11 + 0.03 + 0.44 = 0.58
  Verifica ZZ: 0.18 + 0.02 + 0.44 = 0.65

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.02 (L/36305) $f_{Z,L}$=0.00 (L/484079)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.09 (L/6440) $f_{Z,L}$=0.01 (L/55855)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-18487.60 T_z=93.15 M_y=66.36 T_y=766.30 M_z=-2632.77 M_x=-10.42
  Tensioni: σ_N=-217.26 σ_M=-1433.09 τ=10.45 σ_{max}=-1650.36
  Tensioni: σ_N=-217.26 σ_M=-112.92 τ=38.47 τ_{max}=38.47
  Tensioni: σ_N=-217.26 σ_M=-1433.09 τ=10.45 $\sigma_{ID,max}$=1650.46

Asta n. 4105 (-852 1998) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-11738.80 M,Ed=0.12
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=78.22
  αmy, αmz, αLT = 0.95, ----, ----
  λ=19.38 Ncr=1185880.00 λ^*=0.25
  Curva a: Φ=0.54 χ,min=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
  Verifica: 0.16 + 0.00 = 0.16

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/28281)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/5190)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-11738.80
  N,Ed=-11738.80 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.16

Asta n. 4106 (-855 1999) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-10812.80 M,Ed=0.29
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=66.17
  αmy, αmz, αLT = 0.95, ----, ----
  λ=16.39 Ncr=1657040.00 λ^*=0.21
  Curva a: Φ=0.52 χ,min=1.00
  Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
  Verifica: 0.15 + 0.00 = 0.15

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/31537)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/5981)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-10812.80 T=1.76
  N,Ed=-10812.80 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.15

Asta n. 4211 (1924 1926) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3312.47 My,Ed=1269.47 Mz,Ed=-1999.99
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=379.60
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=3.80 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=39930.60 λ_{LT}=0.51
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.62 β_{LT}=0.75 f=0.98 χ_{LT}=0.98
  λ_Y=62.61 Ncr,y=307021.00 λ^*_y=0.82 Curva b: Φ_y=0.94 χ_y=0.71
  λ_Z=83.04 Ncr,z=174529.00 λ^*_z=1.09 Curva c: Φ_z=1.31 χ_z=0.49
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
  Verifica YY: 0.02 + 0.13 + 0.51 = 0.65
  Verifica ZZ: 0.02 + 0.10 + 0.51 = 0.63

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.06 (L/6611) $f_{Z,L}$=0.04 (L/10757)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.32 (L/1184) $f_{Z,L}$=0.20 (L/1930)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3312.47 T_z=334.43 M_y=1269.47 T_y=596.54 M_z=-1999.99
  Tensioni: σ_N=-57.05 σ_M=-2206.08 τ=0.00 σ_{max}=-2263.13
  Tensioni: σ_N=-57.05 σ_M=-453.73 τ=23.51 τ_{max}=23.51

Tensioni: σ_N=-57.05 σ_M=-2206.08 τ=0.00 $\sigma_{ID,max}$=2263.13

Asta n. 4212 (1924 1925) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3573.13 My,Ed=-1164.00 Mz,Ed=-2528.98
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=334.12
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.34 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=47739.80 λ_{LT}=0.47
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.59 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=55.11 Ncr,y=396295.00 λ^*_y=0.72 Curva b: Φ_y=0.85 χ_y=0.77
λ_Z=73.09 Ncr,z=225278.00 λ^*_z=0.96 Curva c: Φ_z=1.14 χ_z=0.57
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.11 + 0.64 = 0.77
Verifica ZZ: 0.02 + 0.09 + 0.64 = 0.75

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.06 (L/5868) $f_{Z,L}$=0.02 (L/13739)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.32 (L/1036) $f_{Z,L}$=0.14 (L/2406)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3573.13 T_z=-348.38 M_y=-1164.00 T_y=818.35 M_z=-2528.98
Tensioni: σ_N=-61.53 σ_M=-2638.68 τ=0.00 σ_{max}=-2700.21
Tensioni: σ_N=-61.53 σ_M=182.32 τ=28.23 τ_{max}=28.23
Tensioni: σ_N=-61.53 σ_M=-2638.68 τ=0.00 $\sigma_{ID,max}$=2700.21

Asta n. 4212 (1927 1929) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-11786.40 My,Ed=684.20 Mz,Ed=238.98
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=437.01
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.37 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=33075.30 λ_{LT}=0.56
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_Y=72.08 Ncr,y=231653.00 λ^*_y=0.94 Curva b: Φ_y=1.07 χ_y=0.63
λ_Z=95.60 Ncr,z=131685.00 λ^*_z=1.25 Curva c: Φ_z=1.54 χ_z=0.41
Kyy, Kyz, Kzy, Kzz = 1.00, 1.03, 0.80, 1.03
Verifica YY: 0.09 + 0.07 + 0.06 = 0.23
Verifica ZZ: 0.15 + 0.06 + 0.06 = 0.27

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.02 (L/19013) $f_{Z,G}$=0.01 (L/34453)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.14 (L/3085) $f_{Z,G}$=0.08 (L/5315)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-11786.40 T_z=156.57 M_y=684.20 T_y=16.58 M_z=234.71
Tensioni: σ_N=-202.98 σ_M=-441.94 τ=0.00 σ_{max}=-644.92
Tensioni: σ_N=-202.98 σ_M=12.57 τ=9.42 τ_{max}=9.42
Tensioni: σ_N=-202.98 σ_M=-441.94 τ=0.00 $\sigma_{ID,max}$=644.92

Asta n. 4213 (1921 1922) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3207.24 My,Ed=1063.37 Mz,Ed=-2081.35
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=352.04
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.52 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=44330.50 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=58.06 Ncr,y=356964.00 λ^*_y=0.76 Curva b: Φ_y=0.88 χ_y=0.75
λ_Z=77.01 Ncr,z=202920.00 λ^*_z=1.01 Curva c: Φ_z=1.21 χ_z=0.54
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.10 + 0.53 = 0.65
Verifica ZZ: 0.02 + 0.08 + 0.53 = 0.63

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.06 (L/6320) $f_{Z,L}$=0.03 (L/13982)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.31 (L/1128) $f_{Z,L}$=0.14 (L/2497)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3207.24 T_z=302.06 M_y=1063.37 T_y=660.89 M_z=-2081.35

Tensioni: σ_N=-55.23 σ_M=-2207.68 τ=0.00 σ_{max}=-2262.92
Tensioni: σ_N=-55.23 σ_M=-401.82 τ=23.51 τ_{max}=23.51
Tensioni: σ_N=-55.23 σ_M=-2207.68 τ=0.00 $\sigma_{ID,max}$=2262.92

Asta n. 4214 (1918 1920) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-8942.63 My,Ed=-879.43 Mz,Ed=-191.12
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=448.31
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.48 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=31994.10 λ_{LT}=0.57
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.65 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_Y=73.94 Ncr,y=220115.00 λ^*_y=0.97 Curva b: Φ_y=1.10 χ_y=0.62
λ_Z=98.07 Ncr,z=125127.00 λ^*_z=1.28 Curva c: Φ_z=1.59 χ_z=0.40
Kyy, Kyz, Kzy, Kzz = 0.99, 1.02, 0.79, 1.02
Verifica YY: 0.07 + 0.09 + 0.05 = 0.22
Verifica ZZ: 0.12 + 0.07 + 0.05 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.03 (L/14027) $f_{Z,G}$=0.00 (L/127051)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.19 (L/2348) $f_{Z,G}$=0.02 (L/23387)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-8942.63 T_z=-196.16 M_y=-879.43 T_y=124.13 M_z=-191.12
Tensioni: σ_N=-154.01 σ_M=-470.10 τ=0.00 σ_{max}=-624.10
Tensioni: σ_N=-154.01 σ_M=-10.24 τ=11.82 τ_{max}=11.82
Tensioni: σ_N=-154.01 σ_M=-470.10 τ=0.00 $\sigma_{ID,max}$=624.10

Asta n. 4222 (1927 1928) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-9056.90 My,Ed=-552.62 Mz,Ed=-269.49
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=458.65
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.59 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=31066.50 λ_{LT}=0.58
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
λ_Y=75.65 Ncr,y=210307.00 λ^*_y=0.99 Curva b: Φ_y=1.12 χ_y=0.60
λ_Z=100.33 Ncr,z=119551.00 λ^*_z=1.31 Curva c: Φ_z=1.63 χ_z=0.38
Kyy, Kyz, Kzy, Kzz = 0.99, 1.02, 0.79, 1.02
Verifica YY: 0.08 + 0.06 + 0.07 = 0.21
Verifica ZZ: 0.12 + 0.05 + 0.07 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.03 (L/16470) $f_{Z,G}$=0.00 (L/126559)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.17 (L/2725) $f_{Z,G}$=0.02 (L/21566)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-9056.90 T_z=-120.49 M_y=-552.62 T_y=121.45 M_z=-269.49
Tensioni: σ_N=-155.97 σ_M=-427.75 τ=0.00 σ_{max}=-583.73
Tensioni: σ_N=-155.97 σ_M=-14.44 τ=7.28 τ_{max}=7.28
Tensioni: σ_N=-155.97 σ_M=-427.75 τ=0.00 $\sigma_{ID,max}$=583.73

Asta n. 4223 (1921 1923) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3676.55 My,Ed=-1203.95 Mz,Ed=-2498.00
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=363.03
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.63 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=42465.80 λ_{LT}=0.49
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.61 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=59.88 Ncr,y=335675.00 λ^*_y=0.78 Curva b: Φ_y=0.91 χ_y=0.73
λ_Z=79.42 Ncr,z=190818.00 λ^*_z=1.04 Curva c: Φ_z=1.25 χ_z=0.52
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.12 + 0.64 = 0.77
Verifica ZZ: 0.02 + 0.09 + 0.64 = 0.75

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.06 (L/5938) $f_{Z,L}$=0.03 (L/12008)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.34 (L/1055) $f_{Z,L}$=0.17 (L/2121)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3676.55 T_z=-331.64 M_y=-1203.95 T_y=749.52 M_z=-2498.00
  Tensioni: σ_N=-63.32 σ_M=-2624.90 τ=0.00 σ_{max}=-2688.21
  Tensioni: σ_N=-63.32 σ_M=194.88 τ=26.28 τ_{max}=26.28
  Tensioni: σ_N=-63.32 σ_M=-2624.90 τ=0.00 $\sigma_{ID,max}$=2688.21

Asta n. 4224 (1918 1919) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-11101.80 My,Ed=523.12 Mz,Ed=263.63
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=426.15
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=4.26 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=34185.30 λ_{LT}=0.55
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
  λ_Y=70.29 Ncr,y=243609.00 λ^*_y=0.92 Curva b: Φ_y=1.05 χ_y=0.65
  λ_Z=93.22 Ncr,z=138482.00 λ^*_z=1.22 Curva c: Φ_z=1.49 χ_z=0.42
  Kyy, Kyz, Kzy, Kzz = 1.00, 1.03, 0.80, 1.03
  Verifica YY: 0.09 + 0.05 + 0.07 = 0.21
  Verifica ZZ: 0.13 + 0.04 + 0.07 = 0.25

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.02 (L/25979) $f_{Z,G}$=0.01 (L/32856)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.10 (L/4129) $f_{Z,G}$=0.08 (L/5066)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-11101.80 T_z=122.76 M_y=523.12 T_y=8.70 M_z=262.48
  Tensioni: σ_N=-191.19 σ_M=-411.46 τ=0.00 σ_{max}=-602.65
  Tensioni: σ_N=-191.19 σ_M=14.06 τ=7.39 τ_{max}=7.39
  Tensioni: σ_N=-191.19 σ_M=-411.46 τ=0.00 $\sigma_{ID,max}$=602.65

Asta n. 4232 (-852 1930) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-4529.17 My,Ed=-87.95 Mz,Ed=-723.47
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=248865.00 λ_{LT}=0.20
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.02 + 0.01 + 0.18 = 0.21
  Verifica ZZ: 0.02 + 0.01 + 0.18 = 0.21

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/41796)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/6713) $f_{Z,L}$=0.00 (L/80980)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-4529.17 T_z=-71.18 M_y=-87.95 T_y=618.71 M_z=-723.47
  Tensioni: σ_N=-78.00 σ_M=-671.05 τ=0.00 σ_{max}=-749.05
  Tensioni: σ_N=-78.00 σ_M=-14.74 τ=16.73 τ_{max}=16.73
  Tensioni: σ_N=-78.00 σ_M=-671.05 τ=0.00 $\sigma_{ID,max}$=749.05

Asta n. 4232 (-851 -852) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3115.42 My,Ed=-87.95 Mz,Ed=-723.47
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.15 M,cr=163309.00 λ_{LT}=0.25
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.01 + 0.18 = 0.21
  Verifica ZZ: 0.02 + 0.01 + 0.18 = 0.20

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/29447)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/5288) $f_{Z,L}$=0.00 (L/46274)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.24 - Classe 3
  Sollecitazioni: N=-3084.60 T_z=19.80 M_y=-87.95 T_y=-430.97 M_z=-723.47
  Tensioni: σ_N=-53.12 σ_M=-671.05 τ=0.00 σ_{max}=-724.17
  Tensioni: σ_N=-53.12 σ_M=-14.74 τ=11.41 τ_{max}=11.41
  Tensioni: σ_N=-53.12 σ_M=-671.05 τ=0.00 $\sigma_{ID,max}$=724.17

Asta n. 4232 (-850 -851) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3146.23 My,Ed=-63.49 Mz,Ed=-231.98
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.22 M,cr=173201.00 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.01 + 0.06 = 0.08
  Verifica ZZ: 0.02 + 0.00 + 0.06 = 0.08

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.00 (L/53986) $f_{Z,G}$=0.00 (L/86378)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.24 - Classe 3
  Sollecitazioni: N=-3115.42 T_z=19.80 M_y=-63.49 T_y=-364.55 M_z=-231.98
  Tensioni: σ_N=-53.65 σ_M=-227.24 τ=0.00 σ_{max}=-280.89
  Tensioni: σ_N=-53.65 σ_M=4.91 τ=9.67 τ_{max}=9.67
  Tensioni: σ_N=-53.65 σ_M=-227.24 τ=0.00 $\sigma_{ID,max}$=280.89

Asta n. 4232 (-849 -850) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3177.04 My,Ed=-39.03 Mz,Ed=504.79
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.40 M,cr=199088.00 λ_{LT}=0.23
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.00 + 0.13 = 0.15
  Verifica ZZ: 0.02 + 0.00 + 0.13 = 0.15

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/44678)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/6644) $f_{Z,L}$=0.00 (L/107973)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3177.04 T_z=19.80 M_y=-14.56 T_y=-231.70 M_z=504.79
  Tensioni: σ_N=-54.71 σ_M=-452.20 τ=0.00 σ_{max}=-506.92
  Tensioni: σ_N=-54.71 σ_M=31.02 τ=6.20 τ_{max}=6.20
  Tensioni: σ_N=-54.71 σ_M=-452.20 τ=0.00 $\sigma_{ID,max}$=506.92

Asta n. 4232 (1927 -849) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3207.86 My,Ed=-14.56 Mz,Ed=750.06
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.17 M,cr=167065.00 λ_{LT}=0.25
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.00 + 0.19 = 0.21
  Verifica ZZ: 0.02 + 0.00 + 0.19 = 0.20

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/20566)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.03 (L/3788)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3207.86 T_z=19.80 M_y=9.90 T_y=-165.28 M_z=750.06
  Tensioni: σ_N=-55.24 σ_M=-667.91 τ=0.00 σ_{max}=-723.15
  Tensioni: σ_N=-55.24 σ_M=37.48 τ=4.48 τ_{max}=4.48
  Tensioni: σ_N=-55.24 σ_M=-667.91 τ=0.00 $\sigma_{ID,max}$=723.15

Asta n. 4234 (1918 -848) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3909.88 My,Ed=261.29 Mz,Ed=599.97
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.67 M,cr=176946.00 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.02 + 0.03 + 0.15 = 0.20
  Verifica ZZ: 0.02 + 0.02 + 0.15 = 0.19

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/23413) $f_{Z,L}$=0.00 (L/126824)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.03 (L/4476) $f_{Z,L}$=0.01 (L/22380)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3909.88 T_z=165.79 M_y=261.29 T_y=-83.10 M_z=599.97
  Tensioni: σ_N=-67.33 σ_M=-620.92 τ=0.00 σ_{max}=-688.25
  Tensioni: σ_N=-67.33 σ_M=32.14 τ=9.99 τ_{max}=9.99
  Tensioni: σ_N=-67.33 σ_M=-620.92 τ=0.00 $\sigma_{ID,max}$=688.25

Asta n. 4234 (-848 -853) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3855.24 My,Ed=-219.95 Mz,Ed=431.17
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.65 M,cr=175372.00 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.02 + 0.02 + 0.11 = 0.15
  Verifica ZZ: 0.02 + 0.02 + 0.11 = 0.14

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/50729) $f_{Z,L}$=0.00 (L/126824)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/7387) $f_{Z,L}$=0.00 (L/31706)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3855.24 T_z=165.79 M_y=20.67 T_y=-149.52 M_z=431.17
  Tensioni: σ_N=-66.39 σ_M=-389.07 τ=0.00 σ_{max}=-455.46
  Tensioni: σ_N=-66.39 σ_M=23.10 τ=10.01 τ_{max}=10.01
  Tensioni: σ_N=-66.39 σ_M=-389.07 τ=0.00 $\sigma_{ID,max}$=455.46

Asta n. 4234 (-853 -854) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3800.61 My,Ed=-460.57 Mz,Ed=-195.66
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.32 M,cr=139641.00 λ_{LT}=0.27
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.02 + 0.04 + 0.05 = 0.11
  Verifica ZZ: 0.02 + 0.04 + 0.05 = 0.10

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.00 (L/47559)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.01 (L/10012) $f_{Z,G}$=0.00 (L/80099)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.45 - Classe 3
  Sollecitazioni: N=-3745.97 T_z=165.79 M_y=-460.57 T_y=-282.36 M_z=-195.66
  Tensioni: σ_N=-64.51 σ_M=-330.87 τ=0.00 σ_{max}=-395.38
  Tensioni: σ_N=-64.51 σ_M=115.26 τ=11.42 τ_{max}=11.42
  Tensioni: σ_N=-64.51 σ_M=-330.87 τ=0.00 $\sigma_{ID,max}$=395.38

Asta n. 4234 (-854 -855) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3745.97 My,Ed=-701.18 Mz,Ed=-653.69
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.19 M,cr=126150.00 λ_{LT}=0.29
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.02 + 0.07 + 0.16 = 0.25
  Verifica ZZ: 0.02 + 0.05 + 0.16 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.00 (L/31706) $f_{Z,G}$=0.00 (L/35392)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.03 (L/5764) $f_{Z,G}$=0.02 (L/6112)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.45 - Classe 3
  Sollecitazioni: N=-3691.34 T_z=165.79 M_y=-701.18 T_y=-348.79 M_z=-653.69
  Tensioni: σ_N=-63.57 σ_M=-818.95 τ=0.00 σ_{max}=-882.52
  Tensioni: σ_N=-63.57 σ_M=156.42 τ=12.63 τ_{max}=12.63
  Tensioni: σ_N=-63.57 σ_M=-818.95 τ=0.00 $\sigma_{ID,max}$=882.52

Asta n. 4234 (-855 1931) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7658.15 My,Ed=-701.19 Mz,Ed=-653.69
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=185555.00 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.96, 0.77, 0.96
  Verifica YY: 0.04 + 0.07 + 0.16 = 0.27
  Verifica ZZ: 0.04 + 0.05 + 0.16 = 0.26

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.00 (L/42274) $f_{Z,G}$=0.00 (L/50729)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/8095) $f_{Z,L}$=0.02 (L/8271)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-7658.15 T_z=-483.11 M_y=-701.19 T_y=483.60 M_z=-653.69
  Tensioni: σ_N=-131.88 σ_M=-818.95 τ=0.00 σ_{max}=-950.84
  Tensioni: σ_N=-131.88 σ_M=-35.02 τ=29.19 τ_{max}=29.19
  Tensioni: σ_N=-131.88 σ_M=-818.95 τ=0.00 $\sigma_{ID,max}$=950.84

Asta n. 5001 (1938 1939) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-5759.17 My,Ed=-2391.39 Mz,Ed=2973.83
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=700.73
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.01 Curva b: α-imp=0.34 k_c=0.94 ψ=1.45 M,cr=33726.70 λ_{LT}=0.72
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.75 β_{LT}=0.75 f=0.97 χ_{LT}=0.88
  λ_Y=98.01 Ncr,y=183603.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.44
  λ_Z=134.26 Ncr,z=97842.80 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24

Kyy, Kyz, Kzy, Kzz = 0.98, 1.00, 0.78, 1.00
Verifica YY: 0.05 + 0.16 + 0.47 = 0.68
Verifica ZZ: 0.08 + 0.13 + 0.47 = 0.68

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/89606) $f_{Z,L}$=0.01 (L/131208)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.05 (L/15452) $f_{Z,L}$=0.03 (L/23856)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.01 - Classe 3
Sollecitazioni: N=-6699.59 T_z=-12.49 M_y=-8.95 T_y=863.11 M_z=3539.92
Tensioni: σ_N=-78.73 σ_M=-1910.73 τ=0.00 σ_{max}=-1989.47
Tensioni: σ_N=-78.73 σ_M=138.89 τ=16.48 τ_{max}=16.48
Tensioni: σ_N=-78.73 σ_M=-1910.73 τ=0.00 $\sigma_{ID,max}$=1989.47

Asta n. 5002 (1932 1933) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-18325.70 My,Ed=-621.05 Mz,Ed=2625.73
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=702.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=7.02 Curva b: α-imp=0.34 k_c=0.94 ψ=1.61 M,cr=37235.00 λ_{LT}=0.69
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.73 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
λ_Y=98.21 Ncr,y=182868.00 λ^*_y=1.29 Curva b: Φ_y=1.51 χ_y=0.43
λ_Z=134.53 Ncr,z=97451.20 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
Kyy, Kyz, Kzy, Kzz = 1.03, 1.10, 0.83, 1.10
Verifica YY: 0.15 + 0.04 + 0.46 = 0.65
Verifica ZZ: 0.26 + 0.03 + 0.46 = 0.76

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.01 (L/55776) $f_{Z,G}$=0.01 (L/73624)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.07 (L/9536) $f_{Z,G}$=0.06 (L/12542)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-18325.70 T_z=-98.66 M_y=-621.05 T_y=-693.33 M_z=2625.73 M_x=7.52
Tensioni: σ_N=-215.36 σ_M=-1540.88 τ=7.53 σ_{max}=-1756.24
Tensioni: σ_N=-215.36 σ_M=202.11 τ=29.75 τ_{max}=29.75
Tensioni: σ_N=-215.36 σ_M=-1540.88 τ=7.53 $\sigma_{ID,max}$=1756.29

Asta n. 5004 (1870 1871) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-5176.94 My,Ed=-3545.12 Mz,Ed=2659.72
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=700.78
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=7.01 Curva b: α-imp=0.34 k_c=0.94 ψ=1.44 M,cr=33396.30 λ_{LT}=0.73
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.75 β_{LT}=0.75 f=0.97 χ_{LT}=0.88
λ_Y=98.02 Ncr,y=183579.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.44
λ_Z=134.27 Ncr,z=97829.90 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
Verifica YY: 0.04 + 0.23 + 0.42 = 0.69
Verifica ZZ: 0.07 + 0.19 + 0.42 = 0.68

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.01 (L/78172)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.05 (L/13098) $f_{Z,G}$=0.05 (L/15042)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.01 - Classe 3
Sollecitazioni: N=-6696.13 T_z=-8.05 M_y=-72.64 T_y=879.70 M_z=3598.56 M_x=-1.14
Tensioni: σ_N=-78.69 σ_M=-1955.17 τ=1.14 σ_{max}=-2033.86
Tensioni: σ_N=-78.69 σ_M=151.44 τ=17.93 τ_{max}=17.93
Tensioni: σ_N=-78.69 σ_M=-1955.17 τ=1.14 $\sigma_{ID,max}$=2033.86

Asta n. 5004 (1934 1935) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-14915.70 My,Ed=-745.02 Mz,Ed=2275.39
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=702.06
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=7.02 Curva b: α-imp=0.34 k_c=0.94 ψ=1.65 M,cr=38110.60 λ_{LT}=0.68
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.72 β_{LT}=0.75 f=0.97 χ_{LT}=0.91

λ_Y=98.19 Ncr,y=182908.00 λ^*_y=1.29 Curva b: Φ_y=1.51 χ_y=0.43
λ_Z=134.51 Ncr,z=97472.40 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
Kyy, Kyz, Kzy, Kzz = 1.02, 1.07, 0.81, 1.07
Verifica YY: 0.12 + 0.05 + 0.39 = 0.56
Verifica ZZ: 0.21 + 0.04 + 0.39 = 0.64

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.02 (L/44888) $f_{Z,G}$=0.01 (L/73986)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.09 (L/7668) $f_{Z,G}$=0.06 (L/12638)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-14915.70 T_z=-116.43 M_y=-745.02 T_y=-580.47 M_z=2275.39 M_x=8.08
Tensioni: σ_N=-175.29 σ_M=-1376.89 τ=8.09 σ_{max}=-1552.18
Tensioni: σ_N=-175.29 σ_M=208.50 τ=30.99 τ_{max}=30.99
Tensioni: σ_N=-175.29 σ_M=-1376.89 τ=8.09 $\sigma_{ID,max}$=1552.25

Asta n. 5005 (-880 -860) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/25420)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.07 (L/4609)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-13131.90
N,Ed=-13131.90 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.18

- Verifica di stabilità (4.2.4.1.3.1) - CC 25
Sollecitazioni: N=-13131.90 L=320.00
λ=79.28 Ncr=70851.00 λ^*=1.04
Curva a: Φ=1.13 χ,min=0.64 N,Ed=-13131.90 Nb,Rd=46443.40 N,Ed/Nb,Rd=0.28

Asta n. 5006 (-881 -863) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/24672)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.04 (L/4497)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-13606.30
N,Ed=-13606.30 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.19

- Verifica di stabilità (4.2.4.1.3.1) - CC 25
Sollecitazioni: N=-13606.30 L=160.00
λ=39.64 Ncr=283404.00 λ^*=0.52
Curva a: Φ=0.67 χ,min=0.92 N,Ed=-13606.30 Nb,Rd=66718.00 N,Ed/Nb,Rd=0.20

Asta n. 5007 (1947 2002) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.01 (L/30146)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.61 - Classe 3
Sollecitazioni: N=5061.72
Tensioni: σ_N=235.56 σ_M=0.00 τ=0.00 σ_{max}=235.56
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=235.56 σ_M=0.00 τ=0.00 $\sigma_{ID,max}$=235.56

Asta n. 5008 (1948 2003) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/52756)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/10048)

- Verifica a compressione (4.2.10) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-7477.80
N,Ed=-7477.80 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.10

Asta n. 5009 (2003 1947) Cir. D=4 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 15 - Classe 3
  Sollecitazioni: N,Ed=-3835.95 M,Ed=4.05
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=259.36
  λ=259.36 Ncr=3872.04 λ^*=3.39 Curva c: Φ=7.04 χ,min=0.08
  χ,min=0.08
  Verifica: 1.19 + 2.04 = 3.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/143133)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.14 (L/1815) $f_{Z,G}$=0.09 (L/2943)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.30 - Classe 3
  Sollecitazioni: N=-4593.83 M=5.39
  Tensioni: σ_N=-365.57 σ_M=-85.86 τ=0.00 σ_{max}=-451.43
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-365.57 σ_M=-85.86 τ=0.00 $\sigma_{ID,max}$=451.43

Asta n. 5010 (2002 1948) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 25 - Classe 3
  L_{cr}=2.10 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
  $\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
  CC 25 My,Ed=-5.68 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 23 - Classe 3
  Sollecitazioni: N,Ed=-807.13 M,Ed=3.28
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=209.96
  λ=209.96 Ncr=5908.50 λ^*=2.75 Curva c: Φ=4.90 χ,min=0.11
  χ,min=0.11
  Verifica: 0.17 + 0.02 = 0.19

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.08 (L/2772) $f_{Z,G}$=0.06 (L/3305)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.05 - Classe 3
  Sollecitazioni: N=6222.77 M=4.37
  Tensioni: σ_N=495.19 σ_M=69.51 τ=0.00 σ_{max}=564.70
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=495.19 σ_M=69.51 τ=0.00 $\sigma_{ID,max}$=564.70

Asta n. 5011 (1944 2000) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/120586)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/20587)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.61 - Classe 3
  Sollecitazioni: N=4975.41
  Tensioni: σ_N=231.54 σ_M=0.00 τ=0.00 σ_{max}=231.54
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=231.54 σ_M=0.00 τ=0.00 $\sigma_{ID,max}$=231.54

Asta n. 5012 (1945 2001) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-7494.50 M,Ed=0.00
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=161.00
  αmy, αmz, αLT = 0.95, ----, ----
  λ=39.89 Ncr=279894.00 λ^*=0.52
  Curva a: Φ=0.67 χ,min=0.92
  Kyy, Kyz, Kzy, Kzz = 0.98, ----, ----, ----
  Verifica: 0.10 = 0.10

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/84410)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/13837)

- Verifica a compressione (4.2.10) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-7494.50
  N,Ed=-7494.50 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.10

Asta n. 5013 (1944 2001) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 23 - Classe 3
  L_{cr}=2.59 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
  $\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
  CC 23 My,Ed=-5.39 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-3432.32 M,Ed=4.05
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=259.36
  λ=259.36 Ncr=3872.04 λ^*=3.39 Curva c: Φ=7.04 χ,min=0.08
  χ,min=0.08
  Verifica: 1.07 + 0.17 = 1.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/113313)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.14 (L/1814) $f_{Z,G}$=0.10 (L/2602)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.30 - Classe 3
  Sollecitazioni: N=-6710.73 M=5.39
  Tensioni: σ_N=-534.02 σ_M=-85.86 τ=0.00 σ_{max}=-619.88
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-534.02 σ_M=-85.86 τ=0.00 $\sigma_{ID,max}$=619.88

Asta n. 5014 (1945 2000) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 25 - Classe 3
  L_{cr}=2.10 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
  $\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
  CC 25 My,Ed=-5.68 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 23 - Classe 3
  Sollecitazioni: N,Ed=-454.29 M,Ed=3.28
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=209.96
  λ=209.96 Ncr=5908.50 λ^*=2.75 Curva c: Φ=4.90 χ,min=0.11
  χ,min=0.11
  Verifica: 0.10 + 0.02 = 0.11

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/110076)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.08 (L/2772) $f_{Z,G}$=0.06 (L/3776)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.05 - Classe 3
  Sollecitazioni: N=9332.68 M=4.37
  Tensioni: σ_N=742.67 σ_M=69.51 τ=0.00 σ_{max}=812.18
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=742.67 σ_M=69.51 τ=0.00 $\sigma_{ID,max}$=812.18

Asta n. 5015 (1939 1935) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2495.74 M,Ed=2.86
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=102.22
  αmy, αmz, αLT = 0.95, ----, ----
  λ=25.33 Ncr=694405.00 λ^*=0.33
  Curva a: Φ=0.57 χ,min=0.97
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.03 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.51 - Classe 3
  Sollecitazioni: N=-2495.74 M=2.86
  Tensioni: σ_N=-116.14 σ_M=-4.91 τ=0.00 σ_{max}=-121.05
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-116.14 σ_M=-4.91 τ=0.00 $\sigma_{ID,max}$=121.05

Asta n. 5016 (1935 1937) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2850.76 M,Ed=4.01
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=120.97
  αmy, αmz, αLT = 0.95, ----, ----

λ=29.97 Ncr=495806.00 λ^*=0.39
Curva a: Φ=0.60 χ,min=0.95
Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.60 - Classe 3
Sollecitazioni: N=-2850.76 M=4.01
Tensioni: σ_N=-132.66 σ_M=-6.88 τ=0.00 σ_{max}=-139.54
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=-132.66 σ_M=-6.88 τ=0.00 $\sigma_{ID,max}$=139.54

Asta n. 5017 (1937 1933) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-2447.89 M,Ed=2.89
Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=102.73
αmy, αmz, αLT = 0.95, ----, ----
λ=25.45 Ncr=687497.00 λ^*=0.33
Curva a: Φ=0.57 χ,min=0.97
Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
Verifica: 0.03 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.51 - Classe 3
Sollecitazioni: N=-2447.89 M=2.89
Tensioni: σ_N=-113.92 σ_M=-4.96 τ=0.00 σ_{max}=-118.87
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=-113.92 σ_M=-4.96 τ=0.00 $\sigma_{ID,max}$=118.87

Asta n. 5018 (1933 1939) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-2847.03 M,Ed=3.97
Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=120.28
αmy, αmz, αLT = 0.95, ----, ----
λ=29.80 Ncr=501459.00 λ^*=0.39
Curva a: Φ=0.60 χ,min=0.96
Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.60 - Classe 3
Sollecitazioni: N=-2847.03 M=3.97
Tensioni: σ_N=-132.49 σ_M=-6.80 τ=0.00 σ_{max}=-139.29
Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
Tensioni: σ_N=-132.49 σ_M=-6.80 τ=0.00 $\sigma_{ID,max}$=139.29

Asta n. 5101 (1939 1946) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-7042.14 My,Ed=402.95 Mz,Ed=-4884.81
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=526.58
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=5.27 Curva b: α-imp=0.34 k_c=0.94 ψ=1.73 M,cr=56525.10 λ_{LT}=0.56
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_Y=73.65 Ncr,y=325125.00 λ^*_y=0.96 Curva b: Φ_y=1.09 χ_y=0.62
λ_Z=100.89 Ncr,z=173260.00 λ^*_z=1.32 Curva c: Φ_z=1.65 χ_z=0.38
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
Verifica YY: 0.04 + 0.02 + 0.77 = 0.83
Verifica ZZ: 0.06 + 0.02 + 0.77 = 0.85

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/38884) $f_{Z,L}$=0.01 (L/52090)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.09 (L/6054) $f_{Z,L}$=0.06 (L/9141)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=5.27 - Classe 3
Sollecitazioni: N=-6590.59 T_z=-78.23 M_y=402.95 T_y=-1635.92 M_z=-4884.81
Tensioni: σ_N=-77.45 σ_M=-2715.23 τ=0.00 σ_{max}=-2792.69
Tensioni: σ_N=-77.45 σ_M=-254.65 τ=31.32 τ_{max}=31.32
Tensioni: σ_N=-77.45 σ_M=-2715.23 τ=0.00 $\sigma_{ID,max}$=2792.69

Asta n. 5102 (1933 1949) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-18615.30 My,Ed=-322.66 Mz,Ed=-2372.71

Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=553.99
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=5.54 Curva b: α-imp=0.34 k_c=0.94 ψ=1.54 M,cr=47484.50 λ_{LT}=0.61
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.68 β_{LT}=0.75 f=0.97 χ_{LT}=0.94
λ_Y=77.48 Ncr,y=293755.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
λ_Z=106.14 Ncr,z=156543.00 λ^*_z=1.39 Curva c: Φ_z=1.76 χ_z=0.35
Kyy, Kyz, Kzy, Kzz = 1.01, 1.05, 0.81, 1.05
Verifica YY: 0.11 + 0.02 + 0.40 = 0.53
Verifica ZZ: 0.18 + 0.02 + 0.40 = 0.60

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.02 (L/33384) $f_{Z,L}$=0.00 (L/132021)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.09 (L/5933) $f_{Z,L}$=0.02 (L/23423)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-18615.30 T_z=65.98 M_y=67.02 T_y=770.98 M_z=-2372.71 M_x=-9.82
Tensioni: σ_N=-218.77 σ_M=-1292.99 τ=9.84 σ_{max}=-1511.75
Tensioni: σ_N=-218.77 σ_M=-102.93 τ=36.00 τ_{max}=36.00
Tensioni: σ_N=-218.77 σ_M=-1292.99 τ=9.84 $\sigma_{ID,max}$=1511.85

Asta n. 5103 (1937 1943) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-7042.14 My,Ed=116.10 Mz,Ed=-4891.02
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=526.43
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=5.26 Curva b: α-imp=0.34 k_c=0.94 ψ=1.22 M,cr=39967.10 λ_{LT}=0.66
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.71 β_{LT}=0.75 f=0.97 χ_{LT}=0.91
λ_Y=73.63 Ncr,y=325318.00 λ^*_y=0.96 Curva b: Φ_y=1.09 χ_y=0.62
λ_Z=100.86 Ncr,z=173363.00 λ^*_z=1.32 Curva c: Φ_z=1.65 χ_z=0.38
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
Verifica YY: 0.04 + 0.01 + 0.77 = 0.82
Verifica ZZ: 0.06 + 0.01 + 0.77 = 0.84

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/39712) $f_{Z,L}$=0.00 (L/501815)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.09 (L/6174) $f_{Z,L}$=0.01 (L/51588)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=5.26 - Classe 3
Sollecitazioni: N=-6590.59 T_z=-35.53 M_y=116.10 T_y=-1648.68 M_z=-4891.02 M_x=6.80
Tensioni: σ_N=-77.45 σ_M=-2660.88 τ=6.82 σ_{max}=-2738.33
Tensioni: σ_N=-77.45 σ_M=-208.63 τ=38.65 τ_{max}=38.65
Tensioni: σ_N=-77.45 σ_M=-2660.88 τ=6.82 $\sigma_{ID,max}$=2738.36

Asta n. 5104 (1935 1940) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-20197.20 My,Ed=-103.11 Mz,Ed=-1870.63
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=553.99
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=5.54 Curva b: α-imp=0.34 k_c=0.94 ψ=1.30 M,cr=39854.40 λ_{LT}=0.67
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.71 β_{LT}=0.75 f=0.97 χ_{LT}=0.91
λ_Y=77.48 Ncr,y=293755.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
λ_Z=106.14 Ncr,z=156543.00 λ^*_z=1.39 Curva c: Φ_z=1.76 χ_z=0.35
Kyy, Kyz, Kzy, Kzz = 1.02, 1.06, 0.81, 1.06
Verifica YY: 0.12 + 0.01 + 0.32 = 0.44
Verifica ZZ: 0.20 + 0.01 + 0.32 = 0.52

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.02 (L/35857) $f_{Z,L}$=0.00 (L/363059)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.09 (L/6447) $f_{Z,L}$=0.01 (L/69154)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-20197.20 T_z=28.00 M_y=52.02 T_y=744.26 M_z=-1870.63 M_x=-7.04
Tensioni: σ_N=-237.36 σ_M=-1019.22 τ=7.06 σ_{max}=-1256.57
Tensioni: σ_N=-237.36 σ_M=-81.02 τ=27.00 τ_{max}=27.00
Tensioni: σ_N=-237.36 σ_M=-1019.22 τ=7.06 $\sigma_{ID,max}$=1256.63

Asta n. 5105 (-860 2004) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-11549.50 M,Ed=0.12
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=78.22
  αmy, αmz, αLT = 0.95, ----, ----
  λ=19.38 Ncr=1185880.00 λ^*=0.25
  Curva a: Φ=0.54 χ,min=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
  Verifica: 0.16 + 0.00 = 0.16

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/27338)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/5257)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-11549.50
  N,Ed=-11549.50 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.16

Asta n. 5106 (-863 2005) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-10739.30 M,Ed=0.29
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=66.17
  αmy, αmz, αLT = 0.95, ----, ----
  λ=16.39 Ncr=1657040.00 λ^*=0.21
  Curva a: Φ=0.52 χ,min=1.00
  Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
  Verifica: 0.15 + 0.00 = 0.15

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/31537)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/6086)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-10739.30 T=1.76
  N,Ed=-10739.30 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.15

Asta n. 5211 (1946 1948) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3296.87 My,Ed=1263.87 Mz,Ed=-1994.86
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=379.60
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=3.80 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=39930.60 λ_{LT}=0.51
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.62 β_{LT}=0.75 f=0.98 χ_{LT}=0.98
  λ_Y=62.61 Ncr,y=307021.00 λ^*_y=0.82 Curva b: Φ_y=0.94 χ_y=0.71
  λ_Z=83.04 Ncr,z=174529.00 λ^*_z=1.09 Curva c: Φ_z=1.31 χ_z=0.49
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
  Verifica YY: 0.02 + 0.13 + 0.51 = 0.65
  Verifica ZZ: 0.02 + 0.10 + 0.51 = 0.62

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.06 (L/6622) $f_{Z,L}$=0.03 (L/10995)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.32 (L/1187) $f_{Z,L}$=0.20 (L/1945)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3296.87 T_z=332.95 M_y=1263.87 T_y=595.19 M_z=-1994.86
  Tensioni: σ_N=-56.78 σ_M=-2199.62 τ=0.00 σ_{max}=-2256.40
  Tensioni: σ_N=-56.78 σ_M=-451.92 τ=23.42 τ_{max}=23.42
  Tensioni: σ_N=-56.78 σ_M=-2199.62 τ=0.00 $\sigma_{ID,max}$=2256.40

Asta n. 5212 (1946 1947) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3555.81 My,Ed=-1159.06 Mz,Ed=-2514.56
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=334.12
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=3.34 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=47739.80 λ_{LT}=0.47
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.59 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=55.11 Ncr,y=396295.00 λ^*_y=0.72 Curva b: Φ_y=0.85 χ_y=0.77

λ_z=73.09 Ncr,z=225278.00 λ^*_z=0.96 Curva c: Φ_z=1.14 χ_z=0.57
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.11 + 0.64 = 0.77
Verifica ZZ: 0.02 + 0.09 + 0.64 = 0.75

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{z,G}$=0.06 (L/5878) $f_{z,L}$=0.02 (L/13371)

- Verifica Freccia massima carichi totali - CC 26
$f_{z,G}$=0.32 (L/1042) $f_{z,L}$=0.14 (L/2399)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3555.81 T_z=-346.90 M_y=-1159.06 T_y=814.03 M_z=-2514.56
Tensioni: σ_N=-61.24 σ_M=-2624.22 τ=0.00 σ_{max}=-2685.45
Tensioni: σ_N=-61.24 σ_M=181.74 τ=28.09 τ_{max}=28.09
Tensioni: σ_N=-61.24 σ_M=-2624.22 τ=0.00 $\sigma_{ID,max}$=2685.45

Asta n. 5212 (1949 1951) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-11653.00 My,Ed=657.96 Mz,Ed=241.88
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=437.01
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.37 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=33075.30 λ_{LT}=0.56
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_y=72.08 Ncr,y=231653.00 λ^*_y=0.94 Curva b: Φ_y=1.07 χ_y=0.63
λ_z=95.60 Ncr,z=131685.00 λ^*_z=1.25 Curva c: Φ_z=1.54 χ_z=0.41
Kyy, Kyz, Kzy, Kzz = 1.00, 1.03, 0.80, 1.03
Verifica YY: 0.09 + 0.07 + 0.07 = 0.23
Verifica ZZ: 0.14 + 0.06 + 0.07 = 0.27

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{z,L}$=0.02 (L/19751) $f_{z,G}$=0.01 (L/34453)

- Verifica Freccia massima carichi totali - CC 26
$f_{z,L}$=0.14 (L/3217) $f_{z,G}$=0.08 (L/5285)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-11653.00 T_z=150.56 M_y=657.96 T_y=15.83 M_z=237.99
Tensioni: σ_N=-200.68 σ_M=-435.88 τ=0.00 σ_{max}=-636.56
Tensioni: σ_N=-200.68 σ_M=12.75 τ=9.06 τ_{max}=9.06
Tensioni: σ_N=-200.68 σ_M=-435.88 τ=0.00 $\sigma_{ID,max}$=636.56

Asta n. 5213 (1943 1944) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3183.15 My,Ed=1056.35 Mz,Ed=-2060.58
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=352.04
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.52 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=44330.50 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_y=58.06 Ncr,y=356964.00 λ^*_y=0.76 Curva b: Φ_y=0.88 χ_y=0.75
λ_z=77.01 Ncr,z=202920.00 λ^*_z=1.01 Curva c: Φ_z=1.21 χ_z=0.54
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.10 + 0.52 = 0.64
Verifica ZZ: 0.02 + 0.08 + 0.52 = 0.62

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{z,G}$=0.05 (L/6442) $f_{z,L}$=0.02 (L/14089)

- Verifica Freccia massima carichi totali - CC 26
$f_{z,G}$=0.31 (L/1141) $f_{z,L}$=0.14 (L/2521)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3183.15 T_z=300.07 M_y=1056.35 T_y=654.99 M_z=-2060.58
Tensioni: σ_N=-54.82 σ_M=-2186.88 τ=0.00 σ_{max}=-2241.70
Tensioni: σ_N=-54.82 σ_M=-398.79 τ=23.32 τ_{max}=23.32
Tensioni: σ_N=-54.82 σ_M=-2186.88 τ=0.00 $\sigma_{ID,max}$=2241.70

Asta n. 5214 (1940 1942) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-8918.77 My,Ed=-879.10 Mz,Ed=-186.03
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=448.31
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.48 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=31994.10 λ_{LT}=0.57

$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.65 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_Y=73.94 Ncr,y=220115.00 λ^*_y=0.97 Curva b: Φ_y=1.10 χ_y=0.62
λ_Z=98.07 Ncr,z=125127.00 λ^*_z=1.28 Curva c: Φ_z=1.59 χ_z=0.40
Kyy, Kyz, Kzy, Kzz = 0.99, 1.02, 0.79, 1.02
Verifica YY: 0.07 + 0.09 + 0.05 = 0.22
Verifica ZZ: 0.11 + 0.07 + 0.05 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.03 (L/14177) $f_{Z,G}$=0.00 (L/138261)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.19 (L/2349) $f_{Z,G}$=0.02 (L/23741)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-8918.77 T_z=-196.09 M_y=-879.10 T_y=123.00 M_z=-186.03
Tensioni: σ_N=-153.59 σ_M=-465.47 τ=0.00 σ_{max}=-619.07
Tensioni: σ_N=-153.59 σ_M=-9.97 τ=11.82 τ_{max}=11.82
Tensioni: σ_N=-153.59 σ_M=-465.47 τ=0.00 $\sigma_{ID,max}$=619.07

Asta n. 5222 (1949 1950) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-9602.56 My,Ed=-721.72 Mz,Ed=-178.36
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=458.65
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.59 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=31066.50 λ_{LT}=0.58
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
λ_Y=75.65 Ncr,y=210307.00 λ^*_y=0.99 Curva b: Φ_y=1.12 χ_y=0.60
λ_Z=100.33 Ncr,z=119551.00 λ^*_z=1.31 Curva c: Φ_z=1.63 χ_z=0.38
Kyy, Kyz, Kzy, Kzz = 1.00, 1.02, 0.80, 1.02
Verifica YY: 0.08 + 0.08 + 0.05 = 0.21
Verifica ZZ: 0.13 + 0.06 + 0.05 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.03 (L/16993) $f_{Z,G}$=0.00 (L/123314)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.16 (L/2799) $f_{Z,G}$=0.02 (L/22060)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-9602.56 T_z=-157.36 M_y=-721.72 T_y=120.39 M_z=-178.36
Tensioni: σ_N=-165.37 σ_M=-404.85 τ=0.00 σ_{max}=-570.22
Tensioni: σ_N=-165.37 σ_M=-9.55 τ=9.49 τ_{max}=9.49
Tensioni: σ_N=-165.37 σ_M=-404.85 τ=0.00 $\sigma_{ID,max}$=570.22

Asta n. 5223 (1943 1945) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3676.60 My,Ed=-1191.96 Mz,Ed=-2503.13
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=363.03
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.63 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=42465.80 λ_{LT}=0.49
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.61 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=59.88 Ncr,y=335675.00 λ^*_y=0.78 Curva b: Φ_y=0.91 χ_y=0.73
λ_Z=79.42 Ncr,z=190818.00 λ^*_z=1.04 Curva c: Φ_z=1.25 χ_z=0.52
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.12 + 0.64 = 0.77
Verifica ZZ: 0.02 + 0.09 + 0.64 = 0.75

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.06 (L/5947) $f_{Z,L}$=0.03 (L/12084)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.34 (L/1054) $f_{Z,L}$=0.17 (L/2143)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3676.60 T_z=-328.33 M_y=-1191.96 T_y=750.94 M_z=-2503.13
Tensioni: σ_N=-63.32 σ_M=-2625.34 τ=0.00 σ_{max}=-2688.66
Tensioni: σ_N=-63.32 σ_M=191.33 τ=26.19 τ_{max}=26.19
Tensioni: σ_N=-63.32 σ_M=-2625.34 τ=0.00 $\sigma_{ID,max}$=2688.66

Asta n. 5224 (1940 1941) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-11080.30 My,Ed=528.77 Mz,Ed=259.58
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=426.15

αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.26 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=34185.30 λ_{LT}=0.55
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_Y=70.29 Ncr,y=243609.00 λ^*_y=0.92 Curva b: Φ_y=1.05 χ_y=0.65
λ_Z=93.22 Ncr,z=138482.00 λ^*_z=1.22 Curva c: Φ_z=1.49 χ_z=0.42
Kyy, Kyz, Kzy, Kzz = 1.00, 1.03, 0.80, 1.03
Verifica YY: 0.09 + 0.06 + 0.07 = 0.21
Verifica ZZ: 0.13 + 0.04 + 0.07 = 0.25

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.02 (L/26285) $f_{Z,G}$=0.01 (L/33852)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.10 (L/4084) $f_{Z,G}$=0.08 (L/5124)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-11080.30 T_z=124.08 M_y=528.77 T_y=9.71 M_z=258.15
Tensioni: σ_N=-190.82 σ_M=-409.56 τ=0.00 σ_{max}=-600.37
Tensioni: σ_N=-190.82 σ_M=13.83 τ=7.47 τ_{max}=7.47
Tensioni: σ_N=-190.82 σ_M=-409.56 τ=0.00 $\sigma_{ID,max}$=600.37

Asta n. 5232 (-860 1952) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-4505.19 My,Ed=-87.84 Mz,Ed=-718.05
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=248865.00 λ_{LT}=0.20
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.01 + 0.18 = 0.21
Verifica ZZ: 0.02 + 0.01 + 0.18 = 0.21

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/43189)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/6819) $f_{Z,L}$=0.00 (L/53986)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-4505.19 T_z=-71.09 M_y=-87.84 T_y=614.32 M_z=-718.05
Tensioni: σ_N=-77.59 σ_M=-666.21 τ=0.00 σ_{max}=-743.80
Tensioni: σ_N=-77.59 σ_M=-14.48 τ=16.62 τ_{max}=16.62
Tensioni: σ_N=-77.59 σ_M=-666.21 τ=0.00 $\sigma_{ID,max}$=743.80

Asta n. 5232 (-859 -860) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3110.87 My,Ed=-87.84 Mz,Ed=-718.05
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.14 M,cr=161654.00 λ_{LT}=0.25
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.02 + 0.01 + 0.18 = 0.20
Verifica ZZ: 0.02 + 0.01 + 0.18 = 0.20

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/31601)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/5376) $f_{Z,L}$=0.00 (L/46274)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.24 - Classe 3
Sollecitazioni: N=-3080.06 T_z=18.42 M_y=-87.84 T_y=-426.77 M_z=-718.05
Tensioni: σ_N=-53.04 σ_M=-666.21 τ=0.00 σ_{max}=-719.26
Tensioni: σ_N=-53.04 σ_M=-14.48 τ=11.29 τ_{max}=11.29
Tensioni: σ_N=-53.04 σ_M=-666.21 τ=0.00 $\sigma_{ID,max}$=719.26

Asta n. 5232 (-858 -859) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3141.68 My,Ed=-65.08 Mz,Ed=-231.75
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.19 M,cr=169806.00 λ_{LT}=0.25
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.01 + 0.06 = 0.08
  Verifica ZZ: 0.02 + 0.01 + 0.06 = 0.08

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.00 (L/53986) $f_{Z,G}$=0.00 (L/92548)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.24 - Classe 3
  Sollecitazioni: N=-3110.87 T_z=18.42 M_y=-65.08 T_y=-360.35 M_z=-231.75
  Tensioni: σ_N=-53.57 σ_M=-227.58 τ=0.00 σ_{max}=-281.15
  Tensioni: σ_N=-53.57 σ_M=5.35 τ=9.55 τ_{max}=9.55
  Tensioni: σ_N=-53.57 σ_M=-227.58 τ=0.00 $\sigma_{ID,max}$=281.15

Asta n. 5232 (-857 -858) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3172.50 My,Ed=-42.32 Mz,Ed=494.63
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.33 M,cr=188962.00 λ_{LT}=0.23
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.00 + 0.12 = 0.14
  Verifica ZZ: 0.02 + 0.00 + 0.12 = 0.14

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/46274)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/6819) $f_{Z,L}$=0.00 (L/107973)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3172.50 T_z=18.42 M_y=-19.56 T_y=-227.50 M_z=494.63
  Tensioni: σ_N=-54.64 σ_M=-444.91 τ=0.00 σ_{max}=-499.55
  Tensioni: σ_N=-54.64 σ_M=31.84 τ=6.08 τ_{max}=6.08
  Tensioni: σ_N=-54.64 σ_M=-444.91 τ=0.00 $\sigma_{ID,max}$=499.55

Asta n. 5232 (1949 -857) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3203.31 My,Ed=-19.56 Mz,Ed=734.71
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.59 M,cr=225594.00 λ_{LT}=0.21
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.02 + 0.00 + 0.18 = 0.20
  Verifica ZZ: 0.02 + 0.00 + 0.18 = 0.20

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/20566)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.03 (L/3822) $f_{Z,L}$=0.00 (L/107973)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3203.31 T_z=18.42 M_y=3.20 T_y=-161.08 M_z=734.71
  Tensioni: σ_N=-55.17 σ_M=-652.02 τ=0.00 σ_{max}=-707.18
  Tensioni: σ_N=-55.17 σ_M=38.48 τ=4.36 τ_{max}=4.36
  Tensioni: σ_N=-55.17 σ_M=-652.02 τ=0.00 $\sigma_{ID,max}$=707.18

Asta n. 5234 (1940 -856) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3889.25 My,Ed=262.66 Mz,Ed=601.88
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.66 M,cr=176029.00 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.02 + 0.03 + 0.15 = 0.20
  Verifica ZZ: 0.02 + 0.02 + 0.15 = 0.19

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/24157) $f_{Z,L}$=0.00 (L/95118)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.03 (L/4476) $f_{Z,L}$=0.01 (L/21137)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3889.25 T_z=165.09 M_y=262.66 T_y=-83.74 M_z=601.88
  Tensioni: σ_N=-66.98 σ_M=-623.07 τ=0.00 σ_{max}=-690.05
  Tensioni: σ_N=-66.98 σ_M=32.24 τ=9.95 τ_{max}=9.95
  Tensioni: σ_N=-66.98 σ_M=-623.07 τ=0.00 $\sigma_{ID,max}$=690.05

Asta n. 5234 (-856 -861) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3834.61 My,Ed=-216.56 Mz,Ed=432.14
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.64 M,cr=174065.00 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.02 + 0.02 + 0.11 = 0.15
  Verifica ZZ: 0.02 + 0.02 + 0.11 = 0.14

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/50729) $f_{Z,L}$=0.00 (L/95118)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/7316) $f_{Z,L}$=0.00 (L/31706)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3834.61 T_z=165.09 M_y=23.05 T_y=-150.16 M_z=432.14
  Tensioni: σ_N=-66.04 σ_M=-390.74 τ=0.00 σ_{max}=-456.78
  Tensioni: σ_N=-66.04 σ_M=23.15 τ=9.97 τ_{max}=9.97
  Tensioni: σ_N=-66.04 σ_M=-390.74 τ=0.00 $\sigma_{ID,max}$=456.78

Asta n. 5234 (-861 -862) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3779.98 My,Ed=-456.17 Mz,Ed=-196.55
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.32 M,cr=139870.00 λ_{LT}=0.27
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.02 + 0.04 + 0.05 = 0.11
  Verifica ZZ: 0.02 + 0.04 + 0.05 = 0.10

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.00 (L/54353)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.01 (L/9755) $f_{Z,G}$=0.00 (L/80099)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.45 - Classe 3
  Sollecitazioni: N=-3725.34 T_z=165.09 M_y=-456.17 T_y=-283.01 M_z=-196.55
  Tensioni: σ_N=-64.16 σ_M=-330.15 τ=0.00 σ_{max}=-394.31
  Tensioni: σ_N=-64.16 σ_M=114.01 τ=11.40 τ_{max}=11.40
  Tensioni: σ_N=-64.16 σ_M=-330.15 τ=0.00 $\sigma_{ID,max}$=394.31

Asta n. 5234 (-862 -863) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3725.34 My,Ed=-695.79 Mz,Ed=-655.51
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.19 M,cr=126235.00 λ_{LT}=0.29
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.02 + 0.07 + 0.16 = 0.25
  Verifica ZZ: 0.02 + 0.05 + 0.16 = 0.24

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.00 (L/31706) $f_{Z,G}$=0.00 (L/33819)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.03 (L/5764) $f_{Z,G}$=0.02 (L/6015)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.45 - Classe 3
  Sollecitazioni: N=-3670.71 T_z=165.09 M_y=-695.79 T_y=-349.43 M_z=-655.51
  Tensioni: σ_N=-63.22 σ_M=-818.72 τ=0.00 σ_{max}=-881.93
  Tensioni: σ_N=-63.22 σ_M=154.85 τ=12.62 τ_{max}=12.62
  Tensioni: σ_N=-63.22 σ_M=-818.72 τ=0.00 $\sigma_{ID,max}$=881.93

Asta n. 5234 (-863 1953) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7616.75 My,Ed=-695.79 Mz,Ed=-655.51
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=185555.00 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.96, 0.77, 0.96
  Verifica YY: 0.04 + 0.07 + 0.16 = 0.27
  Verifica ZZ: 0.04 + 0.05 + 0.16 = 0.26

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.00 (L/47559) $f_{Z,G}$=0.00 (L/50729)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/8009) $f_{Z,L}$=0.02 (L/8647)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-7616.75 T_z=-479.39 M_y=-695.79 T_y=484.85 M_z=-655.51
  Tensioni: σ_N=-131.17 σ_M=-818.72 τ=0.00 σ_{max}=-949.89
  Tensioni: σ_N=-131.17 σ_M=-35.12 τ=28.97 τ_{max}=28.97
  Tensioni: σ_N=-131.17 σ_M=-818.72 τ=0.00 $\sigma_{ID,max}$=949.89

Asta n. 6001 (1960 1961) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7400.32 My,Ed=-66.00 Mz,Ed=3619.68
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=700.73
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.01 Curva b: α-imp=0.34 k_c=0.94 ψ=1.23 M,cr=28516.30 λ_{LT}=0.79
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.80 β_{LT}=0.75 f=0.97 χ_{LT}=0.85
  λ_Y=98.01 Ncr,y=183603.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.44
  λ_Z=134.26 Ncr,z=97842.80 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 0.98, 1.01, 0.79, 1.01
  Verifica YY: 0.06 + 0.00 + 0.58 = 0.65
  Verifica ZZ: 0.11 + 0.00 + 0.58 = 0.69

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/88526) $f_{Z,L}$=0.00 (L/293907)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.05 (L/15212) $f_{Z,L}$=0.01 (L/72749)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.01 - Classe 3
  Sollecitazioni: N=-6792.46 T_z=15.07 M_y=-66.00 T_y=884.70 M_z=3619.68 M_x=-3.61
  Tensioni: σ_N=-79.82 σ_M=-1965.22 τ=3.62 σ_{max}=-2045.05

Tensioni: σ_N=-79.82 σ_M=151.19 τ=20.60 τ_{max}=20.60
Tensioni: σ_N=-79.82 σ_M=-1965.22 τ=3.62 $\sigma_{ID,max}$=2045.06

Asta n. 6002 (1954 1955) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-19862.00 My,Ed=-360.74 Mz,Ed=-1766.72
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=702.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=7.02 Curva b: α-imp=0.34 k_c=0.94 ψ=1.55 M,cr=35798.20 λ_{LT}=0.70
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.74 β_{LT}=0.75 f=0.97 χ_{LT}=0.89
λ_Y=98.21 Ncr,y=182868.00 λ^*_y=1.29 Curva b: Φ_y=1.51 χ_y=0.43
λ_Z=134.53 Ncr,z=97451.20 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
Kyy, Kyz, Kzy, Kzz = 1.04, 1.11, 0.83, 1.11
Verifica YY: 0.16 + 0.02 + 0.31 = 0.50
Verifica ZZ: 0.28 + 0.02 + 0.31 = 0.62

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.01 (L/51128) $f_{Z,G}$=0.01 (L/73994)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.08 (L/9067) $f_{Z,G}$=0.06 (L/12553)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.02 - Classe 3
Sollecitazioni: N=-19254.20 T_z=-62.02 M_y=74.71 T_y=-476.67 M_z=-1766.72 M_x=5.21
Tensioni: σ_N=-226.28 σ_M=-967.75 τ=5.22 σ_{max}=-1194.02
Tensioni: σ_N=-226.28 σ_M=-80.64 τ=20.40 τ_{max}=20.40
Tensioni: σ_N=-226.28 σ_M=-967.75 τ=5.22 $\sigma_{ID,max}$=1194.06

Asta n. 6004 (1892 1893) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-5228.71 My,Ed=-4075.46 Mz,Ed=2595.61
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=700.78
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=7.01 Curva b: α-imp=0.34 k_c=0.94 ψ=1.44 M,cr=33466.60 λ_{LT}=0.73
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.75 β_{LT}=0.75 f=0.97 χ_{LT}=0.88
λ_Y=98.02 Ncr,y=183579.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.44
λ_Z=134.27 Ncr,z=97829.90 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
Verifica YY: 0.04 + 0.27 + 0.41 = 0.72
Verifica ZZ: 0.07 + 0.21 + 0.41 = 0.70

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.01 (L/74981) $f_{Z,G}$=0.01 (L/86449)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.05 (L/12868) $f_{Z,G}$=0.05 (L/15011)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.01 - Classe 3
Sollecitazioni: N=-6709.53 T_z=-8.47 M_y=-72.89 T_y=882.55 M_z=3609.32 M_x=-1.15
Tensioni: σ_N=-78.85 σ_M=-1961.02 τ=1.15 σ_{max}=-2039.87
Tensioni: σ_N=-78.85 σ_M=151.89 τ=17.99 τ_{max}=17.99
Tensioni: σ_N=-78.85 σ_M=-1961.02 τ=1.15 $\sigma_{ID,max}$=2039.87

Asta n. 6004 (1956 1957) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-20838.90 My,Ed=-379.43 Mz,Ed=-2090.78
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=702.06
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=7.02 Curva b: α-imp=0.34 k_c=0.94 ψ=1.55 M,cr=35968.50 λ_{LT}=0.70
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.74 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
λ_Y=98.19 Ncr,y=182908.00 λ^*_y=1.29 Curva b: Φ_y=1.51 χ_y=0.43
λ_Z=134.51 Ncr,z=97472.40 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
Kyy, Kyz, Kzy, Kzz = 1.05, 1.12, 0.84, 1.12
Verifica YY: 0.17 + 0.03 + 0.37 = 0.57
Verifica ZZ: 0.30 + 0.02 + 0.37 = 0.69

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.01 (L/48431) $f_{Z,G}$=0.01 (L/70446)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.08 (L/8640) $f_{Z,G}$=0.06 (L/12137)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.02 - Classe 3
  Sollecitazioni: N=-20231.00 T_z=-64.82 M_y=75.66 T_y=-566.74 M_z=-2090.78 M_x=6.01
  Tensioni: σ_N=-237.76 σ_M=-1142.69 τ=6.03 σ_{max}=-1380.45
  Tensioni: σ_N=-237.76 σ_M=-93.38 τ=23.51 τ_{max}=23.51
  Tensioni: σ_N=-237.76 σ_M=-1142.69 τ=6.03 $\sigma_{ID,max}$=1380.49

Asta n. 6005 (-882 -868) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/25040)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.07 (L/4540)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-13337.00
  N,Ed=-13337.00 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.18

- Verifica di stabilità (4.2.4.1.3.1) - CC 25
  Sollecitazioni: N=-13337.00 L=320.00
  λ=79.28 Ncr=70851.00 λ^*=1.04
  Curva a: Φ=1.13 χ,min=0.64 N,Ed=-13337.00 Nb,Rd=46443.40 N,Ed/Nb,Rd=0.29

Asta n. 6006 (-883 -871) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/24314)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.04 (L/4438)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-13804.70
  N,Ed=-13804.70 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.19

- Verifica di stabilità (4.2.4.1.3.1) - CC 25
  Sollecitazioni: N=-13804.70 L=160.00
  λ=39.64 Ncr=283404.00 λ^*=0.52
  Curva a: Φ=0.67 χ,min=0.92 N,Ed=-13804.70 Nb,Rd=66718.00 N,Ed/Nb,Rd=0.21

Asta n. 6007 (1969 2008) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/28136)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.61 - Classe 3
  Sollecitazioni: N=5609.35
  Tensioni: σ_N=261.04 σ_M=0.00 τ=0.00 σ_{max}=261.04
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=261.04 σ_M=0.00 τ=0.00 $\sigma_{ID,max}$=261.04

Asta n. 6008 (1970 2009) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/56273)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/10048)

- Verifica a compressione (4.2.10) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-8421.42
  N,Ed=-8421.42 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.12

Asta n. 6009 (2009 1969) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 23 - Classe 3
  L_{cr}=2.59 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
  $\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
  CC 23 My,Ed=-5.39 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 1 - Classe 3
  Sollecitazioni: N,Ed=-3663.23 M,Ed=4.05
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=259.36
  λ=259.36 Ncr=3872.04 λ^*=3.39 Curva c: Φ=7.04 χ,min=0.08
  χ,min=0.08
  Verifica: 1.14 + 0.35 = 1.49

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.14 (L/1814) $f_{Z,G}$=0.09 (L/2877)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.30 - Classe 3
  Sollecitazioni: N=-5607.05 M=5.39
  Tensioni: σ_N=-446.19 σ_M=-85.86 τ=0.00 σ_{max}=-532.05
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-446.19 σ_M=-85.86 τ=0.00 $\sigma_{ID,max}$=532.05

Asta n. 6010 (2008 1970) Cir. D=4 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 25 - Classe 3
  L_{cr}=2.10 Curva d: α-imp=0.76 k_c=0.94 ψ=1.75 M,cr=0.00 λ_{LT}=0.00
  $\lambda_{LT,0}$=0.00 β_{LT}=0.00 Φ_{LT}=0.00 β_{LT}=0.00 f=0.00 χ_{LT}=1.00
  CC 25 My,Ed=-5.68 My,b,Rd=212.43 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 23 - Classe 3
  Sollecitazioni: N,Ed=-2230.33 M,Ed=3.28
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=209.96
  λ=209.96 Ncr=5908.50 λ^*=2.75 Curva c: Φ=4.90 χ,min=0.11
  χ,min=0.11
  Verifica: 0.47 + 0.02 = 0.49

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.08 (L/2769) $f_{Z,G}$=0.06 (L/3407)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.05 - Classe 3
  Sollecitazioni: N=7755.51 M=4.37
  Tensioni: σ_N=617.16 σ_M=69.51 τ=0.00 σ_{max}=686.67
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=617.16 σ_M=69.51 τ=0.00 $\sigma_{ID,max}$=686.67

Asta n. 6011 (1966 2006) Cir.c D=120/6 Crit. 1

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/31263)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.61 - Classe 3
  Sollecitazioni: N=2348.03
  Tensioni: σ_N=109.27 σ_M=0.00 τ=0.00 σ_{max}=109.27
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=109.27 σ_M=0.00 τ=0.00 $\sigma_{ID,max}$=109.27

Asta n. 6012 (1967 2007) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-4619.93 M,Ed=0.00
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=161.00
  αmy, αmz, αLT = 0.95, ----, ----
  λ=39.89 Ncr=279894.00 λ^*=0.52
  Curva a: Φ=0.67 χ,min=0.92
  Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
  Verifica: 0.06 = 0.06

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/70342)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/13189)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-4619.93
  N,Ed=-4619.93 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.06

Asta n. 6013 (1966 2007) Cir. D=4 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.1) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2816.03 M,Ed=5.26
  Resistenze: Nc,Rd=42486.30 M,c,Rd=212.43 L=259.36
  λ=259.36 Ncr=3872.04 λ^*=3.39 Curva c: Φ=7.04 χ,min=0.08
  χ,min=0.08
  Verifica: 0.88 + 0.09 = 0.97

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/90651)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.14 (L/1815) $f_{Z,G}$=0.10 (L/2565)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.30 - Classe 3
  Sollecitazioni: N=-2803.40 M=7.01
  Tensioni: σ_N=-223.09 σ_M=-111.62 τ=0.00 σ_{max}=-334.70
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-223.09 σ_M=-111.62 τ=0.00 $\sigma_{ID,max}$=334.70

Asta n. 6014 (1967 2006) Cir. D=4 Crit. 1

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/100069)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.08 (L/2769) $f_{Z,G}$=0.05 (L/3822)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.05 - Classe 3
  Sollecitazioni: N=3466.35 M=5.68
  Tensioni: σ_N=275.84 σ_M=90.36 τ=0.00 σ_{max}=366.20
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=275.84 σ_M=90.36 τ=0.00 $\sigma_{ID,max}$=366.20

Asta n. 6015 (1961 1957) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2571.54 M,Ed=2.86
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=102.22
  αmy, αmz, αLT = 0.95, ----, ----
  λ=25.33 Ncr=694405.00 λ^*=0.33
  Curva a: Φ=0.57 χ,min=0.97
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.51 - Classe 3
  Sollecitazioni: N=-2571.54 M=2.86
  Tensioni: σ_N=-119.67 σ_M=-4.91 τ=0.00 σ_{max}=-124.58
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-119.67 σ_M=-4.91 τ=0.00 $\sigma_{ID,max}$=124.58

Asta n. 6016 (1957 1959) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2916.06 M,Ed=4.01
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=120.97
  αmy, αmz, αLT = 0.95, ----, ----
  λ=29.97 Ncr=495806.00 λ^*=0.39
  Curva a: Φ=0.60 χ,min=0.95
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.60 - Classe 3
  Sollecitazioni: N=-2916.06 M=4.01
  Tensioni: σ_N=-135.70 σ_M=-6.88 τ=0.00 σ_{max}=-142.58
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-135.70 σ_M=-6.88 τ=0.00 $\sigma_{ID,max}$=142.58

Asta n. 6017 (1959 1955) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2482.13 M,Ed=2.89
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=102.73
  αmy, αmz, αLT = 0.95, ----, ----
  λ=25.45 Ncr=687497.00 λ^*=0.33
  Curva a: Φ=0.57 χ,min=0.97
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.03 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.51 - Classe 3
  Sollecitazioni: N=-2482.13 M=2.89
  Tensioni: σ_N=-115.51 σ_M=-4.96 τ=0.00 σ_{max}=-120.47
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-115.51 σ_M=-4.96 τ=0.00 $\sigma_{ID,max}$=120.47

Asta n. 6018 (1955 1961) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-2879.60 M,Ed=3.97
  Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=120.28
  αmy, αmz, αLT = 0.95, ----, ----
  λ=29.80 Ncr=501459.00 λ^*=0.39
  Curva a: Φ=0.60 χ,min=0.96
  Kyy, Kyz, Kzy, Kzz = 0.96, ----, ----, ----
  Verifica: 0.04 + 0.00 = 0.04

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.60 - Classe 3
  Sollecitazioni: N=-2879.60 M=3.97
  Tensioni: σ_N=-134.01 σ_M=-6.80 τ=0.00 σ_{max}=-140.80
  Tensioni: σ_N=0.00 σ_M=0.00 τ=0.00 τ_{max}=0.00
  Tensioni: σ_N=-134.01 σ_M=-6.80 τ=0.00 $\sigma_{ID,max}$=140.80

Asta n. 6101 (1961 1968) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7141.58 My,Ed=418.99 Mz,Ed=-4953.12
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=526.58
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.27 Curva b: α-imp=0.34 k_c=0.94 ψ=1.59 M,cr=52117.30 λ_{LT}=0.58
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
  λ_Y=73.65 Ncr,y=325125.00 λ^*_y=0.96 Curva b: Φ_y=1.09 χ_y=0.62
  λ_Z=100.89 Ncr,z=173260.00 λ^*_z=1.32 Curva c: Φ_z=1.65 χ_z=0.38
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
  Verifica YY: 0.04 + 0.03 + 0.78 = 0.85
  Verifica ZZ: 0.07 + 0.02 + 0.78 = 0.87

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.01 (L/38884) $f_{Z,L}$=0.01 (L/55773)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.09 (L/6008) $f_{Z,L}$=0.05 (L/9807)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=5.27 - Classe 3
  Sollecitazioni: N=-6690.03 T_z=-92.10 M_y=418.99 T_y=-1664.04 M_z=-4953.12 M_x=3.82
  Tensioni: σ_N=-78.62 σ_M=-2755.30 τ=3.83 σ_{max}=-2833.92
  Tensioni: σ_N=-78.62 σ_M=-259.88 τ=35.71 τ_{max}=35.71
  Tensioni: σ_N=-78.62 σ_M=-2755.30 τ=3.83 $\sigma_{ID,max}$=2833.93

Asta n. 6102 (1955 1971) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-20120.40 My,Ed=-209.42 Mz,Ed=-1767.57
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=553.99
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.54 Curva b: α-imp=0.34 k_c=0.94 ψ=1.51 M,cr=46544.50 λ_{LT}=0.62
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.68 β_{LT}=0.75 f=0.97 χ_{LT}=0.94
  λ_Y=77.48 Ncr,y=293755.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
  λ_Z=106.14 Ncr,z=156543.00 λ^*_z=1.39 Curva c: Φ_z=1.76 χ_z=0.35
  Kyy, Kyz, Kzy, Kzz = 1.02, 1.06, 0.81, 1.06
  Verifica YY: 0.12 + 0.01 + 0.30 = 0.43
  Verifica ZZ: 0.20 + 0.01 + 0.30 = 0.51

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.02 (L/35857) $f_{Z,L}$=0.00 (L/145223)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.09 (L/6273) $f_{Z,L}$=0.03 (L/21675)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=5.54 - Classe 3
  Sollecitazioni: N=-19668.80 T_z=46.92 M_y=-209.42 T_y=552.98 M_z=1755.39 M_x=-6.82
  Tensioni: σ_N=-231.15 σ_M=-988.74 τ=6.83 σ_{max}=-1219.89
  Tensioni: σ_N=-231.15 σ_M=101.93 τ=25.16 τ_{max}=25.16
  Tensioni: σ_N=-231.15 σ_M=-988.74 τ=6.83 $\sigma_{ID,max}$=1219.94

Asta n. 6103 (1959 1965) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-6878.02 My,Ed=195.29 Mz,Ed=-5332.61
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=526.43
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=5.26 Curva b: α-imp=0.34 k_c=0.94 ψ=1.09 M,cr=35749.80 λ_{LT}=0.70

$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.74 β_{LT}=0.75 f=0.97 χ_{LT}=0.89
λ_Y=73.63 Ncr,y=325318.00 λ^*_y=0.96 Curva b: Φ_y=1.09 χ_y=0.62
λ_Z=100.86 Ncr,z=173363.00 λ^*_z=1.32 Curva c: Φ_z=1.65 χ_z=0.38
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
Verifica YY: 0.02 + 0.01 + 0.84 = 0.88
Verifica ZZ: 0.02 + 0.01 + 0.84 = 0.87

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/39428) $f_{Z,L}$=0.00 (L/250907)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.09 (L/6072) $f_{Z,L}$=0.02 (L/33454)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=5.26 - Classe 3
Sollecitazioni: N=-6530.68 T_z=-43.84 M_y=195.29 T_y=-1607.26 M_z=-5332.61 M_x=10.42
Tensioni: σ_N=-76.75 σ_M=-2914.94 τ=10.44 σ_{max}=-2991.69
Tensioni: σ_N=-76.75 σ_M=-238.54 τ=45.82 τ_{max}=45.82
Tensioni: σ_N=-76.75 σ_M=-2914.94 τ=10.44 $\sigma_{ID,max}$=2991.74

Asta n. 6104 (1957 1962) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-21113.50 My,Ed=-210.99 Mz,Ed=-2091.51
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=553.99
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=5.54 Curva b: α-imp=0.34 k_c=0.94 ψ=1.50 M,cr=46181.10 λ_{LT}=0.62
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.68 β_{LT}=0.75 f=0.97 χ_{LT}=0.94
λ_Y=77.48 Ncr,y=293755.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
λ_Z=106.14 Ncr,z=156543.00 λ^*_z=1.39 Curva c: Φ_z=1.76 χ_z=0.35
Kyy, Kyz, Kzy, Kzz = 1.02, 1.07, 0.82, 1.07
Verifica YY: 0.12 + 0.01 + 0.36 = 0.49
Verifica ZZ: 0.21 + 0.01 + 0.36 = 0.58

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.02 (L/33005) $f_{Z,L}$=0.00 (L/111710)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.09 (L/5891) $f_{Z,L}$=0.02 (L/22342)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-21113.50 T_z=47.77 M_y=53.64 T_y=827.97 M_z=-2091.51 M_x=-7.13
Tensioni: σ_N=-248.13 σ_M=-1138.66 τ=7.14 σ_{max}=-1386.78
Tensioni: σ_N=-248.13 σ_M=-89.86 τ=28.60 τ_{max}=28.60
Tensioni: σ_N=-248.13 σ_M=-1138.66 τ=7.14 $\sigma_{ID,max}$=1386.84

Asta n. 6105 (-868 2010) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-11725.60 M,Ed=0.12
Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=78.22
αmy, αmz, αLT = 0.95, ----, ----
λ=19.38 Ncr=1185880.00 λ^*=0.25
Curva a: Φ=0.54 χ,min=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
Verifica: 0.16 + 0.00 = 0.16

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/27338)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/5126)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-11725.60
N,Ed=-11725.60 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.16

Asta n. 6106 (-871 2011) Cir.c D=120/6 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-10868.10 M,Ed=0.29
Resistenze: Nc,Rd=72651.60 M,c,Rd=1972.49 L=66.17
αmy, αmz, αLT = 0.95, ----, ----
λ=16.39 Ncr=1657040.00 λ^*=0.21
Curva a: Φ=0.52 χ,min=1.00
Kyy, Kyz, Kzy, Kzz = 0.97, ----, ----, ----
Verifica: 0.15 + 0.00 = 0.15

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.00 (L/31537)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.01 (L/6086)

- Verifica a compressione (4.2.10) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-10868.10 T=1.76
  N,Ed=-10868.10 Nc,Rd=-72651.60 N,Ed/Nc,Rd=0.15

Asta n. 6211 (1968 1970) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3314.22 My,Ed=1285.98 Mz,Ed=-2018.23
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=379.60
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=3.80 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=39930.60 λ_{LT}=0.51
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.62 β_{LT}=0.75 f=0.98 χ_{LT}=0.98
  λ_y=62.61 Ncr,y=307021.00 λ^*_y=0.82 Curva b: Φ_y=0.94 χ_y=0.71
  λ_z=83.04 Ncr,z=174529.00 λ^*_z=1.09 Curva c: Φ_z=1.31 χ_z=0.49
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
  Verifica YY: 0.02 + 0.13 + 0.51 = 0.66
  Verifica ZZ: 0.02 + 0.10 + 0.51 = 0.63

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.06 (L/6546) $f_{Z,L}$=0.04 (L/10586)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.32 (L/1172) $f_{Z,L}$=0.20 (L/1906)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3314.22 T_z=338.78 M_y=1285.98 T_y=601.35 M_z=-2018.23
  Tensioni: σ_N=-57.08 σ_M=-2227.89 τ=0.00 σ_{max}=-2284.97
  Tensioni: σ_N=-57.08 σ_M=-459.21 τ=23.76 τ_{max}=23.76
  Tensioni: σ_N=-57.08 σ_M=-2227.89 τ=0.00 $\sigma_{ID,max}$=2284.97

Asta n. 6212 (1968 1969) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-3643.71 My,Ed=-1171.15 Mz,Ed=-2554.41
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=334.12
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=3.34 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=47739.80 λ_{LT}=0.47
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.59 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_y=55.11 Ncr,y=396295.00 λ^*_y=0.72 Curva b: Φ_y=0.85 χ_y=0.77
  λ_z=73.09 Ncr,z=225278.00 λ^*_z=0.96 Curva c: Φ_z=1.14 χ_z=0.57
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
  Verifica YY: 0.02 + 0.11 + 0.65 = 0.78
  Verifica ZZ: 0.02 + 0.09 + 0.65 = 0.76

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.06 (L/5771) $f_{Z,L}$=0.03 (L/13321)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.33 (L/1025) $f_{Z,L}$=0.14 (L/2381)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3643.71 T_z=-350.52 M_y=-1171.15 T_y=825.96 M_z=-2554.41
  Tensioni: σ_N=-62.75 σ_M=-2663.66 τ=0.00 σ_{max}=-2726.41
  Tensioni: σ_N=-62.75 σ_M=182.91 τ=28.45 τ_{max}=28.45
  Tensioni: σ_N=-62.75 σ_M=-2663.66 τ=0.00 $\sigma_{ID,max}$=2726.41

Asta n. 6212 (1971 1973) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-11554.50 My,Ed=580.15 Mz,Ed=224.29
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=437.01
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=4.37 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=33075.30 λ_{LT}=0.56
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
  λ_y=72.08 Ncr,y=231653.00 λ^*_y=0.94 Curva b: Φ_y=1.07 χ_y=0.63
  λ_z=95.60 Ncr,z=131685.00 λ^*_z=1.25 Curva c: Φ_z=1.54 χ_z=0.41
  Kyy, Kyz, Kzy, Kzz = 1.00, 1.03, 0.80, 1.03
  Verifica YY: 0.09 + 0.06 + 0.06 = 0.21
  Verifica ZZ: 0.14 + 0.05 + 0.06 = 0.25

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.02 (L/22684) $f_{Z,G}$=0.01 (L/35521)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.12 (L/3648) $f_{Z,G}$=0.08 (L/5520)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-11554.50 T_z=132.76 M_y=580.15 T_y=20.45 M_z=217.81
  Tensioni: σ_N=-198.99 σ_M=-391.39 τ=0.00 σ_{max}=-590.37
  Tensioni: σ_N=-198.99 σ_M=11.67 τ=7.99 τ_{max}=7.99
  Tensioni: σ_N=-198.99 σ_M=-391.39 τ=0.00 $\sigma_{ID,max}$=590.37

Asta n. 6213 (1965 1966) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-3174.24 My,Ed=1139.18 Mz,Ed=-2177.86
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=352.04
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=3.52 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=44330.50 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=58.06 Ncr,y=356964.00 λ^*_y=0.76 Curva b: Φ_y=0.88 χ_y=0.75
  λ_Z=77.01 Ncr,z=202920.00 λ^*_z=1.01 Curva c: Φ_z=1.21 χ_z=0.54
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
  Verifica YY: 0.02 + 0.11 + 0.55 = 0.68
  Verifica ZZ: 0.02 + 0.09 + 0.55 = 0.66

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,G}$=0.06 (L/6320) $f_{Z,L}$=0.03 (L/13877)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.31 (L/1129) $f_{Z,L}$=0.14 (L/2484)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-3174.24 T_z=323.59 M_y=1139.18 T_y=672.23 M_z=-2177.86
  Tensioni: σ_N=-54.67 σ_M=-2319.11 τ=0.00 σ_{max}=-2373.78
  Tensioni: σ_N=-54.67 σ_M=-427.69 τ=24.49 τ_{max}=24.49
  Tensioni: σ_N=-54.67 σ_M=-2319.11 τ=0.00 $\sigma_{ID,max}$=2373.78

Asta n. 6214 (1962 1964) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-8425.83 My,Ed=-829.06 Mz,Ed=-354.68
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=448.31
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=4.48 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=31994.10 λ_{LT}=0.57
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.65 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
  λ_Y=73.94 Ncr,y=220115.00 λ^*_y=0.97 Curva b: Φ_y=1.10 χ_y=0.62
  λ_Z=98.07 Ncr,z=125127.00 λ^*_z=1.28 Curva c: Φ_z=1.59 χ_z=0.40
  Kyy, Kyz, Kzy, Kzz = 0.99, 1.01, 0.79, 1.01
  Verifica YY: 0.07 + 0.09 + 0.09 = 0.25
  Verifica ZZ: 0.11 + 0.07 + 0.09 = 0.27

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.04 (L/12548) $f_{Z,G}$=0.00 (L/95936)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.21 (L/2098) $f_{Z,G}$=0.02 (L/22174)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
  Sollecitazioni: N=-8425.83 T_z=-184.93 M_y=-829.06 T_y=141.81 M_z=-354.68
  Tensioni: σ_N=-145.10 σ_M=-597.78 τ=0.00 σ_{max}=-742.88
  Tensioni: σ_N=-145.10 σ_M=-19.00 τ=11.15 τ_{max}=11.15
  Tensioni: σ_N=-145.10 σ_M=-597.78 τ=0.00 $\sigma_{ID,max}$=742.88

Asta n. 6222 (1971 1972) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-9534.94 My,Ed=-653.02 Mz,Ed=-184.00
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=458.65
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=4.59 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=31066.50 λ_{LT}=0.58
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
  λ_Y=75.65 Ncr,y=210307.00 λ^*_y=0.99 Curva b: Φ_y=1.12 χ_y=0.60
  λ_Z=100.33 Ncr,z=119551.00 λ^*_z=1.31 Curva c: Φ_z=1.63 χ_z=0.38

Kyy, Kyz, Kzy, Kzz = 1.00, 1.02, 0.80, 1.02
Verifica YY: 0.08 + 0.07 + 0.05 = 0.20
Verifica ZZ: 0.13 + 0.06 + 0.05 = 0.23

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.02 (L/18640) $f_{Z,G}$=0.00 (L/123314)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.15 (L/3080) $f_{Z,G}$=0.02 (L/21860)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-7975.47 T_z=-130.73 M_y=-599.59 T_y=115.65 M_z=-242.86
Tensioni: σ_N=-137.35 σ_M=-420.23 τ=0.00 σ_{max}=-557.58
Tensioni: σ_N=-137.35 σ_M=-13.01 τ=7.89 τ_{max}=7.89
Tensioni: σ_N=-137.35 σ_M=-420.23 τ=0.00 $\sigma_{ID,max}$=557.58

Asta n. 6223 (1965 1967) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-3599.23 My,Ed=-1279.87 Mz,Ed=-2811.08
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=363.03
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=3.63 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=42465.80 λ_{LT}=0.49
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.61 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=59.88 Ncr,y=335675.00 λ^*_y=0.78 Curva b: Φ_y=0.91 χ_y=0.73
λ_Z=79.42 Ncr,z=190818.00 λ^*_z=1.04 Curva c: Φ_z=1.25 χ_z=0.52
Kyy, Kyz, Kzy, Kzz = 0.96, 0.97, 0.77, 0.97
Verifica YY: 0.02 + 0.13 + 0.71 = 0.86
Verifica ZZ: 0.02 + 0.10 + 0.71 = 0.83

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.06 (L/5758) $f_{Z,L}$=0.03 (L/11933)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.36 (L/1022) $f_{Z,L}$=0.17 (L/2115)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-3599.23 T_z=-352.55 M_y=-1279.87 T_y=821.58 M_z=-2811.08
Tensioni: σ_N=-61.98 σ_M=-2928.23 τ=0.00 σ_{max}=-2990.22
Tensioni: σ_N=-61.98 σ_M=198.84 τ=28.43 τ_{max}=28.43
Tensioni: σ_N=-61.98 σ_M=-2928.23 τ=0.00 $\sigma_{ID,max}$=2990.22

Asta n. 6224 (1962 1963) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-10131.20 My,Ed=552.58 Mz,Ed=447.87
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=426.15
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=4.26 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=34185.30 λ_{LT}=0.55
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_Y=70.29 Ncr,y=243609.00 λ^*_y=0.92 Curva b: Φ_y=1.05 χ_y=0.65
λ_Z=93.22 Ncr,z=138482.00 λ^*_z=1.22 Curva c: Φ_z=1.49 χ_z=0.42
Kyy, Kyz, Kzy, Kzz = 0.99, 1.02, 0.79, 1.02
Verifica YY: 0.08 + 0.06 + 0.12 = 0.26
Verifica ZZ: 0.12 + 0.05 + 0.12 = 0.29

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.02 (L/23033) $f_{Z,G}$=0.02 (L/27754)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.12 (L/3580) $f_{Z,G}$=0.10 (L/4346)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=0.00 - Classe 3
Sollecitazioni: N=-10131.20 T_z=129.67 M_y=552.58 T_y=67.03 M_z=447.87
Tensioni: σ_N=-174.47 σ_M=-585.78 τ=0.00 σ_{max}=-760.25
Tensioni: σ_N=-174.47 σ_M=23.99 τ=7.81 τ_{max}=7.81
Tensioni: σ_N=-174.47 σ_M=-585.78 τ=0.00 $\sigma_{ID,max}$=760.25

Asta n. 6232 (-868 1974) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-4609.86 My,Ed=-90.26 Mz,Ed=-744.32
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=248865.00 λ_{LT}=0.20
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00

λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.01 + 0.19 = 0.22
Verifica ZZ: 0.02 + 0.01 + 0.19 = 0.22

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/40490)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/6577) $f_{Z,L}$=0.00 (L/64784)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-4609.86 T_z=-73.04 M_y=-90.26 T_y=635.58 M_z=-744.32
Tensioni: σ_N=-79.39 σ_M=-690.31 τ=0.00 σ_{max}=-769.70
Tensioni: σ_N=-79.39 σ_M=-15.23 τ=17.19 τ_{max}=17.19
Tensioni: σ_N=-79.39 σ_M=-690.31 τ=0.00 $\sigma_{ID,max}$=769.70

Asta n. 6232 (-867 -868) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3191.27 My,Ed=-90.26 Mz,Ed=-744.32
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.13 M,cr=160375.00 λ_{LT}=0.25
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.02 + 0.01 + 0.19 = 0.21
Verifica ZZ: 0.02 + 0.01 + 0.19 = 0.21

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/28792)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/5041) $f_{Z,L}$=0.00 (L/53986)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.24 - Classe 3
Sollecitazioni: N=-3160.45 T_z=17.83 M_y=-90.26 T_y=-426.85 M_z=-744.32
Tensioni: σ_N=-54.43 σ_M=-690.31 τ=0.00 σ_{max}=-744.74
Tensioni: σ_N=-54.43 σ_M=-15.23 τ=11.29 τ_{max}=11.29
Tensioni: σ_N=-54.43 σ_M=-690.31 τ=0.00 $\sigma_{ID,max}$=744.74

Asta n. 6232 (-866 -867) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
Sollecitazioni: N,Ed=-2811.48 My,Ed=-174.69 Mz,Ed=-232.31
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.10 M,cr=155869.00 λ_{LT}=0.26
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01 + 0.02 + 0.06 = 0.09
Verifica ZZ: 0.01 + 0.01 + 0.06 = 0.09

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/107973)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.00 (L/47988) $f_{Z,L}$=0.00 (L/64784)

- Verifica in termini tensionali (4.2.5) - CC 9 Xl=1.24 - Classe 3
Sollecitazioni: N=-2787.78 T_z=33.58 M_y=-174.69 T_y=-292.86 M_z=-232.31
Tensioni: σ_N=-48.01 σ_M=-265.56 τ=0.00 σ_{max}=-313.57
Tensioni: σ_N=-48.01 σ_M=35.25 τ=7.92 τ_{max}=7.92
Tensioni: σ_N=-48.01 σ_M=-265.56 τ=0.00 $\sigma_{ID,max}$=313.57

Asta n. 6232 (-865 -866) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3252.90 My,Ed=-46.19 Mz,Ed=468.66
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95

L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.28 M,cr=182448.00 λ_{LT}=0.24
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.02 + 0.00 + 0.12 = 0.14
Verifica ZZ: 0.02 + 0.00 + 0.12 = 0.14

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/47988)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/7279)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3252.90 T_z=17.83 M_y=-24.15 T_y=-227.58 M_z=468.66
Tensioni: σ_N=-56.02 σ_M=-423.48 τ=0.00 σ_{max}=-479.50
Tensioni: σ_N=-56.02 σ_M=31.70 τ=6.07 τ_{max}=6.07
Tensioni: σ_N=-56.02 σ_M=-423.48 τ=0.00 $\sigma_{ID,max}$=479.50

Asta n. 6232 (1971 -865) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3283.71 My,Ed=-24.15 Mz,Ed=708.84
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=123.57
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.24 Curva b: α-imp=0.34 k_c=0.94 ψ=1.66 M,cr=236094.00 λ_{LT}=0.21
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=20.38 Ncr,y=2897440.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=27.03 Ncr,z=1647080.00 λ^*_z=0.35 Curva c: Φ_z=0.60 χ_z=0.92
Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
Verifica YY: 0.02 + 0.00 + 0.18 = 0.20
Verifica ZZ: 0.02 + 0.00 + 0.18 = 0.20

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/21594)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.03 (L/3999)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3283.71 T_z=17.83 M_y=-2.12 T_y=-161.16 M_z=708.84
Tensioni: σ_N=-56.55 σ_M=-628.73 τ=0.00 σ_{max}=-685.28
Tensioni: σ_N=-56.55 σ_M=38.55 τ=4.35 τ_{max}=4.35
Tensioni: σ_N=-56.55 σ_M=-628.73 τ=0.00 $\sigma_{ID,max}$=685.28

Asta n. 6234 (1962 -864) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3928.44 My,Ed=239.74 Mz,Ed=674.37
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.74 M,cr=184412.00 λ_{LT}=0.24
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.02 + 0.17 = 0.21
Verifica ZZ: 0.02 + 0.02 + 0.17 = 0.21

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.01 (L/21435) $f_{Z,L}$=0.00 (L/126824)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.04 (L/4026) $f_{Z,L}$=0.01 (L/25364)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3928.44 T_z=163.48 M_y=239.74 T_y=-101.23 M_z=674.37
Tensioni: σ_N=-67.65 σ_M=-679.46 τ=0.00 σ_{max}=-747.12
Tensioni: σ_N=-67.65 σ_M=36.13 τ=9.85 τ_{max}=9.85
Tensioni: σ_N=-67.65 σ_M=-679.46 τ=0.00 $\sigma_{ID,max}$=747.12

Asta n. 6234 (-864 -869) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3

Sollecitazioni: N,Ed=-3873.80 My,Ed=-234.81 Mz,Ed=479.24
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.74 M,cr=184388.00 λ_{LT}=0.24
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.02 + 0.12 = 0.16
Verifica ZZ: 0.02 + 0.02 + 0.12 = 0.16

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,G}$=0.00 (L/49093)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,G}$=0.02 (L/6734) $f_{Z,L}$=0.00 (L/29267)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
Sollecitazioni: N=-3873.80 T_z=163.48 M_y=2.47 T_y=-167.65 M_z=479.24
Tensioni: σ_N=-66.71 σ_M=-425.44 τ=0.00 σ_{max}=-492.15
Tensioni: σ_N=-66.71 σ_M=25.67 τ=9.88 τ_{max}=9.88
Tensioni: σ_N=-66.71 σ_M=-425.44 τ=0.00 $\sigma_{ID,max}$=492.15

Asta n. 6234 (-869 -870) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3819.17 My,Ed=-472.08 Mz,Ed=-200.23
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.30 M,cr=138049.00 λ_{LT}=0.27
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.05 + 0.05 = 0.12
Verifica ZZ: 0.02 + 0.04 + 0.05 = 0.11

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.00 (L/47559)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.02 (L/9511) $f_{Z,G}$=0.00 (L/60875)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.45 - Classe 3
Sollecitazioni: N=-3764.53 T_z=163.48 M_y=-472.08 T_y=-300.50 M_z=-200.23
Tensioni: σ_N=-64.83 σ_M=-338.85 τ=0.00 σ_{max}=-403.68
Tensioni: σ_N=-64.83 σ_M=118.16 τ=11.65 τ_{max}=11.65
Tensioni: σ_N=-64.83 σ_M=-338.85 τ=0.00 $\sigma_{ID,max}$=403.68

Asta n. 6234 (-870 -871) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-3764.53 My,Ed=-709.35 Mz,Ed=-684.57
Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.18 M,cr=125550.00 λ_{LT}=0.29
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
λ_Z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02 + 0.07 + 0.17 = 0.26
Verifica ZZ: 0.02 + 0.05 + 0.17 = 0.25

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.00 (L/29267) $f_{Z,G}$=0.00 (L/33819)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.03 (L/5514) $f_{Z,G}$=0.02 (L/5808)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=1.45 - Classe 3
Sollecitazioni: N=-3709.90 T_z=163.48 M_y=-709.35 T_y=-366.92 M_z=-684.57
Tensioni: σ_N=-63.89 σ_M=-849.11 τ=0.00 σ_{max}=-913.00
Tensioni: σ_N=-63.89 σ_M=156.99 τ=12.90 τ_{max}=12.90
Tensioni: σ_N=-63.89 σ_M=-849.11 τ=0.00 $\sigma_{ID,max}$=913.00

Asta n. 6234 (-871 1975) Is 146x215x13x10x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7725.94 My,Ed=-709.35 Mz,Ed=-684.57
  Resistenze: Nc,Rd=196322.00 My,c,Rd=9885.72 Mz,c,Rd=3816.13 L=145.14
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.45 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=185554.00 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=23.94 Ncr,y=2100110.00 λ^*_y=0.31 Curva b: Φ_y=0.57 χ_y=0.96
  λ_z=31.75 Ncr,z=1193830.00 λ^*_z=0.42 Curva c: Φ_z=0.64 χ_z=0.89
  Kyy, Kyz, Kzy, Kzz = 0.96, 0.96, 0.77, 0.96
  Verifica YY: 0.04 + 0.07 + 0.17 = 0.28
  Verifica ZZ: 0.04 + 0.05 + 0.17 = 0.27

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.00 (L/42274) $f_{Z,G}$=0.00 (L/47559)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,G}$=0.02 (L/7534) $f_{Z,L}$=0.02 (L/8454)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=0.00 - Classe 3
  Sollecitazioni: N=-7725.94 T_z=-488.74 M_y=-709.35 T_y=504.88 M_z=-684.57
  Tensioni: σ_N=-133.05 σ_M=-849.11 τ=0.00 σ_{max}=-982.16
  Tensioni: σ_N=-133.05 σ_M=-36.67 τ=29.54 τ_{max}=29.54
  Tensioni: σ_N=-133.05 σ_M=-849.11 τ=0.00 $\sigma_{ID,max}$=982.16

Asta n. 7004 (1914 1915) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 - Classe 3
  Sollecitazioni: N,Ed=-5146.79 My,Ed=-3638.56 Mz,Ed=2623.42
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=700.78
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.01 Curva b: α-imp=0.34 k_c=0.94 ψ=1.44 M,cr=33525.40 λ_{LT}=0.73
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.75 β_{LT}=0.75 f=0.97 χ_{LT}=0.88
  λ_y=98.02 Ncr,y=183579.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.44
  λ_z=134.27 Ncr,z=97829.90 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.78, 0.99
  Verifica YY: 0.04 + 0.24 + 0.41 = 0.69
  Verifica ZZ: 0.07 + 0.19 + 0.41 = 0.68

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.01 (L/69322) $f_{Z,G}$=0.01 (L/86449)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.06 (L/12006) $f_{Z,G}$=0.05 (L/14965)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.01 - Classe 3
  Sollecitazioni: N=-6721.86 T_z=-10.15 M_y=-71.73 T_y=883.71 M_z=3614.56 M_x=-1.06
  Tensioni: σ_N=-79.00 σ_M=-1963.61 τ=1.06 σ_{max}=-2042.61
  Tensioni: σ_N=-79.00 σ_M=151.91 τ=17.93 τ_{max}=17.93
  Tensioni: σ_N=-79.00 σ_M=-1963.61 τ=1.06 $\sigma_{ID,max}$=2042.61

Asta n. 8004 (1936 1937) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
  Sollecitazioni: N,Ed=-7308.83 My,Ed=-158.44 Mz,Ed=3600.56
  Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=700.78
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=7.01 Curva b: α-imp=0.34 k_c=0.94 ψ=1.34 M,cr=31074.10 λ_{LT}=0.75
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.77 β_{LT}=0.75 f=0.97 χ_{LT}=0.87
  λ_y=98.02 Ncr,y=183579.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.44
  λ_z=134.27 Ncr,z=97829.90 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
  Kyy, Kyz, Kzy, Kzz = 0.98, 1.01, 0.79, 1.01
  Verifica YY: 0.06 + 0.01 + 0.58 = 0.65
  Verifica ZZ: 0.10 + 0.01 + 0.58 = 0.69

- Verifica Freccia massima per soli carichi accidentali - CC 26
  $f_{Z,L}$=0.01 (L/65608) $f_{Z,G}$=0.01 (L/88002)

- Verifica Freccia massima carichi totali - CC 26
  $f_{Z,L}$=0.06 (L/11270) $f_{Z,G}$=0.05 (L/15073)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.01 - Classe 3
  Sollecitazioni: N=-6700.98 T_z=-12.44 M_y=-71.26 T_y=880.32 M_z=3600.56
  Tensioni: σ_N=-78.75 σ_M=-1955.97 τ=0.00 σ_{max}=-2034.72

Tensioni: σ_N=-78.75 σ_M=151.29 τ=16.81 τ_{max}=16.81
Tensioni: σ_N=-78.75 σ_M=-1955.97 τ=0.00 $\sigma_{ID,max}$=2034.72

Asta n. 9004 (1958 1959) Is 175x250x18x12x0x0x10000 Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 - Classe 3
Sollecitazioni: N,Ed=-7417.40 My,Ed=-251.08 Mz,Ed=3675.92
Resistenze: Nc,Rd=287692.00 My,c,Rd=16807.20 Mz,c,Rd=6269.63 L=700.78
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=7.01 Curva b: α-imp=0.34 k_c=0.94 ψ=1.57 M,cr=36565.50 λ_{LT}=0.69
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.73 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
λ_Y=98.02 Ncr,y=183579.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.44
λ_Z=134.27 Ncr,z=97829.90 λ^*_z=1.76 Curva c: Φ_z=2.43 χ_z=0.24
Kyy, Kyz, Kzy, Kzz = 0.98, 1.01, 0.79, 1.01
Verifica YY: 0.06 + 0.02 + 0.59 = 0.67
Verifica ZZ: 0.11 + 0.01 + 0.59 = 0.71

- Verifica Freccia massima per soli carichi accidentali - CC 26
$f_{Z,L}$=0.01 (L/51385) $f_{Z,G}$=0.01 (L/85943)

- Verifica Freccia massima carichi totali - CC 26
$f_{Z,L}$=0.08 (L/8706) $f_{Z,G}$=0.05 (L/14844)

- Verifica in termini tensionali (4.2.5) - CC 25 Xl=7.01 - Classe 3
Sollecitazioni: N=-6809.55 T_z=-29.54 M_y=-44.06 T_y=899.68 M_z=3675.92
Tensioni: σ_N=-80.03 σ_M=-1991.14 τ=0.00 σ_{max}=-2071.16
Tensioni: σ_N=-80.03 σ_M=149.83 τ=17.20 τ_{max}=17.20
Tensioni: σ_N=-80.03 σ_M=-1991.14 τ=0.00 $\sigma_{ID,max}$=2071.16

Sintesi

Tipo di normativa: stati limite D.M. 08
Tipo di calcolo: analisi sismica dinamica

Dati generali della struttura

- Zona sismica: zona 2
- Sito di costruzione: crotone LON. 17.13210 LAT. 39.08140
Contenuto tra ID reticolo: 40794 40793 40572 40571

Pericolosità sismica di base

Simbologia

TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLU S = Stato limite ultimo (azione sismica)
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
SLD = Stato limite di danno
SLV = Stato limite di salvaguardia della vita
SLC = Stato limite di prevenzione del collasso
SLO = Stato limite di operatività
SLU I = Stato limite di resistenza al fuoco
T_R = Periodo di ritorno
Ag = Accelerazione orizzontale massima al sito
FO = Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
FV = Valore massimo del fattore di amplificazione dello spettro in accelerazione verticale
TC* = Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale
S_S = Coefficiente di amplificazione stratigrafica
C_C = Coefficiente funzione della categoria del suolo
S = Coefficiente di amplificazione stratigrafica e topografica
TC = Periodo corrispondente all'inizio del tratto dello spettro a velocità costante
TB = Periodo corrispondente all'inizio del tratto dello spettro ad accelerazione costante
TD = Periodo corrispondente all'inizio del tratto dello spettro a spostamento costante

TCC	T_R	Ag	FO	FV	TC*	S_S	C_C	S	TC	TB	TD
SLD	75	0.0654	2.40	0.83	0.32	1.50	1.53	1.50	0.49	0.16	1.86
SLV	712	0.1793	2.43	1.39	0.38	1.44	1.45	1.44	0.55	0.18	2.32

- Tipo di opera: Opera ordinaria
- Vita nominale V_N: 50.00
- Classe d'uso: Classe III
- Coefficiente d'uso CU: 1.50
- Periodo di riferimento VR: 75.00

Dati di progetto

- Categoria del suolo di fondazione: C
- Tipologia edificio: c.a. a pendolo inverso

Coeff. C_1	0.05
Periodo T_1	0.42285
Coeff. λ SLD	1.00
Coeff. λ SLV	1.00
Rapporto di sovraresistenza (α_u/α_1)	--
Valore di riferimento del fattore di struttura (q_0)	1.50
Fattore riduttivo (K_w)	1.00
Fattore riduttivo regolarità in altezza (KR)	1.00
Fattore di struttura (q)	1.50

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media i<=15°
- Coeff. amplificazione topografica S_T: 1.00
- Quota di riferimento: 0.00 <m>
- Altezza della struttura: 17.23 <m>
- Numero piani edificio: 0
- Coefficiente θ: 0.00
- Edificio regolare in altezza: si
- Edificio regolare in pianta: si
- Classe di duttilità: Classe B
- Fattore di struttura per sisma verticale (qv): 1.50
- Smorzamento spettro: 5.00
- Coefficiente θ: 0.00

Spettro SLD Z.TXT :

0.0000 0.2215
0.0500 0.5313
0.1000 0.5313
0.1500 0.5313
0.2000 0.3985
0.2500 0.3188
0.3000 0.2656
0.3500 0.2277
0.4000 0.1992
0.4500 0.1771
0.5000 0.1594
0.5500 0.1449
0.6000 0.1328
0.6500 0.1226
0.7000 0.1138
0.7500 0.1063
0.8000 0.0996
0.8500 0.0938
0.9000 0.0885
0.9500 0.0839
1.0000 0.0797
1.0500 0.0723
1.1000 0.0659
1.1500 0.0603
1.2000 0.0553
1.2500 0.0510
1.3000 0.0472
1.3500 0.0437
1.4000 0.0407
1.4500 0.0379
1.5000 0.0354
1.5500 0.0332
1.6000 0.0311
1.6500 0.0293
1.7000 0.0276
1.7500 0.0260
1.8000 0.0246
1.8500 0.0233
1.9000 0.0221
1.9500 0.0210
2.0000 0.0199
2.0500 0.0190
2.1000 0.0181
2.1500 0.0172
2.2000 0.0165
2.2500 0.0157
2.3000 0.0151

```
2.3500  0.0144
2.4000  0.0138
2.4500  0.0133
2.5000  0.0128
2.5500  0.0123
2.6000  0.0118
2.6500  0.0113
2.7000  0.0109
2.7500  0.0105
2.8000  0.0102
2.8500  0.0098
2.9000  0.0095
2.9500  0.0092
3.0000  0.0089
3.0500  0.0086
3.1000  0.0083
3.1500  0.0080
3.2000  0.0078
3.2500  0.0075
3.3000  0.0073
3.3500  0.0071
3.4000  0.0069
3.4500  0.0067
3.5000  0.0065
3.5500  0.0063
3.6000  0.0061
3.6500  0.0060
3.7000  0.0058
3.7500  0.0057
3.8000  0.0055
3.8500  0.0054
3.9000  0.0052
3.9500  0.0051
4.0000  0.0050
```

Spettro SLD.TXT :

```
0.0000  0.9624
0.0500  1.3733
0.1000  1.7842
0.1500  2.1952
0.1638  2.3082
0.2000  2.3082
0.2500  2.3082
0.3000  2.3082
0.3500  2.3082
0.4000  2.3082
0.4500  2.3082
0.4913  2.3082
0.5000  2.2679
0.5500  2.0617
0.6000  1.8899
0.6500  1.7446
0.7000  1.6199
0.7500  1.5119
0.8000  1.4174
0.8500  1.3341
0.9000  1.2600
0.9500  1.1936
1.0000  1.1340
1.0500  1.0800
1.1000  1.0309
1.1500  0.9861
1.2000  0.9450
1.2500  0.9072
1.3000  0.8723
1.3500  0.8400
1.4000  0.8100
1.4500  0.7820
1.5000  0.7560
1.5500  0.7316
1.6000  0.7087
1.6500  0.6872
1.7000  0.6670
1.7500  0.6480
1.8000  0.6300
1.8500  0.6130
1.8616  0.6091
1.9000  0.5848
```

1.9500 0.5552
2.0000 0.5278
2.0500 0.5023
2.1000 0.4787
2.1500 0.4567
2.2000 0.4362
2.2500 0.4170
2.3000 0.3991
2.3500 0.3823
2.4000 0.3665
2.4500 0.3517
2.5000 0.3378
2.5500 0.3246
2.6000 0.3123
2.6500 0.3006
2.7000 0.2896
2.7500 0.2791
2.8000 0.2693
2.8500 0.2599
2.9000 0.2510
2.9500 0.2426
3.0000 0.2346
3.0500 0.2269
3.1000 0.2197
3.1500 0.2127
3.2000 0.2062
3.2500 0.1999
3.3000 0.1938
3.3500 0.1881
3.4000 0.1826
3.4500 0.1774
3.5000 0.1723
3.5500 0.1675
3.6000 0.1629
3.6500 0.1585
3.7000 0.1542
3.7500 0.1501
3.8000 0.1462
3.8500 0.1424
3.9000 0.1388
3.9500 0.1353
4.0000 0.1319

Spettro SLV Z.TXT :

0.0000 1.0051
0.0500 1.6271
0.1000 1.6271
0.1500 1.6271
0.2000 1.2203
0.2500 0.9763
0.3000 0.8135
0.3500 0.6973
0.4000 0.6102
0.4500 0.5424
0.5000 0.4881
0.5500 0.4438
0.6000 0.4068
0.6500 0.3755
0.7000 0.3517
0.7500 0.3517
0.8000 0.3517
0.8500 0.3517
0.9000 0.3517
0.9500 0.3517
1.0000 0.3517
1.0500 0.3517
1.1000 0.3517
1.1500 0.3517
1.2000 0.3517
1.2500 0.3517
1.3000 0.3517
1.3500 0.3517
1.4000 0.3517
1.4500 0.3517
1.5000 0.3517
1.5500 0.3517
1.6000 0.3517
1.6500 0.3517

1.7000 0.3517
1.7500 0.3517
1.8000 0.3517
1.8500 0.3517
1.9000 0.3517
1.9500 0.3517
2.0000 0.3517
2.0500 0.3517
2.1000 0.3517
2.1500 0.3517
2.2000 0.3517
2.2500 0.3517
2.3000 0.3517
2.3500 0.3517
2.4000 0.3517
2.4500 0.3517
2.5000 0.3517
2.5500 0.3517
2.6000 0.3517
2.6500 0.3517
2.7000 0.3517
2.7500 0.3517
2.8000 0.3517
2.8500 0.3517
2.9000 0.3517
2.9500 0.3517
3.0000 0.3517
3.0500 0.3517
3.1000 0.3517
3.1500 0.3517
3.2000 0.3517
3.2500 0.3517
3.3000 0.3517
3.3500 0.3517
3.4000 0.3517
3.4500 0.3517
3.5000 0.3517
3.5500 0.3517
3.6000 0.3517
3.6500 0.3517
3.7000 0.3517
3.7500 0.3517
3.8000 0.3517
3.8500 0.3517
3.9000 0.3517
3.9500 0.3517
4.0000 0.3517

Spettro SLV.TXT :

0.0000 2.5303
0.0500 2.9603
0.1000 3.3904
0.1500 3.8205
0.1820 4.0959
0.2000 4.0959
0.2500 4.0959
0.3000 4.0959
0.3500 4.0959
0.4000 4.0959
0.4500 4.0959
0.5000 4.0959
0.5461 4.0959
0.5500 4.0665
0.6000 3.7276
0.6500 3.4409
0.7000 3.1951
0.7500 2.9821
0.8000 2.7957
0.8500 2.6312
0.9000 2.4851
0.9500 2.3543
1.0000 2.2366
1.0500 2.1301
1.1000 2.0332
1.1500 1.9448
1.2000 1.8638
1.2500 1.7892
1.3000 1.7204

1.3500	1.6567
1.4000	1.5975
1.4500	1.5425
1.5000	1.4910
1.5500	1.4429
1.6000	1.3978
1.6500	1.3555
1.7000	1.3156
1.7500	1.2780
1.8000	1.2425
1.8500	1.2090
1.9000	1.1771
1.9500	1.1470
2.0000	1.1183
2.0500	1.0910
2.1000	1.0650
2.1500	1.0403
2.2000	1.0166
2.2500	0.9940
2.3000	0.9724
2.3170	0.9653
2.3500	0.9384
2.4000	0.8997
2.4500	0.8633
2.5000	0.8292
2.5500	0.7970
2.6000	0.7666
2.6500	0.7379
2.7000	0.7109
2.7500	0.6853
2.8000	0.6610
2.8500	0.6380
2.9000	0.6162
2.9500	0.5955
3.0000	0.5758
3.0500	0.5571
3.1000	0.5393
3.1500	0.5223
3.2000	0.5061
3.2500	0.4906
3.3000	0.4759
3.3500	0.4618
3.4000	0.4483
3.4500	0.4354
3.5000	0.4230
3.5500	0.4112
3.6000	0.3999
3.6500	0.3890
3.7000	0.3785
3.7500	0.3685
3.8000	0.3589
3.8500	0.3517
3.9000	0.3517
3.9500	0.3517
4.0000	0.3517

Condizioni di carico elementari

Simbologia

CCE	= Numero della condizione di carico elementare
Comm.	= Commento
Mx	= Moltiplicatore della massa in dir. X
My	= Moltiplicatore della massa in dir. Y
Mz	= Moltiplicatore della massa in dir. Z
Jpx	= Moltiplicatore del momento d'inerzia intorno all'asse X
Jpy	= Moltiplicatore del momento d'inerzia intorno all'asse Y
Jpz	= Moltiplicatore del momento d'inerzia intorno all'asse Z
Tipo CCE	= Tipo di CCE per calcolo agli stati limite
Sicurezza	= Contributo alla sicurezza F = a favore S = a sfavore A = ambigua
Variabilità	= Tipo di variabilità B = di base I = indipendente A = ambigua

CCE	Comm.	Mx	My	Mz	Jpx	Jpy	Jpz	Tipo CCE	Sicurezza	Variabilità

1	permanenti	1.00	1.00	1.00	0.00	0.00	1.00	1	S		--
2	neve	1.00	1.00	0.00	0.00	0.00	1.00	11	S		B

Elenco tipi cce definiti

Simbologia

Tipo CCE = Tipo condizione di carico elementare
Comm. = Commento
Tipo = Tipologia
- G = Permanente
- Q = Variabile
- I = Da ignorare
- A = Azione eccezionale
- P = Precompressione

Durata = Durata del carico
- N = Non definita
- P = Permanente
- L = Lunga
- M = Media
- B = Breve
- I = Istantanea

γ min. = Coeff. $\gamma_{min.}$
γ max = Coeff. γ_{max}
ψ_0 = Coeff. ψ_0
ψ_1 = Coeff. ψ_1
ψ_2 = Coeff. ψ_2
$\psi_{0,s}$ = Coeff. ψ_0 sismico (D.M. 96)

Tipo CCE	Comm.	Tipo	Durata	γ min.	γ max	ψ_0	ψ_1	ψ_2	$\psi_{0,s}$
1	D.M. 08 Permanenti strutturali	G	N	1.00	1.30				
2	D.M. 08 Permanenti non strutturali	G	N	0.00	1.50				
3	D.M. 08 Variabili Categoria A Ambienti ad uso residenziale	Q	N	0.00	1.50	0.70	0.50	0.30	0.00
4	D.M. 08 Variabili Categoria B Uffici	Q	N	0.00	1.50	0.70	0.50	0.30	0.00
5	D.M. 08 Variabili Categoria C Ambienti suscettibili di affollamento	Q	N	0.00	1.50	0.70	0.70	0.60	0.00
6	D.M. 08 Variabili Categoria D Ambienti ad uso commerciale	Q	N	0.00	1.50	0.70	0.70	0.60	0.00
7	D.M. 08 Variabili Categoria E Biblioteche, archivi, magazzini e ambienti ad uso industriale	Q	N	0.00	1.50	1.00	0.90	0.80	0.00
8	D.M. 08 Variabili Categoria F Rimesse e parcheggi (per autoveicoli di peso <= 30 kN)	Q	N	0.00	1.50	0.70	0.70	0.60	0.00
9	D.M. 08 Variabili Categoria G Rimesse e parcheggi (per autoveicoli di peso > 30 kN)	Q	N	0.00	1.50	0.70	0.50	0.30	0.00
10	D.M. 08 Variabili Vento	Q	N	0.00	1.50	0.60	0.20	0.00	0.00
11	D.M. 08 Variabili Neve (a quota <= 1000 m s.l.m.)	Q	N	0.00	1.50	0.50	0.20	0.00	0.00
12	D.M. 08 Variabili Neve (a quota > 1000 m s.l.m.)	Q	N	0.00	1.50	0.70	0.50	0.20	0.00
13	D.M. 08 Variabili Variazioni termiche	Q	N	0.00	1.50	0.60	0.50	0.00	0.00
14	D.M. 96 Permanenti	G	N	1.00	1.40				
15	D.M. 96 Variabili Abitazioni	Q	P	0.00	1.50	0.70	0.50	0.20	0.70
16	D.M. 96 Variabili Uffici, negozi, scuole, ecc.	Q	N	0.00	1.50	0.70	0.60	0.30	0.70
17	D.M. 96 Variabili Autorimesse	Q	N	0.00	1.50	0.70	0.70	0.60	0.70
18	D.M. 96 Variabili Vento	Q	N	0.00	1.50	0.70	0.20	0.00	0.00

Elenco masse nodi

Simbologia

Nodo = Numero del nodo
Mo = Massa orizzontale
Mz = Massa in dir. Z

Nodo	Mo <kg>	Mz <kg>	Nodo	Mo <kg>	Mz <kg>	Nodo	Mo <kg>	Mz <kg>	Nodo	Mo <kg>	Mz <kg>	Nodo	Mo <kg>	Mz <kg>
-1421	61.69	61.69	-1420	61.69	61.69	-1419	61.69	61.69	-1418	61.69	61.69	-1417	61.69	61.69
-1416	61.69	61.69	-1415	89.58	89.58	-1414	89.58	89.58	-1413	89.58	89.58	-1412	89.58	89.58
-1411	89.58	89.58	-1410	89.58	89.58	-1409	145.82	145.82	-1408	145.82	145.82	-1407	145.82	145.82
-1406	145.82	145.82	-1405	145.82	145.82	-1404	145.82	145.82	-1403	234.55	234.55	-1402	234.55	234.55
-1401	234.55	234.55	-1400	234.55	234.55	-1399	234.55	234.55	-1398	234.55	234.55	-1397	6.60	6.60
-1396	6.60	6.60	-1395	6.60	6.60	-1394	6.60	6.60	-1393	6.60	6.60	-1392	6.60	6.60
-1391	59.32	59.32	-1390	164.87	164.87	-1389	59.32	59.32	-1388	164.87	164.87	-1387	59.32	59.32
-1386	164.87	164.87	-1385	59.32	59.32	-1384	164.87	164.87	-1383	59.32	59.32	-1382	164.87	164.87
-1381	59.32	59.32	-1380	164.87	164.87	-1379	106.40	106.40	-1378	212.79	212.79	-1377	106.40	106.40
-1376	212.79	212.79	-1375	106.40	106.40	-1374	212.79	212.79	-1373	106.40	106.40	-1372	212.79	212.79
-1371	106.40	106.40	-1370	212.79	212.79	-1369	106.40	106.40	-1368	212.79	212.79	-1367	263.16	263.16
-1366	263.16	263.16	-1365	263.16	263.16	-1364	263.16	263.16	-1363	263.16	263.16	-1362	263.16	263.16
-1361	144.74	144.74	-1360	274.72	274.72	-1359	289.48	289.48	-1358	274.72	274.72	-1357	289.48	289.48
-1356	274.72	274.72	-1355	289.48	289.48	-1354	274.72	274.72	-1353	289.48	289.48	-1352	274.72	274.72
-1351	289.48	289.48	-1350	274.72	274.72	-1349	289.48	289.48	-1348	9.33	9.33	-1347	9.33	9.33
-1346	9.33	9.33	-1345	9.33	9.33	-1344	9.33	9.33	-1343	9.33	9.33	-1342	7.33	7.33
-1341	7.33	7.33	-1340	7.33	7.33	-1339	7.33	7.33	-1338	7.33	7.33	-1337	7.33	7.33
-1336	14.65	14.65	-1335	16.65	16.65	-1334	14.65	14.65	-1333	16.65	16.65	-1332	14.65	14.65
-1331	16.65	16.65	-1330	14.65	14.65	-1329	16.65	16.65	-1328	14.65	14.65	-1327	16.65	16.65
-1326	14.65	14.65	-1325	16.65	16.65	-1324	126.40	126.40	-1323	296.94	296.94	-1322	296.94	296.94
-1321	296.94	296.94	-1320	296.94	296.94	-1319	296.94	296.94	-1318	296.94	296.94	-1317	391.40	391.40

-1316	391.40	391.40	-1315	391.40	391.40	-1314	391.40	391.40	-1313	391.39	391.39	-1312	391.39	391.39
-1311	318.60	318.60	-1310	384.39	384.39	-1309	396.50	396.50	-1308	318.60	318.60	-1307	384.39	384.39
-1306	396.50	396.50	-1305	318.60	318.60	-1304	384.39	384.39	-1303	396.50	396.50	-1302	318.60	318.60
-1301	384.39	384.39	-1300	396.50	396.50	-1299	318.60	318.60	-1298	384.39	384.39	-1297	396.50	396.50
-1296	318.60	318.60	-1295	384.39	384.39	-1294	396.50	396.50	-1293	407.05	407.05	-1292	407.05	407.05
-1291	407.05	407.05	-1290	407.05	407.05	-1289	407.05	407.05	-1288	407.05	407.05	-1287	430.22	430.22
-1286	430.22	430.22	-1285	430.22	430.22	-1284	430.22	430.22	-1283	430.21	430.21	-1282	430.21	430.21
-1281	522.60	522.60	-1280	522.60	522.60	-1279	522.60	522.60	-1278	522.60	522.60	-1277	522.60	522.60
-1276	522.60	522.60	-1275	191.28	191.28	-1274	63.09	63.09	-1273	191.28	191.28	-1272	63.09	63.09
-1271	191.28	191.28	-1270	63.09	63.09	-1269	191.28	191.28	-1268	63.09	63.09	-1267	191.28	191.28
-1266	63.09	63.09	-1265	191.28	191.28	-1264	63.09	63.09	-1263	53.52	53.52	-1262	53.52	53.52
-1261	53.52	53.52	-1260	53.52	53.52	-1259	53.52	53.52	-1258	53.52	53.52	-1257	196.05	196.05
-1256	144.15	144.15	-1255	196.05	196.05	-1254	144.15	144.15	-1253	196.05	196.05	-1252	144.15	144.15
-1251	196.05	196.05	-1250	144.15	144.15	-1249	196.05	196.05	-1248	144.15	144.15	-1247	196.05	196.05
-1246	144.15	144.15	-1245	54.01	54.01	-1244	54.01	54.01	-1243	54.01	54.01	-1242	54.01	54.01
-1241	54.01	54.01	-1240	54.01	54.01	-1239	398.56	398.56	-1238	76.09	76.09	-1237	398.57	398.57
-1236	76.09	76.09	-1235	398.57	398.57	-1234	76.09	76.09	-1233	398.56	398.56	-1232	76.09	76.09
-1231	398.57	398.57	-1230	76.09	76.09	-1229	398.57	398.57	-1228	76.09	76.09	-1227	86.30	86.30
-1226	86.30	86.30	-1225	86.30	86.30	-1224	86.30	86.30	-1223	86.30	86.30	-1222	86.30	86.30
-1221	52.76	52.76	-1220	52.76	52.76	-1219	52.76	52.76	-1218	52.76	52.76	-1217	52.76	52.76
-1216	52.76	52.76	-1215	193.40	193.40	-1214	193.40	193.40	-1213	193.40	193.40	-1212	193.40	193.40
-1211	193.40	193.40	-1210	193.40	193.40	-1209	46.82	46.82	-1208	29.55	29.55	-1207	46.82	46.82
-1206	29.55	29.55	-1205	46.82	46.82	-1204	29.55	29.55	-1203	46.82	46.82	-1202	29.55	29.55
-1201	46.82	46.82	-1200	29.55	29.55	-1199	46.82	46.82	-1198	29.55	29.55	-1197	191.04	191.04
-1196	191.04	191.04	-1195	191.04	191.04	-1194	191.04	191.04	-1193	191.04	191.04	-1192	191.04	191.04
-1191	342.03	342.03	-1190	342.03	342.03	-1189	342.03	342.03	-1188	342.03	342.03	-1187	342.03	342.03
-1186	342.03	342.03	-1185	335.05	335.05	-1184	304.22	304.22	-1183	335.05	335.05	-1182	304.22	304.22
-1181	335.05	335.05	-1180	304.22	304.22	-1179	335.05	335.05	-1178	304.22	304.22	-1177	335.05	335.05
-1176	304.22	304.22	-1175	335.05	335.05	-1174	304.22	304.22	-1173	407.77	407.77	-1172	407.77	407.77
-1171	407.77	407.77	-1170	407.77	407.77	-1169	407.77	407.77	-1168	407.77	407.77	-1167	120.93	120.93
-1166	120.93	120.93	-1165	120.93	120.93	-1164	120.93	120.93	-1163	120.93	120.93	-1162	120.93	120.93
-1161	229.98	229.98	-1160	229.98	229.98	-1159	229.98	229.98	-1158	229.98	229.98	-1157	229.98	229.98
-1156	229.98	229.98	-1155	161.52	161.52	-1154	161.52	161.52	-1153	161.52	161.52	-1152	161.52	161.52
-1151	161.52	161.52	-1150	161.52	161.52	-1149	191.38	191.38	-1148	264.31	264.31	-1147	191.38	191.38
-1146	264.31	264.31	-1145	191.38	191.38	-1144	264.31	264.31	-1143	191.38	191.38	-1142	264.31	264.31
-1141	191.38	191.38	-1140	264.31	264.31	-1139	191.38	191.38	-1138	264.31	264.31	-1137	287.64	287.64
-1136	256.38	256.38	-1135	291.93	291.93	-1134	287.64	287.64	-1133	256.38	256.38	-1132	291.93	291.93
-1131	287.64	287.64	-1130	256.38	256.38	-1129	291.93	291.93	-1128	287.64	287.64	-1127	256.38	256.38
-1126	291.93	291.93	-1125	287.64	287.64	-1124	256.38	256.38	-1123	291.93	291.93	-1122	287.64	287.64
-1121	256.38	256.38	-1120	291.93	291.93	-1119	354.56	354.56	-1118	328.60	328.60	-1117	354.56	354.56
-1116	328.60	328.60	-1115	354.56	354.56	-1114	328.60	328.60	-1113	354.56	354.56	-1112	328.60	328.60
-1111	354.56	354.56	-1110	328.60	328.60	-1109	354.56	354.56	-1108	328.60	328.60	-1107	265.85	265.85
-1106	318.90	318.90	-1105	350.40	350.40	-1104	265.85	265.85	-1103	318.90	318.90	-1102	350.41	350.41
-1101	265.85	265.85	-1100	318.90	318.90	-1099	350.41	350.41	-1098	265.85	265.85	-1097	318.90	318.90
-1096	350.40	350.40	-1095	265.85	265.85	-1094	318.90	318.90	-1093	350.41	350.41	-1092	265.85	265.85
-1091	318.90	318.90	-1090	350.41	350.41	-1089	339.83	339.83	-1088	339.83	339.83	-1087	339.83	339.83
-1086	339.83	339.83	-1085	339.83	339.83	-1084	339.83	339.83	-1083	252.38	252.38	-1082	252.38	252.38
-1081	252.38	252.38	-1080	252.38	252.38	-1079	252.38	252.38	-1078	252.38	252.38	-1077	202.74	202.74
-1076	202.75	202.75	-1075	202.75	202.75	-1074	202.75	202.75	-1073	202.75	202.75	-1072	202.75	202.75
-1071	43.69	43.69	-1070	153.39	153.39	-1069	43.69	43.69	-1068	153.39	153.39	-1067	43.69	43.69
-1066	153.39	153.39	-1065	43.69	43.69	-1064	153.39	153.39	-1063	43.69	43.69	-1062	153.39	153.39
-1061	43.69	43.69	-1060	153.39	153.39	-1059	335.00	335.00	-1058	380.52	380.52	-1057	335.00	335.00
-1056	380.52	380.52	-1055	335.00	335.00	-1054	380.52	380.52	-1053	335.00	335.00	-1052	380.52	380.52
-1051	335.00	335.00	-1050	380.52	380.52	-1049	335.00	335.00	-1048	380.52	380.52	-1047	307.94	307.94
-1046	307.94	307.94	-1045	307.94	307.94	-1044	307.94	307.94	-1043	307.94	307.94	-1042	307.94	307.94
-1041	353.09	353.09	-1040	353.09	353.09	-1039	353.09	353.09	-1038	353.09	353.09	-1037	353.09	353.09
-1036	353.09	353.09	-1035	270.46	270.46	-1034	270.46	270.46	-1033	270.46	270.46	-1032	270.46	270.46
-1031	270.46	270.46	-1030	270.46	270.46	-1029	343.97	343.97	-1028	343.97	343.97	-1027	343.97	343.97
-1026	343.97	343.97	-1025	343.97	343.97	-1024	343.97	343.97	-1023	256.67	256.67	-1022	256.66	256.66
-1021	256.67	256.67	-1020	256.66	256.66	-1019	256.66	256.66	-1018	256.66	256.66	-1017	363.58	363.58
-1016	363.58	363.58	-1015	363.58	363.58	-1014	363.58	363.58	-1013	363.58	363.58	-1012	363.58	363.58
-1011	246.16	246.16	-1010	246.16	246.16	-1009	246.16	246.16	-1008	246.16	246.16	-1007	246.16	246.16
-1006	246.16	246.16	-1005	179.31	179.31	-1004	179.31	179.31	-1003	179.31	179.31	-1002	179.31	179.31
-1001	179.31	179.31	-1000	179.31	179.31	-999	140.97	140.97	-998	140.97	140.97	-997	140.97	140.97
-996	140.97	140.97	-995	140.97	140.97	-994	140.97	140.97	-993	370.49	370.49	-992	370.49	370.49
-991	370.49	370.49	-990	370.49	370.49	-989	370.49	370.49	-988	370.49	370.49	-987	377.56	377.56
-986	377.56	377.56	-985	377.56	377.56	-984	377.56	377.56	-983	377.56	377.56	-982	377.56	377.56
-981	249.49	249.49	-980	249.49	249.49	-979	249.49	249.49	-978	249.49	249.49	-977	249.49	249.49
-976	249.49	249.49	-975	424.44	424.44	-974	578.54	578.54	-973	424.44	424.44	-972	578.54	578.54
-971	424.44	424.44	-970	578.54	578.54	-969	424.44	424.44	-968	578.54	578.54	-967	424.44	424.44
-966	578.53	578.53	-965	424.44	424.44	-964	578.53	578.53	-963	80.93	80.93	-962	24.04	24.04
-961	80.94	80.94	-960	24.04	24.04	-959	80.93	80.93	-958	24.04	24.04	-957	80.93	80.93
-956	24.04	24.04	-955	80.93	80.93	-954	24.04	24.04	-953	80.93	80.93	-952	24.04	24.04
-951	505.21	505.21	-950	504.81	504.81	-949	505.21	505.21	-948	504.81	504.81	-947	505.21	505.21
-946	504.81	504.81	-945	505.21	505.21	-944	504.81	504.81	-943	505.21	505.21	-942	504.81	504.81
-941	505.21	505.21	-940	504.81	504.81	-939	432.44	432.44	-938	480.49	480.49	-937	432.44	432.44
-936	480.49	480.49	-935	432.44	432.44	-934	480.49	480.49	-933	432.44	432.44	-932	480.49	480.49
-931	432.44	432.44	-930	480.49	480.49	-929	432.44	432.44	-928	480.49	480.49	-927	490.87	490.87
-926	490.87	490.87	-925	490.87	490.87	-924	490.87	490.87	-923	490.87	490.87	-922	490.87	490.87

-921	476.61	476.61	-920	476.61	476.61	-919	476.61	476.61	-918	476.61	476.61	-917	476.61	476.61
-916	476.61	476.61	-915	348.25	348.25	-914	160.90	160.90	-913	348.25	348.25	-912	160.90	160.90
-911	348.25	348.25	-910	160.90	160.90	-909	348.25	348.25	-908	160.90	160.90	-907	348.25	348.25
-906	160.90	160.90	-905	348.25	348.25	-904	160.90	160.90	-903	144.74	144.74	-902	98.86	98.86
-901	126.40	126.40	-900	167.52	167.52	-899	144.74	144.74	-898	98.86	98.86	-897	126.40	126.40
-896	167.52	167.52	-895	144.74	144.74	-894	98.86	98.86	-893	126.40	126.40	-892	167.52	167.52
-891	144.74	144.74	-890	98.86	98.86	-889	126.40	126.40	-888	167.52	167.52	-887	144.74	144.74
-886	98.86	98.86	-885	126.40	126.40	-884	167.52	167.52	-871	86.88	86.88	-870	67.44	67.44
-869	67.44	67.44	-868	91.65	91.65	-867	57.42	57.42	-866	57.42	57.42	-865	57.42	57.42
-864	67.44	67.44	-863	86.88	86.88	-862	67.44	67.44	-861	67.44	67.44	-860	91.65	91.65
-859	57.42	57.42	-858	57.42	57.42	-857	57.42	57.42	-856	67.44	67.44	-855	86.88	86.88
-854	67.44	67.44	-853	67.44	67.44	-852	91.65	91.65	-851	57.42	57.42	-850	57.42	57.42
-849	57.42	57.42	-848	67.44	67.44	-847	86.88	86.88	-846	67.44	67.44	-845	67.44	67.44
-844	91.65	91.65	-843	57.42	57.42	-842	57.42	57.42	-841	57.42	57.42	-840	67.44	67.44
-839	86.88	86.88	-838	67.44	67.44	-837	67.44	67.44	-836	91.65	91.65	-835	57.42	57.42
-834	57.42	57.42	-833	57.42	57.42	-832	67.44	67.44	-831	86.88	86.88	-830	67.44	67.44
-829	67.44	67.44	-828	91.65	91.65	-827	57.42	57.42	-826	57.42	57.42	-825	57.42	57.42
-824	67.44	67.44	-823	98.86	98.86	-564	167.52	167.52	-178	53.52	53.52	-174	144.15	144.15
-173	54.01	54.01	-172	76.09	76.09	-171	86.30	86.30	-169	52.76	52.76	-168	193.40	193.40
-167	191.04	191.04	-166	304.22	304.22	-165	342.03	342.03	-164	335.05	335.05	-163	167.52	167.52
-162	407.77	407.77	-161	480.49	480.49	-160	432.44	432.44	-159	384.39	384.39	-158	126.40	126.40
-157	318.60	318.60	-156	196.05	196.05	-155	296.94	296.94	-154	391.40	391.40	-153	396.50	396.50
-152	407.05	407.05	-151	430.21	430.21	-150	522.60	522.60	-149	398.57	398.57	-148	63.09	63.09
-147	191.28	191.28	-146	256.38	256.38	-145	287.64	287.64	-144	318.90	318.90	-143	265.85	265.85
-142	106.40	106.40	-141	212.79	212.79	-140	6.60	6.60	-139	59.32	59.32	-137	9.33	9.33
-136	14.65	14.65	-135	16.65	16.65	-134	7.33	7.33	-133	29.55	29.55	-132	46.82	46.82
-131	61.69	61.69	-130	89.58	89.58	-129	145.82	145.82	-128	234.55	234.55	-127	289.48	289.48
-126	274.72	274.72	-125	164.87	164.87	-124	98.86	98.86	-123	263.16	263.16	-122	328.60	328.60
-121	354.56	354.56	-120	380.52	380.52	-119	144.74	144.74	-118	335.00	335.00	-117	160.90	160.90
-116	348.25	348.25	-115	476.61	476.61	-114	490.87	490.87	-113	504.81	504.81	-112	505.21	505.21
-111	578.53	578.53	-110	424.44	424.44	-109	24.04	24.04	-106	80.93	80.93	-105	249.49	249.49
-104	377.56	377.56	-103	140.97	140.97	-102	179.31	179.31	-101	370.49	370.49	-100	246.16	246.16
-99	363.58	363.58	-98	256.66	256.66	-97	343.97	343.97	-96	270.46	270.46	-95	353.09	353.09
-94	43.69	43.69	-93	153.39	153.39	-92	202.75	202.75	-91	252.38	252.38	-90	350.40	350.40
-89	339.83	339.83	-88	307.94	307.94	-87	291.93	291.93	-86	264.31	264.31	-85	191.38	191.38
-84	161.52	161.52	-83	229.98	229.98	-82	120.93	120.93	-8	86.88	86.88	-7	67.44	67.44
-6	67.44	67.44	-5	67.44	67.44	-4	91.65	91.65	-3	57.42	57.42	-2	57.42	57.42
-1	57.42	57.42	2	446.83	446.83	4	446.82	446.82	6	437.04	437.04	8	436.97	436.97
9	425.49	425.49	10	378.10	378.10	11	397.98	397.98	12	215.85	215.85	13	345.36	345.36
14	316.75	316.75	15	324.83	324.83	16	345.09	345.09	17	295.09	295.09	18	334.10	334.10
19	425.40	425.40	20	511.07	511.07	21	498.11	498.11	22	351.30	351.30	35	218.09	218.09
36	352.59	352.59	37	440.73	440.73	38	289.63	289.63	39	261.98	261.98	40	93.93	93.93
41	113.51	113.51	42	87.91	87.91	43	71.45	71.45	44	225.97	225.97	45	89.61	89.61
46	324.85	324.85	47	271.23	271.23	48	171.02	171.02	49	416.45	416.45	50	443.69	443.69
51	283.83	283.83	52	85.58	85.58	53	152.11	152.11	54	455.93	455.93	55	193.06	193.06
56	98.90	98.90	57	383.05	383.05	58	467.71	467.71	59	449.91	449.91	60	263.53	263.53
61	495.13	495.13	62	100.77	100.77	63	267.94	267.94	64	290.43	290.43	65	44.11	44.11
66	310.18	310.18	67	106.44	106.44	68	28.05	28.05	69	384.44	384.44	70	333.04	333.04
71	97.55	97.55	72	172.25	172.25	73	49.15	49.15	74	44.77	44.77	75	430.08	430.08
76	212.55	212.55	77	0.00	47.39	78	550.57	550.57	79	140.89	140.89	80	216.46	216.46
81	170.54	170.54	82	114.03	114.03	83	72.17	72.17	84	23.76	23.76	85	27.58	27.58
86	4.19	4.19	87	96.73	96.73	88	143.54	143.54	89	323.38	323.38	90	321.02	321.02
91	0.00	11.06	92	221.54	221.54	93	87.95	87.95	94	7.99	7.99	95	186.71	186.71
96	26.63	26.63	97	336.61	336.61	98	308.32	308.32	99	30.85	30.85	100	226.58	226.58
101	44.79	44.79	102	310.12	310.12	103	334.88	334.88	104	329.74	329.74	105	240.12	240.12
106	23.57	23.57	107	29.81	29.81	108	2.96	2.96	109	12.73	12.73	110	218.76	218.76
111	169.83	169.83	112	305.06	305.06	113	307.21	307.21	114	244.89	244.89	115	72.91	72.91
116	117.28	117.28	117	330.51	330.51	118	0.00	125.12	119	68.96	68.96	120	214.93	214.93
121	321.17	321.17	122	312.56	312.56	123	137.36	137.36	124	252.35	252.35	125	82.43	82.43
126	307.76	307.76	127	210.35	210.35	128	78.19	78.19	129	75.54	75.54	130	171.24	171.24
131	221.88	221.88	132	158.05	158.05	133	28.56	28.56	134	106.87	106.87	135	179.64	179.64
136	98.88	98.88	137	321.65	321.65	138	330.82	330.82	139	198.32	198.32	140	69.41	69.41
141	88.94	88.94	142	176.61	176.61	143	188.81	188.81	144	104.97	104.97	145	153.67	153.67
146	23.75	23.75	147	71.82	71.82	617	218.76	218.76	624	23.57	23.57	674	240.12	240.12
904	47.39	47.39	911	98.90	98.90	918	44.78	44.78	1402	152.11	152.11	1563	68.96	68.96
1682	125.12	125.12	1689	169.83	169.83	1843	171.01	171.01	1845	446.83	446.83	1847	446.82	446.82
1849	437.04	437.04	1851	436.97	436.97	1852	425.49	425.49	1853	378.10	378.10	1854	397.98	397.98
1855	345.36	345.36	1856	316.75	316.75	1857	324.83	324.83	1858	345.09	345.09	1859	295.09	295.09
1860	334.10	334.10	1861	425.40	425.40	1862	511.07	511.07	1863	498.11	498.11	1864	351.30	351.30
1865	215.85	215.85	1867	446.83	446.83	1869	446.82	446.82	1871	437.04	437.04	1873	436.97	436.97
1874	425.49	425.49	1875	378.10	378.10	1876	397.98	397.98	1877	345.36	345.36	1878	316.75	316.75
1879	324.83	324.83	1880	345.09	345.09	1881	295.09	295.09	1882	334.10	334.10	1883	425.40	425.40
1884	511.07	511.07	1885	498.11	498.11	1886	351.30	351.30	1887	215.85	215.85	1889	446.83	446.83
1891	446.82	446.82	1893	437.04	437.04	1895	436.97	436.97	1896	425.49	425.49	1897	378.10	378.10
1898	397.98	397.98	1899	345.36	345.36	1900	316.75	316.75	1901	324.83	324.83	1902	345.09	345.09
1903	295.09	295.09	1904	334.10	334.10	1905	425.40	425.40	1906	511.07	511.07	1907	498.11	498.11
1908	351.30	351.30	1909	215.85	215.85	1911	446.83	446.83	1913	446.82	446.82	1915	437.04	437.04
1917	436.97	436.97	1918	425.49	425.49	1919	378.10	378.10	1920	397.98	397.98	1921	345.36	345.36
1922	316.75	316.75	1923	324.83	324.83	1924	345.09	345.09	1925	295.09	295.09	1926	334.10	334.10

1927	425.40	425.40	1928	511.07	511.07	1929	498.11	498.11	1930	351.30	351.30	1931	215.85	215.85
1933	446.83	446.83	1935	446.82	446.82	1937	437.04	437.04	1939	436.97	436.97	1940	425.49	425.49
1941	378.10	378.10	1942	397.98	397.98	1943	345.36	345.36	1944	316.75	316.75	1945	324.83	324.83
1946	345.09	345.09	1947	295.09	295.09	1948	334.10	334.10	1949	425.40	425.40	1950	511.07	511.07
1951	498.11	498.11	1952	351.30	351.30	1953	215.85	215.85	1955	446.83	446.83	1957	446.82	446.82
1959	437.04	437.04	1961	436.97	436.97	1962	425.49	425.49	1963	378.10	378.10	1964	397.98	397.98
1965	345.36	345.36	1966	316.75	316.75	1967	324.83	324.83	1968	345.09	345.09	1969	295.09	295.09
1970	334.10	334.10	1971	425.40	425.40	1972	511.07	511.07	1973	498.11	498.11	1974	351.30	351.30
1975	215.85	215.85	1976	267.93	267.93	1977	290.43	290.43	1978	212.55	212.55	1979	172.25	172.25
1980	440.73	440.73	1981	307.76	307.76	1982	267.93	267.93	1983	290.43	290.43	1984	212.55	212.55
1985	172.25	172.25	1986	440.73	440.73	1987	307.76	307.76	1988	267.94	267.94	1989	290.43	290.43
1990	212.55	212.55	1991	172.25	172.25	1992	440.73	440.73	1993	307.76	307.76	1994	267.93	267.93
1995	290.43	290.43	1996	212.55	212.55	1997	172.25	172.25	1998	440.73	440.73	1999	307.76	307.76
2000	267.93	267.93	2001	290.43	290.43	2002	212.55	212.55	2003	172.25	172.25	2004	440.73	440.73
2005	307.76	307.76	2006	267.93	267.93	2007	290.43	290.43	2008	212.55	212.55	2009	172.25	172.25
2010	440.73	440.73	2011	307.76	307.76	2012	171.02	171.02	2013	85.58	85.58	2014	152.11	152.11
2015	193.06	193.06	2016	100.77	100.77	2017	47.39	47.39	2018	44.11	44.11	2019	44.77	44.77
2020	263.53	263.53	2021	98.90	98.90	2022	240.12	240.12	2023	26.63	26.63	2024	23.57	23.57
2025	30.85	30.85	2026	218.76	218.76	2027	44.79	44.79	2028	169.83	169.83	2029	72.91	72.91
2030	125.12	125.12	2031	117.28	117.28	2032	68.96	68.96	2033	137.36	137.36	2034	171.02	171.02
2035	85.58	85.58	2036	152.11	152.11	2037	193.06	193.06	2038	100.77	100.77	2039	47.39	47.39
2040	44.11	44.11	2041	44.77	44.77	2042	263.53	263.53	2043	98.90	98.90	2044	240.12	240.12
2045	26.63	26.63	2046	23.57	23.57	2047	30.85	30.85	2048	218.76	218.76	2049	44.79	44.79
2050	169.83	169.83	2051	72.91	72.91	2052	125.12	125.12	2053	117.28	117.28	2054	68.96	68.96
2055	137.36	137.36	2056	171.02	171.02	2057	85.58	85.58	2058	152.11	152.11	2059	193.06	193.06
2060	100.77	100.77	2061	47.39	47.39	2062	44.11	44.11	2063	44.77	44.77	2064	263.53	263.53
2065	98.90	98.90	2066	240.12	240.12	2067	26.63	26.63	2068	23.57	23.57	2069	30.85	30.85
2070	218.76	218.76	2071	44.79	44.79	2072	169.83	169.83	2073	72.91	72.91	2074	125.12	125.12
2075	117.28	117.28	2076	68.96	68.96	2077	137.36	137.36	2078	171.02	171.02	2079	85.58	85.58
2080	152.11	152.11	2081	193.06	193.06	2082	100.77	100.77	2083	47.39	47.39	2084	44.11	44.11
2085	44.77	44.77	2086	263.53	263.53	2087	98.90	98.90	2088	240.12	240.12	2089	26.63	26.63
2090	23.57	23.57	2091	30.85	30.85	2092	218.76	218.76	2093	44.79	44.79	2094	169.83	169.83
2095	72.91	72.91	2096	125.12	125.12	2097	117.28	117.28	2098	68.96	68.96	2099	137.36	137.36
2100	171.02	171.02	2101	85.58	85.58	2102	152.11	152.11	2103	193.06	193.06	2104	100.77	100.77
2105	47.39	47.39	2106	44.11	44.11	2107	44.77	44.77	2108	263.53	263.53	2109	98.90	98.90
2110	240.12	240.12	2111	26.63	26.63	2112	23.57	23.57	2113	30.85	30.85	2114	218.76	218.76
2115	44.79	44.79	2116	169.83	169.83	2117	72.91	72.91	2118	125.12	125.12	2119	117.28	117.28
2120	68.96	68.96	2121	137.36	137.36	2122	225.97	225.97	2123	225.97	225.97	2124	225.97	225.97
2125	225.97	225.97	2126	225.97	225.97	2127	225.97	225.97	2128	218.09	218.09	2129	352.59	352.59
2130	218.09	218.09	2131	352.59	352.59	2132	218.09	218.09	2133	352.59	352.59	2134	218.09	218.09
2135	352.59	352.59	2136	218.09	218.09	2137	352.59	352.59	2138	218.09	218.09	2139	352.59	352.59
2140	443.69	443.69	2141	443.69	443.69	2142	443.68	443.68	2143	443.69	443.69	2144	443.68	443.68
2145	443.69	443.69	2146	467.71	467.71	2147	455.93	455.93	2148	467.71	467.71	2149	455.93	455.93
2150	467.71	467.71	2151	455.93	455.93	2152	467.71	467.71	2153	455.93	455.93	2154	467.71	467.71
2155	455.93	455.93	2156	467.71	467.71	2157	455.93	455.93	2158	29.81	29.81	2159	87.95	87.95
2160	29.81	29.81	2161	87.95	87.95	2162	29.81	29.81	2163	87.95	87.95	2164	29.81	29.81
2165	87.95	87.95	2166	29.81	29.81	2167	87.95	87.95	2168	29.81	29.81	2169	87.95	87.95
2170	384.44	384.44	2171	550.57	550.57	2172	384.44	384.44	2173	550.57	550.57	2174	384.44	384.44
2175	550.57	550.57	2176	384.44	384.44	2177	550.57	550.57	2178	384.44	384.44	2179	550.57	550.57
2180	384.44	384.44	2181	550.57	550.57	2182	221.54	221.54	2183	221.54	221.54	2184	221.54	221.54
2185	221.54	221.54	2186	221.54	221.54	2187	221.54	221.54	2188	336.61	336.61	2189	336.61	336.61
2190	336.61	336.61	2191	336.61	336.61	2192	336.61	336.61	2193	336.61	336.61	2194	308.32	308.32
2195	308.32	308.32	2196	308.32	308.32	2197	308.32	308.32	2198	308.32	308.32	2199	308.32	308.32
2200	226.58	226.58	2201	226.58	226.58	2202	226.58	226.58	2203	226.58	226.58	2204	226.58	226.58
2205	226.58	226.58	2206	310.12	310.12	2207	310.12	310.12	2208	310.12	310.12	2209	310.12	310.12
2210	310.12	310.12	2211	310.12	310.12	2212	244.89	244.89	2213	244.89	244.89	2214	244.89	244.89
2215	244.89	244.89	2216	244.89	244.89	2217	244.89	244.89	2218	307.21	307.21	2219	307.21	307.21
2220	307.21	307.21	2221	307.21	307.21	2222	307.21	307.21	2223	307.21	307.21	2224	330.51	330.51
2225	330.51	330.51	2226	330.51	330.51	2227	330.51	330.51	2228	330.51	330.51	2229	330.51	330.51
2230	69.41	69.41	2231	69.41	69.41	2232	69.41	69.41	2233	69.41	69.41	2234	69.41	69.41
2235	69.41	69.41	2236	106.87	106.87	2237	106.87	106.87	2238	106.87	106.87	2239	106.87	106.87
2240	106.87	106.87	2241	106.87	106.87	2242	158.05	158.05	2243	158.05	158.05	2244	158.05	158.05
2245	158.05	158.05	2246	158.05	158.05	2247	158.05	158.05	2248	252.35	252.35	2249	252.35	252.35
2250	252.35	252.35	2251	252.35	252.35	2252	252.35	252.35	2253	252.35	252.35	2254	312.56	312.56
2255	312.56	312.56	2256	312.56	312.56	2257	312.56	312.56	2258	312.56	312.56	2259	312.56	312.56
2260	321.17	321.17	2261	321.17	321.17	2262	321.17	321.17	2263	321.17	321.17	2264	321.17	321.17
2265	321.17	321.17	2266	221.88	221.88	2267	221.88	221.88	2268	221.88	221.88	2269	221.88	221.88
2270	221.88	221.88	2271	221.88	221.88	2272	198.32	198.32	2273	198.32	198.32	2274	198.32	198.32
2275	198.32	198.32	2276	198.32	198.32	2277	198.32	198.32	2278	88.94	88.94	2279	88.94	88.94
2280	88.94	88.94	2281	88.94	88.94	2282	88.94	88.94	2283	88.94	88.94	2284	416.45	416.45
2285	416.45	416.45	2286	416.45	416.45	2287	416.45	416.45	2288	416.45	416.45	2289	416.45	416.45
2290	383.05	383.05	2291	383.05	383.05	2292	383.05	383.05	2293	383.05	383.05	2294	383.05	383.05
2295	383.05	383.05	2296	26.63	26.63	2297	334.88	334.88	2298	321.02	321.02	2299	334.88	334.88
2300	321.02	321.02	2301	334.88	334.88	2302	321.02	321.02	2303	334.88	334.88	2304	321.02	321.02
2305	334.88	334.88	2306	321.02	321.02	2307	334.88	334.88	2308	321.02	321.02	2309	87.91	87.91
2310	87.91	87.91	2311	87.91	87.91	2312	87.91	87.91	2313	87.91	87.91	2314	87.91	87.91
2315	333.04	333.04	2316	97.55	97.55	2317	333.04	333.04	2318	97.55	97.55	2319	333.04	333.04
2320	97.55	97.55	2321	333.04	333.04	2322	97.55	97.55	2323	333.04	333.04	2324	97.55	97.55
2325	333.04	333.04	2326	97.55	97.55	2327	71.45	71.45	2328	71.45	71.45	2329	71.45	71.45

2330	71.45	71.45	2331	71.45	71.45	2332	71.45	71.45	2333	263.53	263.53	2334	0.00	100.77
2335	140.89	140.89	2336	140.89	140.89	2337	140.89	140.89	2338	140.89	140.89	2339	140.89	140.89
2340	140.89	140.89	2341	89.61	89.61	2342	89.61	89.61	2343	89.61	89.61	2344	89.61	89.61
2345	89.61	89.61	2346	89.61	89.61	2347	78.19	78.19	2348	210.35	210.35	2349	78.19	78.19
2350	210.35	210.35	2351	78.19	78.19	2352	210.35	210.35	2353	78.19	78.19	2354	210.35	210.35
2355	78.19	78.19	2356	210.35	210.35	2357	78.19	78.19	2358	210.35	210.35	2359	310.18	310.18
2360	495.13	495.13	2361	310.18	310.18	2362	495.13	495.13	2363	310.18	310.18	2364	495.13	495.13
2365	310.18	310.18	2366	495.13	495.13	2367	310.18	310.18	2368	495.13	495.13	2369	310.18	310.18
2370	495.13	495.13	2371	449.91	449.91	2372	449.91	449.91	2373	449.91	449.91	2374	449.91	449.91
2375	449.91	449.91	2376	449.91	449.91	2377	283.83	283.83	2378	283.83	283.83	2379	283.83	283.83
2380	283.83	283.83	2381	283.83	283.83	2382	283.83	283.83	2383	289.63	289.63	2384	289.63	289.63
2385	289.63	289.63	2386	289.63	289.63	2387	289.63	289.63	2388	289.63	289.63	2389	261.98	261.98
2390	261.98	261.98	2391	261.98	261.98	2392	261.98	261.98	2393	261.98	261.98	2394	261.98	261.98
2395	324.85	324.85	2396	324.85	324.85	2397	324.85	324.85	2398	324.85	324.85	2399	324.85	324.85
2400	324.85	324.85	2401	193.06	193.06	2402	7.99	7.99	2403	7.99	7.99	2404	7.99	7.99
2405	7.99	7.99	2406	7.99	7.99	2407	0.00	7.99	2408	137.36	137.36	2409	214.93	214.93
2410	214.93	214.93	2411	214.93	214.93	2412	214.93	214.93	2413	214.93	214.93	2414	214.93	214.93
2415	28.56	28.56	2416	82.43	82.43	2417	28.56	28.56	2418	82.43	82.43	2419	28.56	28.56
2420	82.43	82.43	2421	28.56	28.56	2422	82.43	82.43	2423	28.56	28.56	2424	82.43	82.43
2425	28.56	28.56	2426	82.43	82.43	2427	117.28	117.28	2428	0.00	72.91	2429	44.79	44.79
2430	30.85	30.85	2431	104.97	104.97	2432	71.82	71.82	2433	153.67	153.67	2434	104.97	104.97
2435	71.82	71.82	2436	153.67	153.67	2437	104.97	104.97	2438	71.82	71.82	2439	153.67	153.67
2440	104.97	104.97	2441	71.82	71.82	2442	153.67	153.67	2443	104.97	104.97	2444	71.82	71.82
2445	153.67	153.67	2446	104.97	104.97	2447	71.82	71.82	2448	153.67	153.67	2449	23.75	23.75
2450	23.75	23.75	2451	23.75	23.75	2452	23.75	23.75	2453	23.75	23.75	2454	23.75	23.75
2455	321.65	321.65	2456	188.81	188.81	2457	321.65	321.65	2458	188.81	188.81	2459	321.65	321.65
2460	188.81	188.81	2461	321.65	321.65	2462	188.81	188.81	2463	321.65	321.65	2464	188.81	188.81
2465	321.65	321.65	2466	188.81	188.81	2467	176.61	176.61	2468	330.82	330.82	2469	176.61	176.61
2470	330.82	330.82	2471	176.61	176.61	2472	330.82	330.82	2473	176.61	176.61	2474	330.82	330.82
2475	176.61	176.61	2476	330.82	330.82	2477	176.61	176.61	2478	330.82	330.82	2479	179.64	179.64
2480	179.64	179.64	2481	179.64	179.64	2482	179.64	179.64	2483	179.64	179.64	2484	179.64	179.64
2485	98.88	98.88	2486	98.88	98.88	2487	98.88	98.88	2488	98.88	98.88	2489	98.88	98.88
2490	98.88	98.88	2491	75.54	75.54	2492	171.24	171.24	2493	75.54	75.54	2494	171.24	171.24
2495	75.54	75.54	2496	171.24	171.24	2497	75.54	75.54	2498	171.24	171.24	2499	75.54	75.54
2500	171.24	171.24	2501	75.54	75.54	2502	171.24	171.24	2503	305.06	305.06	2504	305.06	305.06
2505	305.06	305.06	2506	305.06	305.06	2507	305.06	305.06	2508	305.06	305.06	2509	12.73	12.73
2510	12.73	12.73	2511	12.73	12.73	2512	12.73	12.73	2513	12.73	12.73	2514	12.73	12.73
2515	2.96	2.96	2516	2.96	2.96	2517	2.96	2.96	2518	2.96	2.96	2519	2.96	2.96
2520	2.96	2.96	2521	11.06	11.06	2522	11.06	11.06	2523	11.06	11.06	2524	11.06	11.06
2525	11.06	11.06	2526	11.06	11.06	2527	329.74	329.74	2528	329.74	329.74	2529	329.74	329.74
2530	329.74	329.74	2531	329.74	329.74	2532	329.74	329.74	2533	323.38	323.38	2534	323.38	323.38
2535	323.38	323.38	2536	323.38	323.38	2537	323.38	323.38	2538	323.38	323.38	2539	186.71	186.71
2540	186.71	186.71	2541	186.71	186.71	2542	186.71	186.71	2543	186.71	186.71	2544	186.71	186.71
2545	143.54	143.54	2546	143.54	143.54	2547	143.54	143.54	2548	143.54	143.54	2549	143.54	143.54
2550	143.54	143.54	2551	96.73	96.73	2552	96.73	96.73	2553	96.73	96.73	2554	96.73	96.73
2555	96.73	96.73	2556	96.73	96.73	2557	27.58	27.58	2558	27.58	27.58	2559	27.58	27.58
2560	27.58	27.58	2561	27.58	27.58	2562	27.58	27.58	2563	4.19	4.19	2564	4.19	4.19
2565	4.19	4.19	2566	4.19	4.19	2567	4.19	4.19	2568	4.19	4.19	2569	72.17	72.17
2570	114.03	114.03	2571	23.76	23.76	2572	72.17	72.17	2573	114.03	114.03	2574	23.76	23.76
2575	72.17	72.17	2576	114.03	114.03	2577	23.76	23.76	2578	72.17	72.17	2579	114.03	114.03
2580	23.76	23.76	2581	72.17	72.17	2582	114.03	114.03	2583	23.76	23.76	2584	72.17	72.17
2585	114.03	114.03	2586	23.76	23.76	2587	170.54	170.54	2588	170.54	170.54	2589	170.54	170.54
2590	170.54	170.54	2591	170.54	170.54	2592	170.54	170.54	2593	271.23	271.23	2594	271.23	271.23
2595	271.23	271.23	2596	271.23	271.23	2597	271.23	271.23	2598	271.23	271.23	2599	216.46	216.46
2600	216.46	216.46	2601	216.46	216.46	2602	216.46	216.46	2603	216.46	216.46	2604	216.47	216.47
2605	430.08	430.08	2606	430.08	430.08	2607	430.08	430.08	2608	430.08	430.08	2609	430.08	430.08
2610	430.08	430.08	2611	49.15	49.15	2612	49.15	49.15	2613	49.15	49.15	2614	49.15	49.15
2615	49.15	49.15	2616	49.15	49.15	2617	106.44	106.44	2618	106.44	106.44	2619	106.44	106.44
2620	106.44	106.44	2621	106.44	106.44	2622	106.44	106.44	2623	28.05	28.05	2624	28.05	28.05
2625	28.05	28.05	2626	28.05	28.05	2627	28.05	28.05	2628	28.05	28.05	2629	44.11	44.11
2630	85.58	85.58	2631	93.93	93.93	2632	93.93	93.93	2633	93.93	93.93	2634	93.93	93.93
2635	93.93	93.93	2636	93.93	93.93	2637	113.51	113.51	2638	113.51	113.51	2639	113.51	113.51
2640	113.51	113.51	2641	113.51	113.51	2642	113.51	113.51						

Totali masse nodi

Mo	Mz
<kg>	<kg>
357584.00	357950.00

Elenco modi di vibrare, masse partecipanti e coefficienti di partecipazione

Simbologia

Modo = Numero del modo di vibrare
C = * indica che il modo è stato considerato
Per. = Periodo
Diff. = Minima differenza percentuale dagli altri periodi

Φ_x = Coefficiente di partecipazione in dir. X
Φ_y = Coefficiente di partecipazione in dir. Y
Φ_z = Coefficiente di partecipazione in dir. Z
%Mx = Percentuale massa partecipante in dir. X
%My = Percentuale massa partecipante in dir. Y
%Mz = Percentuale massa partecipante in dir. Z
%Jpz = Percentuale momento d'inerzia polare partecipante intorno all'asse Z

Modo	C	Per.	Diff.	Φ_x	Φ_y	Φ_z	%Mx	%My	%Mz	%Jpz
1	*	0.88	75.35	-0.21	158.26	0.57	0.00	70.04	0.00	0.00
2	*	0.50	29.54	1.54	0.69	0.54	0.01	0.00	0.00	0.00
3	*	0.39	6.14	1.15	32.96	0.94	0.00	3.04	0.00	0.00
4	*	0.37	6.14	-4.12	4.30	-0.55	0.05	0.05	0.00	0.00
5	*	0.34	2.42	-0.66	24.59	-1.70	0.00	1.69	0.01	0.00
6	*	0.33	2.07	0.05	3.66	2.57	0.00	0.04	0.02	0.00
7	*	0.33	1.28	1.70	0.66	1.67	0.01	0.00	0.01	0.00
8	*	0.32	1.28	0.57	0.42	3.23	0.00	0.00	0.03	0.00
9	*	0.31	2.17	1.10	-1.76	3.52	0.00	0.01	0.03	0.00
10	*	0.30	2.17	-1.37	7.72	-1.81	0.01	0.17	0.01	0.00
11	*	0.30	0.84	0.28	6.63	-1.49	0.00	0.12	0.01	0.00
12	*	0.29	0.84	-0.17	4.11	1.84	0.00	0.05	0.01	0.00
13	*	0.29	0.82	-1.01	1.86	-0.65	0.00	0.01	0.00	0.00
14	*	0.29	0.03	-2.25	-1.85	0.54	0.01	0.01	0.00	0.00
15	*	0.29	0.03	0.46	2.31	-1.72	0.00	0.01	0.01	0.00
16	*	0.29	0.46	0.54	1.66	-1.00	0.00	0.01	0.00	0.00
17	*	0.28	0.02	-0.79	-0.65	3.67	0.00	0.00	0.04	0.00
18	*	0.28	0.02	-0.27	-2.26	3.48	0.00	0.01	0.03	0.00
19	*	0.28	0.06	-1.21	3.14	-9.10	0.00	0.03	0.23	0.00
20	*	0.28	0.04	-0.07	1.98	-3.07	0.00	0.01	0.03	0.00
21	*	0.28	0.04	-0.37	-0.66	3.25	0.00	0.00	0.03	0.00
22	*	0.28	0.35	-1.07	1.12	-1.49	0.00	0.00	0.01	0.00
23	*	0.28	0.36	0.37	2.55	4.21	0.00	0.02	0.05	0.00
24	*	0.28	0.27	1.69	0.80	3.11	0.01	0.00	0.03	0.00
25	*	0.28	0.27	1.17	-4.20	-9.25	0.00	0.05	0.24	0.00
26	*	0.27	1.30	-0.07	-7.46	4.24	0.00	0.16	0.05	0.00
27	*	0.26	4.84	5.80	-0.50	2.85	0.09	0.00	0.02	0.00
28	*	0.25	1.34	3.92	6.24	6.16	0.04	0.11	0.11	0.00
29	*	0.24	1.34	-3.08	2.98	0.92	0.03	0.02	0.00	0.00
30	*	0.24	0.45	-0.33	5.37	4.28	0.00	0.08	0.05	0.00
31	*	0.24	0.45	7.26	-0.27	2.29	0.15	0.00	0.01	0.00
32	*	0.23	2.89	-0.18	-3.32	-3.79	0.00	0.03	0.04	0.00
33	*	0.23	1.91	-15.43	-0.52	0.52	0.67	0.00	0.00	0.00
34	*	0.22	1.91	-1.88	3.84	123.95	0.01	0.04	42.92	0.00
35	*	0.21	2.48	24.81	4.74	2.85	1.72	0.06	0.02	0.00
36	*	0.21	1.85	1.83	-3.10	6.56	0.01	0.03	0.12	0.00
37	*	0.20	0.72	12.79	-0.78	1.45	0.46	0.00	0.01	0.00
38	*	0.20	0.72	12.28	-6.44	4.62	0.42	0.12	0.06	0.00
39	*	0.20	1.15	-0.28	4.72	-1.19	0.00	0.06	0.00	0.00
40	*	0.20	1.62	-6.37	-0.67	-1.08	0.11	0.00	0.00	0.00
41	*	0.19	1.99	1.89	-8.54	-6.54	0.01	0.20	0.12	0.00
42	*	0.18	0.07	14.40	4.51	-4.61	0.58	0.06	0.06	0.00
43	*	0.18	0.07	9.39	-0.69	2.07	0.25	0.00	0.01	0.00
44	*	0.17	2.74	7.33	6.69	-17.19	0.15	0.13	0.83	0.00
45	*	0.17	2.59	1.77	-7.15	6.06	0.01	0.14	0.10	0.00
46	*	0.16	0.19	-7.79	-17.64	3.23	0.17	0.87	0.03	0.00
47	*	0.16	0.19	22.82	-4.02	4.76	1.46	0.05	0.06	0.00
48	*	0.15	0.99	-20.57	8.06	-0.10	1.18	0.18	0.00	0.00
49	*	0.15	0.97	-19.31	-4.19	2.99	1.04	0.05	0.03	0.00
50	*	0.15	0.97	-17.45	3.63	-8.20	0.85	0.04	0.19	0.00
51	*	0.14	4.69	-0.90	9.15	-8.89	0.00	0.23	0.22	0.00
52	*	0.14	4.69	-7.71	2.81	0.99	0.17	0.02	0.00	0.00
53	*	0.13	2.72	8.60	12.46	-6.74	0.21	0.43	0.13	0.00
54	*	0.13	0.92	0.79	7.04	-0.67	0.00	0.14	0.00	0.00
55	*	0.12	0.36	1.61	1.43	9.45	0.01	0.01	0.25	0.00
56	*	0.12	0.36	0.20	10.58	-4.30	0.00	0.31	0.05	0.00
57	*	0.12	0.43	1.96	8.12	-5.00	0.01	0.18	0.07	0.00
58	*	0.12	0.32	-0.13	9.78	-2.19	0.00	0.27	0.01	0.00
59	*	0.12	0.32	-3.62	1.04	-0.33	0.04	0.00	0.00	0.00
60	*	0.12	3.15	-2.72	-5.27	-4.05	0.02	0.08	0.05	0.00
61	*	0.12	2.61	4.09	4.02	4.00	0.05	0.05	0.04	0.00
62	*	0.11	1.85	1.66	6.73	-2.16	0.01	0.13	0.01	0.00
63	*	0.11	1.33	-3.37	-9.51	2.34	0.03	0.25	0.02	0.00
64	*	0.11	1.33	6.66	-3.47	-7.52	0.12	0.03	0.16	0.00
65	*	0.10	1.59	0.79	-3.05	6.83	0.00	0.03	0.13	0.00
66	*	0.10	1.59	1.78	-9.61	-0.62	0.01	0.26	0.00	0.00
67	*	0.10	0.96	7.26	-0.95	5.80	0.15	0.00	0.09	0.00
68	*	0.10	0.96	-0.69	4.05	13.03	0.00	0.05	0.47	0.00

69	*	0.10	1.07	-0.75	-4.90	-17.12	0.00	0.07	0.82	0.00
70	*	0.10	1.18	10.67	-0.83	20.19	0.32	0.00	1.14	0.00
71	*	0.09	0.28	-2.78	4.21	-9.26	0.02	0.05	0.24	0.00
72	*	0.09	0.28	0.55	-9.64	5.79	0.00	0.26	0.09	0.00
73	*	0.09	0.16	-3.41	-1.87	1.86	0.03	0.01	0.01	0.00
74	*	0.09	0.16	-1.79	3.27	1.71	0.01	0.03	0.01	0.00
75	*	0.09	0.37	-4.64	-5.92	8.58	0.06	0.10	0.21	0.00
76	*	0.09	0.21	1.69	-1.20	9.63	0.01	0.00	0.26	0.00
77	*	0.09	0.18	0.16	-0.84	-22.30	0.00	0.00	1.39	0.00
78	*	0.09	0.18	3.20	1.08	0.13	0.03	0.00	0.00	0.00
79	*	0.09	0.43	-0.02	0.55	0.71	0.00	0.00	0.00	0.00
80	*	0.09	0.44	-0.14	-4.62	2.11	0.00	0.06	0.01	0.00
81	*	0.09	0.44	-6.20	-4.34	2.94	0.11	0.05	0.02	0.00
82	*	0.09	0.09	-3.47	-7.07	5.19	0.03	0.14	0.08	0.00
83	*	0.09	0.09	1.15	1.54	-6.35	0.00	0.01	0.11	0.00
84	*	0.09	0.64	4.30	0.30	-9.58	0.05	0.00	0.26	0.00
85	*	0.09	0.64	-3.90	2.92	6.72	0.04	0.02	0.13	0.00
86	*	0.09	1.06	3.07	7.88	-0.40	0.03	0.17	0.00	0.00
87	*	0.09	1.06	0.83	-7.28	-1.11	0.00	0.15	0.00	0.00
88	*	0.08	1.97	-1.81	-1.76	3.26	0.01	0.01	0.03	0.00
89	*	0.08	0.03	-16.54	2.46	-6.46	0.76	0.02	0.12	0.00
90	*	0.08	0.03	4.88	3.93	5.04	0.07	0.04	0.07	0.00
91	*	0.08	0.28	-7.46	-0.58	-4.54	0.16	0.00	0.06	0.00
92	*	0.08	0.05	7.34	1.44	0.79	0.15	0.01	0.00	0.00
93	*	0.08	0.05	1.38	0.80	0.09	0.01	0.00	0.00	0.00
94	*	0.08	0.28	-15.26	-0.36	-3.44	0.65	0.00	0.03	0.00
95	*	0.08	0.41	5.56	-0.65	0.87	0.09	0.00	0.00	0.00
96	*	0.08	0.43	-0.70	-0.91	-7.95	0.00	0.00	0.18	0.00
97	*	0.08	0.43	-7.62	0.59	-2.12	0.16	0.00	0.01	0.00
98	*	0.08	1.05	-3.25	0.39	9.10	0.03	0.00	0.23	0.00
99	*	0.08	1.11	28.76	6.75	-22.17	2.31	0.13	1.37	0.00
100	*	0.08	0.82	12.78	5.69	-39.45	0.46	0.09	4.35	0.00
101	*	0.08	0.82	1.97	1.81	-9.11	0.01	0.01	0.23	0.00
102	*	0.07	1.38	9.75	-14.49	-24.42	0.27	0.59	1.67	0.00
103	*	0.07	1.80	0.84	-1.12	-4.78	0.00	0.00	0.06	0.00
104	*	0.07	1.98	19.86	1.89	-6.83	1.10	0.01	0.13	0.00
105	*	0.07	0.63	27.28	13.32	-5.07	2.08	0.50	0.07	0.00
106	*	0.07	0.63	-18.33	1.91	-10.87	0.94	0.01	0.33	0.00
107	*	0.07	0.10	33.85	2.88	4.50	3.20	0.02	0.06	0.00
108	*	0.07	0.10	-10.88	-0.84	-4.83	0.33	0.00	0.07	0.00
109	*	0.07	0.20	-40.48	0.74	-24.33	4.58	0.00	1.65	0.00
110	*	0.07	0.20	8.44	3.19	7.11	0.20	0.03	0.14	0.00
111	*	0.07	0.43	26.00	-2.37	7.04	1.89	0.02	0.14	0.00
112	*	0.07	0.43	-5.44	0.94	-6.24	0.08	0.00	0.11	0.00
113	*	0.07	0.67	3.22	-4.53	5.83	0.03	0.06	0.09	0.00
114	*	0.07	1.80	-40.06	-2.26	-6.58	4.49	0.01	0.12	0.00
115	*	0.06	0.92	-37.58	-4.02	21.71	3.95	0.05	1.32	0.00
116	*	0.06	0.29	-1.39	1.18	-30.29	0.01	0.00	2.56	0.00
117	*	0.06	0.29	-7.00	0.12	-37.32	0.14	0.00	3.89	0.00
118	*	0.06	0.34	-2.59	2.27	-2.04	0.02	0.01	0.01	0.00
119	*	0.06	0.34	0.51	2.20	-15.13	0.00	0.01	0.64	0.00
120	*	0.06	0.23	-1.99	-3.68	-16.73	0.01	0.04	0.78	0.00
121	*	0.06	0.23	0.57	2.84	-24.01	0.00	0.02	1.61	0.00
122	*	0.06	0.29	23.02	-3.95	7.40	1.48	0.04	0.15	0.00
123	*	0.06	0.29	-2.73	7.04	-13.07	0.02	0.14	0.48	0.00
124	*	0.06	1.10	-8.56	9.64	-13.78	0.21	0.26	0.53	0.00
125	*	0.06	0.71	-2.60	12.72	18.31	0.02	0.45	0.94	0.00
126	*	0.06	0.71	-1.83	4.25	-5.86	0.01	0.05	0.10	0.00
127	*	0.06	0.40	-4.30	5.12	-8.80	0.05	0.07	0.22	0.00
128	*	0.06	0.40	-7.24	7.74	-8.85	0.15	0.17	0.22	0.00
129	*	0.06	0.49	-12.07	10.02	-1.50	0.41	0.28	0.01	0.00
130	*	0.06	0.49	-15.55	8.24	-6.28	0.68	0.19	0.11	0.00
131	*	0.06	0.69	4.14	-0.17	-5.94	0.05	0.00	0.10	0.00
132	*	0.06	0.51	2.68	2.63	13.30	0.02	0.02	0.49	0.00
133	*	0.06	0.51	-2.14	5.33	10.74	0.01	0.08	0.32	0.00
134	*	0.06	0.70	6.78	-3.70	-0.55	0.13	0.04	0.00	0.00
135	*	0.05	0.47	-7.04	-2.32	0.94	0.14	0.02	0.00	0.00
136	*	0.05	0.15	7.29	-3.73	-1.08	0.15	0.04	0.00	0.00
137	*	0.05	0.15	2.88	-10.38	-7.49	0.02	0.30	0.16	0.00
138	*	0.05	1.25	0.59	-4.93	-2.26	0.00	0.07	0.01	0.00
139	*	0.05	0.52	8.47	-8.71	-2.63	0.20	0.21	0.02	0.00
140	*	0.05	0.52	-4.06	-2.64	3.08	0.05	0.02	0.03	0.00
141	*	0.05	0.62	2.06	0.69	0.40	0.01	0.00	0.00	0.00
142	*	0.05	0.27	0.51	5.08	2.78	0.00	0.07	0.02	0.00
143	*	0.05	0.27	1.78	2.79	1.72	0.01	0.02	0.01	0.00
144	*	0.05	0.70	8.04	-0.37	-5.77	0.18	0.00	0.09	0.00
145	*	0.05	0.42	-1.69	-1.65	-5.62	0.01	0.01	0.09	0.00
146	*	0.05	0.33	-3.30	-0.16	-15.31	0.03	0.00	0.65	0.00
147	*	0.05	0.33	2.75	-2.40	6.85	0.02	0.02	0.13	0.00

148	*	0.05	0.13	0.27	-1.00	-0.48	0.00	0.00	0.00	0.00
149	*	0.05	0.13	0.55	-1.65	-3.78	0.00	0.01	0.04	0.00
150	*	0.05	0.16	3.53	-1.00	-2.49	0.03	0.00	0.02	0.00
Tot.cons.							43.37	85.69	79.24	0.00

Materiali

Cemento armato

Elenco dei criteri di progetto e delle loro principali caratteristiche meccaniche utilizzate:
Sezioni generiche: 10 Nessun controllo di normativa

Calcestruzzo

Tipo di calcestruzzo: C28/35
Rck calcestruzzo <daN/cmq>: 350.00
Resistenza caratteristica cilindrica (Fck) <daN/cmq>: 290.50
Resistenza caratteristica a trazione (Fctk) <daN/cmq>: 19.84
α_{cc}: 0.85
γ_c: 1.50
Resistenza di progetto cilindrica (Fcd) <daN/cmq>: 164.62
Resistenza di progetto a trazione (Fctd) <daN/cmq>: 13.23

Acciaio

Tipo di acciaio: B450C
Tensione caratteristica di snervamento (Fyk) <daN/cmq>: 4500.00
γ_s: 1.15
Tensione di progetto di snervamento (Fyd) <daN/cmq>: 3913.04

Acciaio

Elenco dei criteri di progetto e delle loro principali caratteristiche meccaniche utilizzate:
"Aste in acciaio: 1 "

Tipo di acciaio: S355 UNI EN 10025-2
Elenco dei criteri di progetto e delle loro principali caratteristiche meccaniche utilizzate:
"Aste in acciaio: 1 "

Tipo di acciaio: S355H UNI EN 10210-1
"Nodi in acciaio: 1 Piastre di fondazione"
"Piastre di fondazione"
Classe bulloni: 4.6
Classe Saldature: SECONDA

Spostamento relativo tra i due nodi

Max = 0.00